# Sepam series 80 <br> Protection, metering and control functions 

## User's manual 02/2016



## Safety instructions

## Safety symbols and messages

Read these instructions carefully and look at the equipment to become familiar with the device before trying to install, operate, service or maintain it. The following special messages may appear throughout this bulletin or on the equipment to warn of potential hazards or to call attention to information that clarifies or simplifies a procedure.

Risk of electric shock
The addition of either symbol to a Danger or Warning safety label indicates that an electrical hazard exists, which will result in personal injury if the instructions are not followed.


## Safety alert

This is the safety alert symbol. It is used to alert you to potential personal injury hazards. Obey all safety messages that follow this symbol to avoid possible injury or death.

## Safety messages

## DANGER

DANGER indicates an imminently hazardous situation which, if not avoided, will result in death or serious injury.

## A WARNING

WARNING indicates a potentially hazardous situation which, if not avoided, can result in death or serious injury.

## A CAUTION

CAUTION indicates a potentially hazardous situation which, if not avoided, can result in minor or moderate injury.

## NOTICE

NOTICE, used without the safety alert symbol, indicates a potentially hazardous situation which, if not avoided, can result in equipment damages.

## Important notes

## Restricted liability

Electrical equipment should be serviced and maintained only by qualified personnel. No responsibility is assumed by Schneider Electric for any consequences arising out of the use of this manual. This document is not intended as an instruction manual for untrained persons.

## Device operation

The user is responsible for checking that the rated characteristics of the device are suitable for its application. The user is responsible for reading and following the device's operating and installation instructions before attempting to commission or maintain it. Failure to follow these instructions can affect device operation and constitute a hazard for people and property.

## Protective grounding

The user is responsible for compliance with all the existing international and national electrical codes concerning protective grounding of any device.

## Introduction

Metering functions

## Protection functions

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The selection guide by application suggests Sepam type(s) suitable for your protection requirements, based on your application characteristics. The most typical applications are presented along with the associated Sepam type.
Each application example is described:
$\square$ By a single-line diagram specifying
ㅁ the device to be protected

- the device to be protected
$\square$ the network configuration
$\square$ the position of the metering sensors
- By the standard and specific Sepam functions to be implemented to protect the application concerned.


Applications


Series 40


| $\square$ | - | - | - | - |
| :---: | :---: | :---: | :---: | :---: |
| $\square$ | - | - |  | - |
| - | Directional earth fault |  | Directional earth fault | - |
| S40) | S41 | S42 | S43 | 544 |
| S50 ${ }^{(4)}$ | S51(4) | S52 ${ }^{(44)}$ | S53(4) | S54 |

T40
T42
T50 ${ }^{(5)}$
T52 ${ }^{(5)}$

## G40

| 0 to 10 |
| :--- |
| 4 to 8 |
| 0 to 16 |
| $3 \mathrm{I}+10$ |
| 3 V |
| Yes |
| 1 to 2 |
| Yes |
| Yes |
| - |
| - |
| - |

(4) S5X applications are identical to S4X applications with the following additional functions:

- earth fault and phase overcurrent cold load pick-up
- broken conductor detection
- fault locator
(5) T5X applications are identical to T4X applications with the following additional functions:
- earth fault and phase overcurrent cold load pick-up
- broken conductor detection

The list of protection functions is given for information only.
Direct earthing or impedance earthing have been represented by the same pictogram, i.e. by a direct earthing system.


## Protection functions suitable for low voltage

## Low voltage earthing systems

There are 4 low voltage (LV) earthing systems designated by a 2 or 3-letter acronym:

- TN-S
- TN-C

■ TT

- IT

| Letter | Meaning |
| :---: | :---: |
| First letter | Transformer neutral point |
| 1 | Earthed with an impedance |
| T | Directly earthed |
| Second letter | Electrical exposed conductive parts of the consumer |
| T | Earthed |
| N | Connected to the neutral conductor |
| Third letter (optional) | Protective Earth conductor |
| S | Separate N neutral conductor and PE Protective Earth conductor |
| C | Combined N neutral conductor and PE Protective Earth conductor (PEN) |

## Protection functions suitable for low voltage

## Compatibility of Sepam low voltage protection functions

Sepam protection functions can be used with low voltage (LV) as long as the conditions below are met:

- The distribution circuit must be rated higher than 32 A .

■ The installation must comply with standard IEC 60364.
For additional information about the compatibility of Sepam protection functions with low voltage, please contact Schneider Electric technical support.

The table below lists the Sepam protection functions suitable for low voltage according to the earthing system used. Sepam protection functions not listed in this table are not suitable for low voltage. The protection functions listed in this table are available according to the Sepam type.


The Sepam range of protection relays is designed for the operation of machines and electrical distribution networks of industrial installations and utility substations at all levels of voltage.
It includes 4 families
■ Sepam series 20
■ Sepam series 40

- Sepam series 60

■ Sepam series 80
to cover all needs, from the simplest to the most complete.


Sepam series 80 with integrated advanced UMI.

## Sepam series 80, intelligent solutions for custom applications

Specially designed for demanding customers on large industrial sites, Sepam series 80 provides proven solutions for electrical distribution and machine protection.

## Main characteristics

■ protection of closed ring networks or networks with parallel incomers by directional protection and logic discrimination
■ directional earth fault protection for impedance-earthed and isolated or compensated neutral systems

- complete protection of transformers and machine-transformer units
- stable, sensitive differential protection with neural network restraint - linked to all necessary backup protection functions
- complete protection of motors and generators
- against internal faults:
- stable, sensitive machine differential protection, with starting and sensor loss restraint
- field loss, stator earth fault, etc.
$\square$ against network and process faults: pole slip, speed control, inadvertent energization, etc.
■ synchro-check between 2 networks before coupling
- measurement of harmonic distortion, current and voltage, to assess network power quality
- 42 inputs / 23 outputs for comprehensive equipment control

■ mimic-based UMI for local switchgear control

- SFT2841 parameter setting and operating software, a simple and complete tool that is indispensable for all Sepam users:
$\square$ assisted preparation of parameter and protection settings
- complete information during commissioning
$\square$ remote equipment management and diagnostics during operation
- logic equation editor built into the SFT2841 software to adapt the predefined control functions
■ optional SFT2885 programming software (Logipam), to program specific control and monitoring functions
- 2 communication ports to integrate Sepam in 2 different networks or redundant architectures
■ removable memory cartridge to get equipment in operation again quickly after the replacement of a faulty base unit
■ battery backup to save historical and disturbance recording data.


## Selection guide

The Sepam series $\mathbf{8 0}$ family includes 16 types to offer the right solution for each application.

| Specific protection functions available | Applications |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Substation | Transformer | Motor | Generator | Busbar | Capacitor |
|  | S80 |  |  |  | B80 |  |
| Directional earth fault | S81 | T81 | M81 |  |  |  |
| Directional earth fault and phase overcurrent | S82 | T82 |  | G82 |  |  |
| Check on 3 phase voltages on 2 sets of busbars |  |  |  |  | B83 |  |
| Rate of change of frequency | S84 |  |  |  |  |  |
| Capacitor bank unbalance |  |  |  |  |  | C86 |
| Transformer or machine differential |  | T87 | M87 | G87 |  |  |
| Machine-transformer unit differential |  |  | M88 | G88 |  |  |Base unit, with different types of User-Machine Interface (UMI):

- Integrated mimic-based UMI
- Integrated or remote advanced UMIParameter and protection settings saved on removable memory cartridge42 logic inputs and 23 relay outputs with 3 optional modules providing 14 inputs and 6 outputs

2 independent communication ports

- Connection:
- direct, to 2-wire RS 485, 4-wire RS 485 or fiber optic networks
- to Ethernet TCP/IP network via PowerLogic Ethernet server (Transparent Ready ${ }^{\text {TM }}$ )
- Protocols:
- DNP3 and IEC 60870-5-103 with ACE969
communication interface
- IEC 61850 and Modbus TCP with ACE850 communication interface

Processing of data from 16 temperature sensors
Pt100, Ni100 or Ni120
1 low level analog output
$0-10 \mathrm{~mA}, 0-10 \mathrm{~mA}, 4-20 \mathrm{~mA}$ or $0-20 \mathrm{~mA}$Synchro-check module
Software tools:

- Sepam parameter and protection setting and adaptation of the predefined functions
- Local or remote installation operation
- Programming of specific functions (Logipam)
- Retrieval and display of disturbance recording data


## Flexibility and upgrading capability

To adapt to as many situations as possible, and allow for future installation upgrading, optional modules may be added to Sepam at any time for new functions.


## Ease of installation

■ Light, compact base unit
■ Easy to integrate due to Sepam's adaptation capabilities:

- universal supply voltage for Sepam and its logic inputs: 24 to 250 V DC
- phase currents can be measured by 1 A or 5 A current transformers, or LPCT
(Low Power Current Transducer) type sensors
- residual current calculated or measured by a choice of methods to fit requirements
- The same, easy-to-install remote modules for all Sepam units:
- mounted on DIN rail
- connected to the Sepam base unit by prefabricated cords


## Commissioning assistance

■ Predefined functions implemented by simple parameter setting
■ User-friendly, powerful SFT2841 PC setting software tool used on all Sepam units to provide users with all the possibilities offered by Sepam

## Intuitive use

■ Integrated or remote advanced User Machine Interface (UMI) installed in the most convenient place for the facility manager

- Integrated mimic-based User Machine Interface for local control of switchgear

■ User-friendly User Machine Interface, with direct access to data

- Clear graphic LCD display of all data required for local operation and installation diagnosis
■ Working language can be customized to be understood by all users.


The figures indicate the number of relays available for each protection function.

- standard, - optional
(1) Protection functions with 2 groups of settings
(2) According to parameter setting and optional MES120 input/output modules
(3) With optional MET148-2 temperature input module
(4) With optional MCSO25 synchro-check module

|  |  | stati |  |  |  | Tran | sform |  |  | Iotor |  |  |  | erator |  |  |  | Cap. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Metering | S80 S81 S82 S84 |  |  |  |  | T81 T82 T87 |  |  | M81 M87 M88 |  |  |  | G82 G87 G88 |  |  | B80 B83 |  | C86 |
| Phase current I1, I2, I3 RMS | - | - |  | ■ | - | - | - | - | $\square$ |  | $\square$ | ■ | - | ■ | $\square$ | - | ■ | $\square$ |
| Measured residual current 10 , calculated $10 \Sigma$ | $\square$ | $\square$ |  | $\square$ | - | $\square$ | $\square$ | $\square$ |  |  | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | ■ | $\square$ |
| Demand current I1, I2, I3 | $\square$ | $\square$ |  | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ |  |  | $\square$ | - | $\square$ | $\square$ | $\square$ | - | $\square$ | $\square$ |
| Peak demand current IM1, IM2, IM3 | $\square$ | $\square$ |  | - | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ |  | $\square$ | $\square$ | $\square$ | - | $\square$ | $\square$ | $\square$ | $\square$ |
| Measured residual current I'0 | - | ■ |  | - | - | $\square$ | - | - | - | - | - | - | $\square$ | - | $\square$ | - |  | $\square$ |
| Voltage U21, U32, U13, V1, V2, V3 | - | - |  | $\square$ | - | $\square$ | ■ | $\square$ |  |  | ■ | $\square$ | $\square$ | $\square$ | $\square$ | - | - | $\square$ |
| Residual voltage V0 | $\square$ | $\square$ |  | $\square$ | $\square$ | $\square$ | $\square$ | - |  |  | $\square$ | - | $\square$ | - | $\square$ | $\square$ | - | $\square$ |
| Positive sequence voltage Vd/rotation direction | $\square$ | $\square$ |  | $\square$ | $\square$ | - | $\square$ | $\square$ |  |  | - | - | $\square$ | $\square$ | $\square$ | - | $\square$ | $\square$ |
| Negative sequence voltage Vi | $\square$ | - |  | $\square$ | - | $\square$ | $\square$ | - |  |  |  | $\square$ | $\square$ | $\square$ | $\square$ | - | ■ | $\square$ |
| Frequency | $\square$ | - |  | - | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ |  | $\square$ | $\square$ | $\square$ | - |  | $\square$ |  | $\square$ |
| Active power P, P1, P2, P3 | - | $\square$ |  | $\square$ | - | $\square$ | $\square$ | $\square$ |  |  | - | $\square$ | $\square$ | $\square$ | $\square$ | - | $\square$ | $\square$ |
| Reactive power Q, Q1, Q2, Q3 | $\square$ | $\square$ |  | - | $\square$ |  | - | $\square$ |  |  | - | $\square$ | $\square$ | $\square$ | $\square$ | - | - | $\square$ |
| Apparent power S, S1, S2, S3 | $\square$ | $\square$ |  | - | $\square$ |  | $\square$ | $\square$ |  |  | $\square$ | - | $\square$ | - | $\square$ | - | $\square$ | $\square$ |
| Peak demand power PM, QM | - | $\square$ |  | - | $\square$ |  | $\square$ | $\square$ |  |  | $\square$ | $\square$ | - | $\square$ | - | - | $\square$ | $\square$ |
| Power factor | $\square$ | - |  | - | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ |  | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ |
| Calculated active and reactive energy ( $\pm$ Wh, $\pm$ VARh) | $\square$ | $\square$ |  | - | $\square$ | $\square$ | - | $\square$ | - | - | $\square$ | $\square$ | $\square$ | ■ | $\square$ | $\square$ | ■ | $\square$ |
| Active and reactive energy by pulse counting ${ }^{(1)}$ $( \pm \mathrm{Wh}, \pm \text { VARh })$ | $\square$ | $\square$ |  | - | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ |  | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ |
| Phase current l'1, I'2, I'3 RMS |  |  |  |  |  |  |  | $\square$ |  |  |  | ■ |  | - | ■ |  |  |  |
| Calculated residual current l'0 |  |  |  |  |  |  |  | $\square$ |  |  | $\square$ | $\square$ |  | $\square$ | $\square$ |  |  |  |
| Voltage U'21, V'1 and frequency |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | $\square$ |  |  |
| Voltage U'21, U'32, U'13, V'1, V'2, V'3, V'd, V'i and frequency |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | - |  |
| Residual voltage V'0 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | $\square$ |  |
| Temperature (16 RTDs) ${ }^{(2)}$ |  |  |  |  |  | $\square$ | $\square$ | $\square$ | $\square$ |  | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ |  |  | $\square$ |
| Rotation speed (1) |  |  |  |  |  |  |  |  | $\square$ |  | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ |  |  |  |
| Neutral point voltage Vnt |  |  |  |  |  |  |  |  | - |  | - | $\square$ | $\square$ | ■ | $\square$ |  |  |  |
| Control and monitoring |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Circuit breaker / contactor control 94/69 | $\square$ | $\square$ | $\square$ |  | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ |  | ㅁ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ |
| Automatic transfer (AT) ${ }^{(1)}$ | $\square$ | ㅁ | $\square$ |  | $\square$ | $\square$ | $\square$ | $\square$ |  |  |  |  | $\square$ | $\square$ | - | 口 | $\square$ |  |
| Load shedding / automatic restart |  |  |  |  |  |  |  |  | - |  | - | - |  |  |  |  |  |  |
| De-excitation |  |  |  |  |  |  |  |  |  |  |  |  | - | - | ■ |  |  |  |
| Genset shutdown |  |  |  |  |  |  |  |  |  |  |  |  | $\square$ | ■ | $\square$ |  |  |  |
| Capacitor step control ${ }^{(1)}$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | $\square$ |
| Logic discrimination ${ }^{(1)} \quad 68$ | $\square$ | $\square$ | $\square$ |  | $\square$ | $\square$ | $\square$ | $\square$ | ㅁ |  | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ |
| Latching / acknowledgement 86 | $\square$ | $\square$ | $\square$ |  | - | $\square$ | $\square$ | $\square$ | $\square$ |  | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ |
| Annunciation 30 | - | $\square$ | $\square$ |  | - | $\square$ | $\square$ | $\square$ | - |  | $\square$ | - | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ |
| Triggering a Motor start report |  |  |  |  |  |  |  |  | - |  | - | - |  |  |  |  |  |  |
| Activating/Deactivating a Data log | - | $\square$ | - |  | - | $\square$ | ■ | ■ | $\square$ |  | $\square$ | - | - | ■ | $\square$ | - | ■ | $\square$ |
| Change of phase rotation direction | $\square$ | $\square$ | $\square$ |  | - | $\square$ | $\square$ | $\square$ | - |  | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | - | $\square$ | $\square$ |
| Switching of groups of settings | - | - | - |  | - | $\square$ | - | ■ | $\square$ |  | $\square$ | - | - | $\square$ | $\square$ | - | - | $\square$ |
| Adaptation using logic equations | $\square$ | - | $\square$ |  | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ |  | $\square$ | ■ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ |
| Logipam programming (Ladder language) | $\square$ | ㅁ | $\square$ |  | $\square$ | - | $\square$ | $\square$ | ㅁ |  | ㅁ | $\square$ | $\square$ | $\square$ | $\square$ | ㅁ | $\square$ | $\square$ |
| The figures indicate the number of relays available for each protection function. standard, a optional <br> (1) According to parameter setting and optional MES120 input/output modules <br> (2) With optional MET148-2 temperature input module |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |


|  | Substation | Transformer | Motor | Generator | Busbar | Cap. |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Network and machine diagnosis | S80 S81 S82 S84 T81 T82 T87 M81 M87 M88 G82 G87 G88 B80 B83 C86 |  |  |  |  |  |

Network and machine diagnosis S80 S81 S82 S84 T81 T82 T87 M81 M87 M88 G82 G87 G88 B80 B83 C86

| Tripping context <br> Tripping current Tripl1, Tripl2, Tripl3 |  |  |  | $\square$ |  | $\square$ | $■$ |  |  | $■$ |  | $■$ |  | $\square$ |  | $■$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Phase fault and earth fault trip counters | $\square$ | ■ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | ■ | $\square$ | $\square$ | $\square$ | ■ | $\square$ | $\square$ |
| Unbalance ratio / negative sequence current li | $\square$ | ■ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ |
| Harmonic distortion (THD), current and voltage lthd, Uthd | ■ | ■ | ■ | ■ | $\square$ | $\square$ | ■ | ■ | $\square$ | ■ | ■ | $\square$ | ■ | ■ | ■ | $\square$ |
| Phase displacement $\varphi 0, \varphi^{\prime} 0, \varphi 0 \Sigma$ Phase displacement $\varphi 1, \varphi 2, \varphi 3$ |  |  |  |  |  | $\square$ |  |  |  | $\square$ |  | $\square$ |  |  |  |  |
| Disturbance recording | $\square$ | ■ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | ■ | $\square$ | $\square$ | $\square$ |
| Motor start report (MSR) |  |  |  |  |  |  |  | $\square$ | $\square$ | $\square$ |  |  |  |  |  |  |
| Motor start trend (MST) |  |  |  |  |  |  |  | $\square$ | $\square$ | ■ |  |  |  |  |  |  |
| Data log (DLG) | ■ | ■ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ |
| Thermal capacity used |  | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | ■ | $\square$ | $\square$ | $\square$ |  |  | $\square$ |
| Remaining operating time before overload tripping Waiting time before closing authorization |  | ■ | ■ | ■ | $\square$ | $\square$ | ■ |  |  |  | $\square$ | $\square$ | ■ |  |  | ■ |
| Running hours counter / operating time |  |  |  |  | ■ | ■ | ■ | $\square$ | $\square$ | ■ | $\square$ | $\square$ | ■ |  |  | $\square$ |
| Starting current and time |  |  |  |  |  |  |  | $\square$ | $\square$ | ■ |  |  |  |  |  |  |
| Start inhibit time <br> Number of starts before inhibition |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Unbalance ratio / negative sequence current l'i |  |  |  |  |  |  | $\square$ |  | $\square$ | ■ |  | $\square$ | ■ |  |  |  |
| Differential current Idiff1, Idiff2, Idiff3 Through current It1, It2, It3 Current I and l' phase displacement $\theta$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Apparent positive sequence impedance Zd Apparent phase-to-phase impedances Z21, Z32, Z13 |  |  |  |  |  |  |  |  |  |  |  | $\square$ |  |  |  |  |
| Third harmonic voltage, neutral point or residual |  |  |  |  |  |  |  |  |  |  | $\square$ | $\square$ | $\square$ |  |  |  |
| Difference in amplitude, frequency and phase of voltages compared for synchro-check ${ }^{(1)}$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ |  |  |  | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ |  |
| Capacitor unbalance current and capacitance |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | $\square$ |
| Switchgear diagnosis ANSI coc |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| CT / VT supervision 60/60FL | ■ | ■ | $\square$ | $\square$ | ■ | $\square$ | $\square$ | $\square$ | ■ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | ■ | $\square$ |
| Trip circuit supervision ${ }^{(2)} \quad 74$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ |
| Auxiliary power supply monitoring | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | ■ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ |
| Cumulative breaking current | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ |
| Number of operations, operating time, charging time, number of racking out operations ${ }^{(2)}$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | number of racking out operations ${ }^{(2)}$

## Modbus, IEC 60870-5-103, DNP3 communication or IEC 61850 (Editions 1 and 2)

Remote indication and time tagging of events ${ }^{(3)}$ (4)
Remote control orders (3) (4)
Remote protection setting (3) (4)
Transfer of disturbance recording data ${ }^{(3)}$ (4)
IEC 61850 GOOSE message ${ }^{(4)}$
The figures indicate the number of relays available for each protection function.

- standard, $\square$ optional
(1) With optional MCS025 synchro-check module
(2) According to parameter setting and optional MES120 input/output modules
(3) With ACE949-2, ACE959, ACE937, ACE969TP-2 or ACE969FO-2 communication interface
(4) With ACE850TP or ACE850FO communication interface


| Electromagnetic compatibility | Standard | Level/Class | Value |
| :---: | :---: | :---: | :---: |
| Emission tests |  |  |  |
| Disturbing field emission | IEC 60255-25 |  |  |
|  | EN 55022 | A |  |
| Conducted disturbance emission | IEC 60255-25 |  |  |
|  | EN 55022 | A |  |
| Immunity tests - Radiated disturbances |  |  |  |
| Immunity to radiated fields | IEC 60255-22-3 |  | $10 \mathrm{~V} / \mathrm{m} ; 80 \mathrm{MHz}-1 \mathrm{GHz}$ |
|  | IEC 61000-4-3 | III | $10 \mathrm{~V} / \mathrm{m} ; 80 \mathrm{MHz}-2 \mathrm{GHz}$ |
|  |  |  | $30 \mathrm{~V} / \mathrm{m}$ non-modulated; $800 \mathrm{MHz}-2 \mathrm{GHz}{ }^{(1)}$ |
|  | ANSI C37.90.2 (2004) |  | $20 \mathrm{~V} / \mathrm{m} ; 80 \mathrm{MHz}-1 \mathrm{GHz}$ |
| Electrostatic discharge | IEC 61000-4-2 ${ }^{(1)}$ | IV | 15 kV air ; 8 kV contact |
|  | IEC 60255-22-2 |  | 8 kV air; 6 kV contact |
|  | ANSI C37.90.3 |  | 8 kV air; 4 kV contact |
| Immunity to magnetic fields at network frequency ${ }^{(2)}$ | IEC 61000-4-8 | 4 | $30 \mathrm{~A} / \mathrm{m}$ (continuous) - $300 \mathrm{~A} / \mathrm{m}$ (1-3 s) |
| Immunity to pulsed magnetic fields ( ${ }^{(1)}$ | IEC 61000-4-9 | IV | $600 \mathrm{~A} / \mathrm{m}$ |
| Immunity to magnetic fields with damped oscillating waves ${ }^{(1)}$ | IIEC 61000-4-10 | 5 | $100 \mathrm{~A} / \mathrm{m}$ |
| Immunity tests - Conducted disturbances |  |  |  |
| Immunity to conducted RF disturbances | IEC 60255-22-6 | III | 10 V |
| Electrical fast transients/burst | IEC 60255-22-4 | A and B | $4 \mathrm{kV} ; 2.5 \mathrm{kHz} / 2 \mathrm{kV} ; 5 \mathrm{kHz}$ |
|  | IEC 61000-4-4 | IV | 4 kV ; 2.5 kHz |
|  | ANSI C37.90.1 |  | 4 kV ; 2.5 kHz |
| 1 MHz damped oscillating wave | IEC 60255-22-1 |  | $2.5 \mathrm{kV} \mathrm{CM} ; 1 \mathrm{kV} \mathrm{DM}$ |
|  | ANSI C37.90.1 |  | 2.5 kV CM; 2.5 kV DM |
| 100 kHz damped sinusoidal wave | IEC 61000-4-12 | III | 2 kV MC |
|  |  | IV (1) | $4 \mathrm{kV} \mathrm{MC} \mathrm{;} \mathrm{2,5} \mathrm{kV} \mathrm{DM}$ |
| Slow damped oscillating wave ( 100 kHz to 1 MHz ) | IEC 61000-4-18 | III |  |
| Fast damped oscillating wave ( $3 \mathrm{MHz}, 10 \mathrm{MHz}, 30 \mathrm{MHz}$ ) | IEC 61000-4-18 | III |  |
| Surges | IEC 61000-4-5 | III | $2 \mathrm{kV} \mathrm{CM;} 1$ kV DM |
|  | GOST R 50746-2000 ${ }^{(1)}$ | 4 | 200 A |
| Immunity to conducted disturbances in common mode from 0 Hz to 150 kHz | IEC 61000-4-16 | III |  |
| Voltage interruptions | IEC 60255-11 |  | 100\% for 100 ms |
| Mechanical robustness | Standard | Level/Class | Value |
| Energized |  |  |  |
| Vibrations | IEC 60255-21-1 | 2 | $1 \mathrm{Gn} ; 10 \mathrm{~Hz}-150 \mathrm{~Hz}$ |
|  | IEC 60068-2-6 | Fc | $3 \mathrm{~Hz}-13.2 \mathrm{~Hz} ; \mathrm{a}= \pm 1 \mathrm{~mm}$ |
|  | IEC 60068-2-64 | 2M1 |  |
| Shocks | IEC 60255-21-2 | 2 | $10 \mathrm{Gn} / 11 \mathrm{~ms}$ |
| Earthquakes | IEC 60255-21-3 | 2 | 2 Gn (horizontal) |
|  |  |  | 1 Gn (vertical) |
| De-energized |  |  |  |
| Vibrations | IEC 60255-21-1 | 2 | $2 \mathrm{Gn} ; 10 \mathrm{~Hz}-150 \mathrm{~Hz}$ |
| Shocks | IEC 60255-21-2 | 2 | $27 \mathrm{Gn} / 11 \mathrm{~ms}$ |
| Jolts | IEC 60255-21-2 | 2 | $20 \mathrm{Gn} / 16 \mathrm{~ms}$ |

(1) Test conducted with a mimic-based HMI in the case of GOST performance testing.
(2) When protection functions $50 \mathrm{~N} / 51 \mathrm{~N}$ or 67 N are used and 10 is calculated on the sum of the phase currents, IsO must be higher than 0.1 In 0 .

| Climatic withstand | Standard | Level/Class | Value |
| :---: | :---: | :---: | :---: |
| During operation |  |  |  |
| Exposure to cold | IEC 60068-2-1 | Ad | $-25^{\circ} \mathrm{C}\left(-13^{\circ} \mathrm{F}\right)$ |
| Exposure to dry heat | IEC 60068-2-2 | Bd | $+70^{\circ} \mathrm{C}\left(+158^{\circ} \mathrm{F}\right)$ |
| Continuous exposure to damp heat | IEC 60068-2-78 | Cab | 10 days; $93 \% \mathrm{RH} ; 40^{\circ} \mathrm{C}\left(104^{\circ} \mathrm{F}\right)$ |
| Salt mist | IEC 60068-2-52 | Kb/2 | 3 days |
| Influence of corrosion/2-gas test | IEC 60068-2-60 | Method 1 | $\begin{aligned} & 21 \text { days; } 75 \% \mathrm{RH} ; 25^{\circ} \mathrm{C}\left(77^{\circ} \mathrm{F}\right) \text {; } \\ & 0.1 \mathrm{ppm} \mathrm{H} \mathrm{H}_{2} \mathrm{~S} ; 0.5 \mathrm{ppm} \mathrm{SSO}_{2} \end{aligned}$ |
| Influence of corrosion/4-gas test | IEC 60068-2-60 | Method 4 | 21 days; $75 \% \mathrm{RH} ; 25^{\circ} \mathrm{C}\left(77^{\circ} \mathrm{F}\right)$; <br> $0.01 \mathrm{ppm} \mathrm{H} \mathrm{H}_{2} \mathrm{~S} ; 0.2 \mathrm{ppm} \mathrm{SO} \mathrm{S}_{2}$; <br> $0.2 \mathrm{ppm} \mathrm{NO} 2 ; 0.01 \mathrm{ppm} \mathrm{Cl}{ }_{2}$ |
|  | EIA 364-65A | IIIA | 42 days ; $75 \% \mathrm{RH}$; $30^{\circ} \mathrm{C}\left(86^{\circ} \mathrm{F}\right)$; <br> $0.1 \mathrm{ppm} \mathrm{H}_{2} \mathrm{~S} ; 0.2 \mathrm{ppm} \mathrm{SO}_{2}$; <br> $0.2 \mathrm{ppm} \mathrm{NO} \mathrm{N}_{2} ; 0.02 \mathrm{ppm} \mathrm{Cl} 2$ |
| In storage ${ }^{(1)}$ |  |  |  |
| Temperature variation with specified variation rate | IEC 60068-2-14 | Nb | $-25^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}\left(-13^{\circ} \mathrm{F}\right.$ to $\left.+158^{\circ} \mathrm{F}\right) 5^{\circ} \mathrm{C} / \mathrm{min}$ |
| Exposure to cold | IEC 60068-2-1 | Ab | $-25^{\circ} \mathrm{C}\left(-13^{\circ} \mathrm{F}\right)$ |
| Exposure to dry heat | IEC 60068-2-2 | Bb | $+70^{\circ} \mathrm{C}\left(+158^{\circ} \mathrm{F}\right)$ |
| Continuous exposure to damp heat | IEC 60068-2-78 | Cab | 56 days; $93 \% \mathrm{RH} ; 40^{\circ} \mathrm{C}\left(104^{\circ} \mathrm{F}\right)$ |
|  | IEC 60068-2-30 | Db | 6 days; $95 \% \mathrm{RH} ; 55^{\circ} \mathrm{C}$ ( $131{ }^{\circ} \mathrm{F}$ ) |
| Safety | Standard | Level/Class | Value |
| Enclosure safety tests |  |  |  |
| Front panel tightness | IEC 60529 | IP52 | Other panels IP20 |
|  | NEMA | Type 12 |  |
| Fire withstand | IEC 60695-2-11 |  | $650^{\circ} \mathrm{C}\left(1200^{\circ} \mathrm{F}\right)$ with glow wire |
| Electrical safety tests |  |  |  |
| $1.2 / 50 \mu$ s impulse wave | IEC 60255-5 |  | $5 \mathrm{kV}{ }^{(2)}$ |
| Power frequency dielectric withstand | IEC 60255-5 |  | $2 \mathrm{kV} 1 \mathrm{~min}^{(3)}$ |
|  | ANSI C37.90 |  | 1 kV 1 min (annunciation output) 1.5 kV 1 min (control output) |
| Functional safety <br> Functional safety of electrical/electronic/programmable electronic safety-related systems | IEC 61508, EN 61508 | SIL2 ${ }^{(1)}$ | System architecture evaluation Hardware evaluation Software evaluation |
| Certification |  |  |  |
|  | EN 50263 harmonized standard | European directiv <br> EMC European 2004 <br> ■ Low Voltage Eur December 2006 <br> - ATEX Directive | irective 2004/108/EC dated 15 December pean Directive 2006/95/EC dated 12 $/ 9 / E C^{(1)}$ |


| $\mathrm{UL}{ }_{\mathrm{c}} \mathrm{TI}_{\text {us }}$ | UL508-CSA C22.2 no. 14-95 | File E212533 |
| :--- | :--- | :--- |
| CSA | CSA C22.2 no. 14-95/no. 94-M91/no. 0.17-00 | File 210625 |

(1) Sepam must be stored in its original packaging.
(2) Except for communication: 3 kV in common mode and 1 kV in differential mode.
(3) Except for communication: 1 kVrms .
(4) See the appendix in "Installation and operation" manual SEPED303003EN, "Functional Safety" section
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Sepam G88 sensor inputs.

Sepam series 80 has analog inputs that are connected to the measurement sensors required for applications:

- main analog inputs, available on all types of Sepam series 80:
- 3 phase current inputs I1, I2, I3
- 1 residual current input 10
$\square 3$ phase voltage inputs V1, V2, V3
- 1 residual voltage input V0
- additional analog inputs, dependent on the type of Sepam:
$\square 3$ additional phase current inputs l'1, l'2, l'3
- 1 additional residual current input l'0
- 3 additional phase voltage inputs $\mathrm{V}^{\prime} 1, \mathrm{~V}^{\prime} 2$, $\mathrm{V}^{\prime} 3$
- 1 additional residual voltage input $\mathrm{V}^{\prime} 0$.

The table below lists the analog inputs available according to the type of Sepam series 80.

|  |  | $\left\lvert\, \begin{array}{l\|l} \text { S80, S81, } \\ \text { S82, S84 } \end{array}\right.$ | $\begin{aligned} & \text { T81, T82, } \\ & \text { M81, G82 } \end{aligned}$ | $\begin{aligned} & \text { T87, M87, } \\ & \text { M88, G87, } \\ & \text { G88 } \end{aligned}$ | B80 | B83 | C86 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Phase current inputs | Main channel | 11, 12, 13 | I1, I2, I3 | 11, 12, 13 | 11, 12, 13 | 11, 12, 13 | 11, 12, 13 |
|  | Additional channels |  |  | l'1, l'2, l'3 |  |  |  |
| Residual current inputs | Main channel | 10 | 10 | 10 | 10 | 10 | 10 |
|  | Additional channels | 1'0 | l'0 | l'0 | l'0 |  |  |
| Unbalance current inputs for capacitor steps |  |  |  |  |  |  | l'1, l'2, l'3, l'o |
| Phase voltage inputs | Main channel | $\begin{aligned} & \text { V1, V2, V3 } \\ & \text { or U21, U32 } \end{aligned}$ | $\begin{array}{\|l\|} \hline \text { V1, V2, V3 } \\ \text { or U21, U32 } \end{array}$ | $\begin{aligned} & \text { V1, V2, V3 } \\ & \text { or U21, U32 } \end{aligned}$ | $\begin{array}{\|l\|} \hline \text { V1, V2, V3 } \\ \text { or U21, U32 } \end{array}$ | $\begin{aligned} & \text { V1, V2, V3 } \\ & \text { or U21, U32 } \end{aligned}$ | $\begin{array}{\|l} \hline \text { V1, V2, V3 } \\ \text { or U21, U32 } \end{array}$ |
|  | Additional channels |  |  |  | V'1 or U'21 | $\begin{array}{\|l} \hline \text { V'1, V'2, V'3 } \\ \text { or U'21, U'32 } \\ \hline \end{array}$ |  |
| Residual voltage inputs | Main channel | V0 | V0 | V0 | V0 ${ }^{(1)}$ | V0 | V0 |
|  | Additional channel |  |  |  |  | V'0 |  |
| Temperature inputs (on MET148-2 module) |  |  | T1 to T16 | T1 to T16 |  |  | T1 to T16 |

Note: by extension, an additional measurement (current or voltage) is a value measured via an additional analog channel.
(1) Available with phase voltage U21, U32.

The general settings define the charactetics of the neasurement sensors connected to Sepam and determine the performance of the metering and protection functions used. They are accessec由 the SFT2841 setting software "General Characteristics", "CT-VETensors" and "Particulamharacteristics" tabs.

| General settings |  | Selection | Value |
| :---: | :---: | :---: | :---: |
| In, l'n | Rated phase current (sensor primary current) | 2 or 31 A / 5 A CTs <br> 3 LPCTs sensors | 1 A to 15 kA 25 A to $3150 \mathrm{~A}^{(1)}$ |
| l'n | Unbalance current sensor rating (capacitor application) | CT 1 A/2A/5A | 1 A to 30 A |
| Ib | Base current, according to rated power of equipment ${ }^{(2)}$ |  | 0.2 to 1.3 ln |
| l'b | Base current on additional channels (not adjustable) | Applications with transformer | l'b = lb x Un1/Un2 |
|  |  | Other applications | $\mathrm{l} \mathrm{l} \mathrm{b}=\mathrm{lb}$ |
| In0, I'n0 | Rated residual current | Sum of 3 phase currents | See In(l'n) rated phase current |
|  |  | CSH120 or CSH200 core balance CT | 2 A or 20 A rating |
|  |  | $1 \mathrm{~A} / 5 \mathrm{~A}$ CT | 1 A to 15 kA |
|  |  | Core balance CT + ACE990 (the core balance CT ratio $1 / n$ must be such that $50 n \leqslant 1500$ ) | According to current monitored and use of ACE990 |
| Unp, U'np | Rated primary phase-to-phase voltage (Vnp: rated primary phase-to-neutral voltage $\mathrm{Vnp}=\mathrm{Unp} / \sqrt{3}$ ) |  | $0 \mathrm{~A}<\ln \leq 6.25 \mathrm{kA}: 220 \mathrm{~V} \leq \mathrm{Unp} \leq 250 \mathrm{kV}$ $6.25 \mathrm{kA}<\ln \leq 15 \mathrm{kA}: 220 \mathrm{~V} \leq \mathrm{Unp} \leq 20 \mathrm{kV}$ (Idem for U'np) |
| Uns, U'ns | Rated secondary phase-to-phase voltage | 3 VTs: V1, V2, V3 | 90 to 230 V |
|  |  | 2 VTs: U21, U32 | 90 to 120 V |
|  |  | 1 VT : U21 | 90 to 120 V |
|  |  | 1 VT : V1 | 90 to 230 V |
| UnsO, U'nso | Secondary zero sequence voltage for primary zero sequence voltage Unp/ $\sqrt{3}$ |  | Uns/3 or Uns/ $\sqrt{3}$ |
| Vntp | Neutral point voltage transformer primary voltage (generator application) |  | 220 V to 250 kV |
| Vnts | Neutral point voltage transformer secondary voltage (generator application) |  | 57.7 V to 133 V |
| fn | Rated frequency |  | 50 Hz or 60 Hz |
|  | Phase rotation direction |  | 1-2-3 or 1-3-2 |
|  | Integration period (for demand current and peak demand current and power) |  | 5, 10, 15, 30, 60 min |
|  | Pulse-type accumulated energy meter | Increments active energy | 0.1 kWh to 5 MWh |
|  |  | Increments reactive energy | 0.1 kVARh to 5 MVARh |
| S | Transformer rated apparent power |  | 100 kVA to 999 MVA |
| Un1 | Rated winding 1 voltage (main channels: I) |  | 220 V to 250 kV |
| Un2 | Rated winding 2 voltage (additional channels: I') |  | 220 V to 400 kV |
| In1 | Rated winding 1 current (not adjustable) |  | In1 $=\mathrm{P} /(\sqrt{3}$ Un1) |
| In2 | Rated winding 2 current (not adjustable) |  | In2 = P/( $\sqrt{3}$ Un2) |
|  | Transformer vector shift |  | 0 to 11 |
| $\Omega$ n | Rated speed (motor, generator) |  | 100 to 3600 rpm |
| R | Number of pulses per rotation (for speed acquisition) |  | 1 to 1800 ( $\Omega \mathrm{n} \times \mathrm{R} / 60 \leqslant 1500$ ) |
|  | Zero speed set point |  | 5 to $20 \%$ of $\Omega \mathrm{n}$ |
|  | Number of capacitor steps |  | 1 to 4 |
|  | Connection of capacitor steps |  | Star / Delta |
|  | Capacitor step ratio | Step 1 | 1 |
|  |  | Step 2 | 1,2 |
|  |  | Step 3 | 1, 2, 3, 4 |
|  |  | Step 4 | 1, 2, 3, 4, 6, 8 |

(1) In values for LPCT, in Amps: 25, 50, 100, 125, 133, 200, 250, 320, 400, 500, 630, 666, 1000, 1600, 2000, 3150.
(2) Even if the value is within the range, it has to be rounded according to the setting step of 1 or 10 A (i.e.: $\mathrm{Ib}=12.2 \mathrm{~A} \rightarrow 13 \mathrm{~A}$ ).


| Functions | Measurement range | Accuracy ${ }^{(1)}$ | ｜MSA141 | Saving |
| :---: | :---: | :---: | :---: | :---: |
| Machine operating assistance |  |  |  |  |
| Thermal capacity used | $\begin{array}{\|l} 0 \text { to } 800 \% \\ (100 \% \text { for phase I = lb) } \end{array}$ | $\pm 1$ \％ | $\square$ | － |
| Remaining operating time before overload tripping | 0 to 999 min | $\pm 1$ min |  |  |
| Waiting time after overload tripping | 0 to 999 min | $\pm 1 \mathrm{~min}$ |  |  |
| Running hours counter／operating time | 0 to 65535 hours | $\pm 1 \%$ or $\pm 0.5 \mathrm{~h}$ |  | －ロ |
| Starting current | 1.2 lb to 40 ln | $\pm 5 \%$ |  | $\square$ |
| Starting time | 0 to 300 s | $\pm 300 \mathrm{~ms}$ |  | $\square$ |
| Number of starts before inhibition | 0 to 60 |  |  |  |
| Start inhibit time | 0 to 360 min | $\pm 1 \mathrm{~min}$ |  |  |
| Differential current | 0.015 to 40 ln | $\pm 1$ \％ |  |  |
| Through current | 0.015 to 40 ln | $\pm 1$ \％ |  |  |
| Phase displacement $\theta 1, \theta 2, \theta 3$（between I and I＇） | 0 to $359^{\circ}$ | $\pm{ }^{\circ}$ |  |  |
| Apparent impedance Zd，Z21，Z32，Z13 | 0 to $200 \mathrm{k} \Omega$ | $\pm 5 \%$ |  |  |
| Third harmonic neutral point voltage | 0.2 to $30 \%$ of Vnp | $\pm 1$ \％ |  |  |
| Third harmonic residual voltage | 0.2 to $90 \%$ of Vnp | $\pm 1$ \％ |  |  |
| Capacitance | 0 to 30 F | $\pm 5 \%$ |  |  |
| Capacitor unbalance current | 0.02 to 40 l ＇n | $\pm 5 \%$ |  |  |
| Switchgear diagnosis assistance |  |  |  |  |
| Cumulative breaking current | 0 to $65535 \mathrm{kA}^{2}$ | $\pm 10$ \％ |  | ㅁㅁ |
| Number of operations | 0 to $4 \times 10^{9}$ | － |  | －ロ |
| Operating time | 20 to 100 s | $\pm 1 \mathrm{~ms}$ |  | －व |
| Charging time | 1 to 20 s | $\pm 0.5 \mathrm{~s}$ |  | －ロ |
| Number of rackouts | 0 to 65535 | － |  | －ロ |
| Auxiliary supply supervision | 20 to 275 V CC | $\pm 10 \%$ or $\pm 4 \mathrm{~V}$ |  |  |

－available on MSA141 analog output module，according to setup
－ㅁ saved in the event of auxiliary supply outage，even without battery
－saved by battery in the event of auxiliary supply outage．
（1）Typical accuracy，see details on subsequent pages．


Values produced by Sepam from the signals measured.

## Measured physical values

Sepam measures the following physical values:

- phase currents (3I)
- residual current (IO)
- phase voltages (3V)
- residual voltage (V0).

Each measured signal is processed by Sepam to produce all the values necessary for the metering, diagnosis and protection functions.

The charts below indicate, for the various functions, the values produced from the signals measured, with:
■ RMS = RMS value up to the 13th harmonic

- H1 = fundamental 50 Hz or 60 Hz component
- $\Sigma \mathrm{H} 1=$ vector sum of the fundamental components of the three phases
- H3 = 3rd harmonic component
- $\Sigma \mathrm{H} 3=$ vector sum of the 3rd harmonic components of the three phases.


## Values used by the metering and diagnosis

 functions

Cumulative breaking current

- standard
$\square$ according to measurement sensors connected.

Values used by the protection functions

|  |  | 31 |  |  | 10 | 3V |  |  | V0 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Protections | ANSI code | RMS | H1 | دH1 | H1 | RMS | H1 | гH1 | гH3 | H1 | H3 |
| Phase overcurrent | 50/51 |  | $\square$ |  |  |  |  |  |  |  |  |
| Earth fault | 50N/51N |  |  | $\square$ | $\square$ |  |  |  |  |  |  |
| Sensitive earth fault | 50G/51G |  |  |  |  |  |  |  |  |  |  |
| Breaker failure | 50BF |  | ■ |  |  |  |  |  |  |  |  |
| Negative sequence / unbalance | 46 |  | $\square$ |  |  |  |  |  |  |  |  |
| Thermal overload for cables | 49RMS | ■ |  |  |  |  |  |  |  |  |  |
| Generic thermal overload | 49RMS | ■ |  |  |  |  |  |  |  |  |  |
| Thermal overload for capacitors | 49RMS | ■ |  |  |  |  |  |  |  |  |  |
| Thermal overload for motors | 49RMS | ■ |  |  |  |  |  |  |  |  |  |
| Thermal overload for transformers | 49RMS | ■ |  |  |  |  |  |  |  |  |  |
| Capacitor bank unbalance | 51C |  | ■ |  |  |  |  |  |  |  |  |
| Restricted earth fault | 64REF |  |  | ■ | ■ |  |  |  |  |  |  |
| Two-winding transformer differential | 87T |  | $\square$ |  |  |  |  |  |  |  |  |
| Machine differential | 87M |  | $\square$ |  |  |  |  |  |  |  |  |
| Directional phase overcurrent | 67 |  | ■ |  |  |  | ■ |  |  |  |  |
| Directional earth fault | 67N/67NC |  |  | $\square$ | ㅁ |  |  | $\square$ |  | ㅁ |  |
| Directional active overpower | 32P |  | ■ |  |  |  | ■ |  |  |  |  |
| Directional reactive overpower | 32Q |  | $\square$ |  |  |  | ■ |  |  |  |  |
| Directional active underpower | 37P |  | $\square$ |  |  |  | ■ |  |  |  |  |
| Phase undercurrent | 37 |  | ■ |  |  |  |  |  |  |  |  |
| Excessive starting time, locked rotor | 48/51LR |  | $\square$ |  |  |  |  |  |  |  |  |
| Starts per hour | 66 |  | $\square$ |  |  |  |  |  |  |  |  |
| Field loss (underimpedance) | 40 |  | ■ |  |  |  | ■ |  |  |  |  |
| Pole slip | 78 PS |  | $\square$ |  |  |  | $\square$ |  |  |  |  |
| Voltage-restrained overcurrent | 50V/51V |  | $\square$ |  |  |  | $\square$ |  |  |  |  |
| Underimpedance | 21B |  | $\square$ |  |  |  | $\square$ |  |  |  |  |
| Inadvertent energization | 50/27 |  | $\square$ |  |  |  | $\square$ |  |  |  |  |
| Third harmonic undervoltage / 100 \% stator earth fault | $\begin{aligned} & \text { 27TN/64G2 } \\ & \text { 64G } \end{aligned}$ |  |  |  |  |  |  |  | $\square$ |  | ■ |
| Overfluxing (V / Hz) | 24 |  |  |  |  |  | ■ |  |  |  |  |
| Positive sequence undercurrent | 27D |  |  |  |  |  | ■ |  |  |  |  |
| Remanent undervoltage | 27R |  |  |  |  |  | ■ |  |  |  |  |
| Undervoltage (L-L or L-N) | 27 |  |  |  |  |  | $\square$ |  |  |  |  |
| Overvoltage (L-L or L-N) | 59 |  |  |  |  |  | ■ |  |  |  |  |
| Neutral voltage displacement | 59N |  |  |  |  |  |  | ㅁ |  | ㅁ |  |
| Negative sequence overvoltage | 47 |  |  |  |  |  | ■ |  |  |  |  |
| Overfrequency | 81H |  |  |  |  |  | ■ |  |  |  |  |
| Underfrequency | 81L |  |  |  |  |  | ■ |  |  |  |  |
| Rate of change of frequency | 81R |  |  |  |  |  | ■ |  |  |  |  |
| a standard according to measurement sensors |  |  |  |  |  |  |  |  |  |  |  |

## Phase rotation direction



Phase rotation direction 1-2-3.


Phase rotation direction 1-3-2.

The rotation direction of the 3 phases of the network may be 1-2-3, or 1-3-2, the phase order in the trigonometric (counter-clockwise) direction.
The phase rotation direction needs to be set for correct calculation of the symmetrical components (Vd, Vi, Id, li).
The phase rotation direction directly affects:

- the direction of energy flow measured in the Sepam relay
- the sign and calculation of the powers and directional functions.


## Phase current Residual current

## Phase current

## Operation

This function gives the RMS value of the phase currents:

- 11: phase 1 current, main channels
- 12: phase 2 current, main channels
- I3: phase 3 current, main channels
- I'1: phase 1 current, additional channels

■ l'2: phase 2 current, additional channels

- I'3: phase 3 current, additional channels

It is based on RMS current measurement and takes into account harmonics up to the 13th.
Different types of sensors may be used to meter phase current

- 1 A or 5 A current transformers
- LPCT (Low Power Current Transducer) type current sensors.


## Readout

The measurements may be accessed via:

- the Sepam display via the key
$\square$ the display of a PC with the SFT2841 software
- the communication link
- an analog converter with the MSA141 option.

Characteristics

| Measurement range | 0.02 to $40 \ln ^{(1)}$ |
| :--- | :--- |
| Units | A or kA |
| Resolution | 0.1 A |
| Accuracy | $\pm 0.5 \%$ typical ${ }^{(\mathbf{2})}$ |
|  | $\pm 1 \%$ from 0.3 to 1.5 In |
|  | $\pm 2 \%$ from 0.1 to 0.3 In |
| Display format | 3 significant digits |
| Refresh interval | 1 second (typical) |
| $(1)$ In |  |

(1) In rated current set in the general settings.
(2) At In, under reference conditions (IEC 60255-6).

## Residual current

## Operation

This operation gives the RMS value of the residual current.
It is based on measurement of the fundamental component.
Four types of residual current values are available depending on the type of Sepam and sensors connected to it:
■ 2 residual currents $\operatorname{IO\Sigma }$ and $\mathrm{I}^{\prime} 0 \Sigma$, calculated by the vector sum of the 3 phase currents
■ 2 measured residual currents IO and I'0.
Different types of sensors may be used to measure residual current:

- CSH120 or CSH200 specific core balance CT
- conventional 1 A or 5 A current transformer
- any core balance CT with an ACE990 interface.


## Readout

The measurements may be accessed via:
$\square$ the Sepam display via the key

- the display of a PC with the SFT2841 software
- the communication link
- an analog converter with the MSA141 option.

| Characteristics |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Measurement range | 102 or l'os |  |  | 0.005 to $40 \ln { }^{(1)}$ |
|  | 10 or l'0 measured by CSH core balance CT | Rating | $\ln 0=2 \mathrm{~A}$ | 0.005 to $20 \mathrm{In} 0^{(1)}$ |
|  |  |  | $\mathrm{In} 0=20 \mathrm{~A}$ | 0.005 to $20 \mathrm{In} 0^{(1)}$ |
|  | 10 or l'0 measured by core balance CT with ACE990 |  |  | 0.005 to $20 \mathrm{In} 0^{(1)}$ |
|  | 10 or l'0 measured by CT |  |  | 0.005 to $20 \mathrm{InO}{ }^{(1)}$ |
| Units |  |  |  | A or kA |
| Resolution |  |  |  | 0.1 A or 1 digit |
| Accuracy ${ }^{(2)}$ |  |  |  | $\pm 1 \%$ typical at $\ln 0$ <br> $\pm 2 \%$ from 0.3 to 1.5 InO <br> $\pm 5 \%$ from 0.1 to $0.3 \ln 0$ |
| Display format |  |  |  | 3 significant digits |
| Refresh interval |  |  |  | 1 second (typical) |

(1) In, In0: nominal rating set in the general settings.
(2) Under reference conditions (IEC 60255-6), excluding sensor accuracy.

Demand current
and peak demand currents

## Operation

Demand current and peak demand currents are calculated according to the 3 phase currents I1, I2 and I3:
■ demand current is calculated over an adjustable period of 5 to 60 minutes

- peak demand current is the greatest demand current and indicates the current drawn by peak loads.
Peak demand currents may be cleared. They are saved in the event of a power failure.


## Readout

The measurements may be accessed via:

- the Sepam display via the $\left(x^{m}\right)$ key

■ the display of a PC with the SFT2841 software

- the communication link.


## Resetting to zero

- via the clear key on the Sepam display if a peak demand is displayed
- via the clear command in the SFT2841 software

■ via the communication link (remote control order TC4).
Characteristics

| Measurement range | 0.02 to $40 \ln { }^{(1)}$ |
| :--- | :--- |
| Units | A or kA |
| Resolution | 0.1 A |
| Accuracy | $\pm 0.5 \%$ typical ${ }^{(2)}$ |
|  | $\pm 1 \%$ from 0.3 to 1.5 In |
|  | $\pm 2 \%$ from 0.1 to 0.3 In |
| Display format | 3 significant digits |
| Integration period | $5,10,15,30,60$ min |

egration period 5, 10, 15, 30, 60 min
(1) In rated current set in the general settings.
(2) At In, under reference conditions (IEC 60255-6)

TS/TC equivalence for each protocol

| Modbus | DNP3 | IEC 60870-5-103 | IEC 61850 |
| :--- | :--- | :--- | :--- |
| TC | Binary Output | ASDU, FUN, INF | LN.DO.DA |
| TC4 | BO12 | - | MSTA1.RsMaxA.ctIVal |

## Operation



1-2-3 network: phase-to-neutral and phase-to-phase voltages.


1-3-2 network: phase-to-neutral and phase-to-phase voltages.

This function gives the RMS value of the fundamental 50 Hz or 60 Hz component of: ■ the main phase-to-phase voltages:

- ( $\left.\mathbf{U}_{\mathbf{2 1}} \mathbf{1}=\overrightarrow{\mathbf{V}} \mathbf{1}-\overrightarrow{\mathbf{V}} \mathbf{2}\right)$, voltage between phases 2 and 1
- ( $\overrightarrow{\mathbf{U}} \mathbf{3 2} \mathbf{=} \overrightarrow{\mathbf{V}} \mathbf{2}-\overrightarrow{\mathbf{V}} \mathbf{3})$, voltage between phases 3 and 2
- ( $\left.\overrightarrow{\mathbf{U}}_{\mathbf{1}} \mathbf{3}=\overrightarrow{\mathbf{V}} \mathbf{3}-\overrightarrow{\mathbf{V}} \mathbf{1}\right)$, voltage between phases 1 and 3 .

■ the additional phase-to-phase voltages:
$\square \vec{U}^{\prime} \mathbf{2 1}=\vec{V}^{\prime} \mathbf{1}-\overrightarrow{\mathbf{V}^{\prime}} \mathbf{2}$, voltage between phases 2 and 1
ロ $\vec{U}^{\prime} \mathbf{3 2}=\vec{V}^{\prime} \mathbf{2}-\overrightarrow{\mathbf{V}^{\prime}} \mathbf{3}$ ), voltage between phases 3 and 2
$\square \overrightarrow{\mathbf{U}}^{\prime} \mathbf{1 3}=\overrightarrow{\mathbf{V}^{\prime}} \mathbf{3}-\overrightarrow{\mathbf{V}}^{\prime} \mathbf{1}$ ), voltage between phases 1 and 3 .

## Readout

The measurements may be accessed via:

- the Sepam display via the key

■ the display of a PC with the SFT2841 software

- the communication link

■ an analog converter with the MSA141 option.

## Characteristics

| Measurement range | 0.05 to 1.2 Unp ${ }^{(1)}$ |
| :--- | :--- |
| Units | V or kV |
| Resolution | 1 V |
| Accuracy | $\pm 0.5 \%$ typical ${ }^{\left({ }^{(2)}\right.}$ main channels |
|  | $\pm 1 \%$ typical ${ }^{(2)}$ additional channels |
|  | $\pm 1 \%$ from 0.5 to 1.2 Unp |
| Display format | $\pm 2 \%$ from 0.06 to 0.5 Unp |
| Refresh interval | 3 significant digits |

(1) Un rated current set in the general settings.
(2) At Unp, under reference conditions (IEC 60255-6).

## Operation

This function gives the RMS value of the fundamental 50 Hz or 60 Hz component of: ■ the main phase-to-neutral voltages $\mathrm{V} 1, \mathrm{~V} 2, \mathrm{~V} 3$ measured on phases 1,2 and 3 ■ the additional phase-to-neutral voltages $\mathrm{V}^{\prime} 1$, $\mathrm{V}^{\prime}$ 2 and $\mathrm{V}^{\prime} 3$ measured on phases 1, 2 and 3.

## Readout

The measurements may be accessed via:

- the Sepam display via the key

■ the display of a PC with the SFT2841 software

- the communication link
- an analog converter with the MSA141 option.

Characteristics

| Measurement range | 0.05 to 1.2 Vnp ${ }^{(1)}$ |
| :--- | :--- |
| Units | V or kV |
| Resolution | 1 V |
| Accuracy | $\pm 0.5 \%$ typical (2) main channels |
|  | $\pm 1 \%$ typical ${ }^{(2)}$ additional channels |
|  | $\pm 1 \%$ from 0.5 to 1.2 Vnp |
| Display format | $\pm 2 \%$ from 0.06 to 0.5 Vnp |
| Refresh interval | 3 significant digits |

(1) Vnp: primary rated phase-to-neutral voltage (Vnp $=U n p / \sqrt{3})$.
(2) At Vnp, under reference conditions (IEC 60255-6).

## Residual voltage

## Operation

This function gives the following values:
■ main residual voltage $\overrightarrow{\mathbf{V}} \mathbf{0}=\overrightarrow{\mathbf{V}} \mathbf{1}+\overrightarrow{\mathbf{V}} \mathbf{2}+\overrightarrow{\mathbf{V}} \mathbf{3}$
■ additional residual voltage $\overrightarrow{V^{\prime}} 0=\vec{V}^{\prime} 1+\vec{V}^{\prime} \mathbf{2}+\vec{V}^{\prime} 3$
The residual voltage value may be:
■ calculated by an open star/delta VT
■ or calculated by taking the internal sum of the 3 phase voltages.
It is based on the measurement of the fundamental 50 Hz or 60 Hz component of the voltages.

## Readout

The measurements may be accessed via:

- the Sepam display via the key
$\square$ the display of a PC with the SFT2841 software
- the communication link.

Characteristics

| Measurement range | 0.015 to $3 \mathrm{Vnp}{ }^{(1)}$ |
| :--- | :--- |
| Units | V or kV |
| Resolution | 1 V |
| Accuracy | $\pm 1 \%$ from 0.5 to 3 Vnp |
|  | $\pm 2 \%$ from 0.05 to 0.5 Vnp |
| Display format | $\pm 5 \%$ from 0.02 to 0.05 Vnp |
| Refresh interval | 3 significant digits |
| (1) Vnp: primary rated phase-to-neutral voltage $($ Vnp $=$ Unp $/ \sqrt{3})$. |  |

## Neutral point voltage

## Operation

This function gives the value of the zero sequence voltage Vnt, measured at the neutral point of a generator or motor by a dedicated VT:
$\vec{V} n t=(\vec{V} 1+\vec{V} 2+\vec{V} 3) / 3$

## Readout

The measurements may be accessed via:

- the Sepam display via the $x^{(x)}$ key
$\square$ the display of a PC with the SFT2841 software
- the communication link.

Characteristics

| Measurement range | 0.015 Vnp to 3 Vntp ${ }^{(1)}$ |
| :--- | :--- |
| Units | V or kV |
| Resolution | 1 V |
| Accuracy | $\pm 1 \%$ from 0.5 to 3 Vntp |
|  | $\pm 2 \%$ from 0.05 to 0.5 Vntp |
|  | $\pm 5 \%$ from 0.02 to 0.05 Vntp |
| Display format | 3 significant digits |
| Refresh interval | 1 second (typical) |

(1) Vntp: neutral point voltage transformer primary voltage.

## Operation

This function calculates the value of the main positive sequence voltage Vd :

- from the 3 main phase-to-neutral voltages:
- phase rotation direction 1-2-3: $\overrightarrow{\mathbf{V}} \mathbf{d}=\frac{1}{3} \times\left(\overrightarrow{\mathbf{V}} 1+a \vec{V} \mathbf{2}+\mathrm{a}^{2} \overrightarrow{\mathbf{V}} \mathbf{3}\right)$
$\square$ phase rotation direction 1-3-2: $\overrightarrow{\mathbf{V}} \mathbf{d}=\frac{\mathbf{1}}{\mathbf{3}} \times\left(\overrightarrow{\mathbf{V}} 1+\mathrm{a}^{2} \overrightarrow{\mathbf{V}} 2+\mathrm{a} \overrightarrow{\mathbf{V}} 3\right)$
■ or from the 2 main phase-to-phase voltages:
- phase rotation direction 1-2-3: $\overrightarrow{\mathbf{V}} \mathbf{d}=\frac{1}{3} \times\left(\overrightarrow{\mathbf{U}} 21-\mathbf{a}^{2} \overrightarrow{\mathbf{U}} 32\right)$
- phase rotation direction 1-3-2: $\vec{V} \mathbf{d}=\frac{1}{3} \times(\overrightarrow{\mathbf{U}} 21-\mathrm{a} \mathbf{U} 32)$
with $a=e^{j \frac{2 \pi}{3}}$
The additional positive sequence voltage V'd is calculated in the same way:
■ from the 3 additional phase-to-neutral voltages $\mathrm{V}^{\prime} 1, \mathrm{~V}^{\prime} 2$ and $\mathrm{V}^{\prime} 3$
■ or from the 2 additional phase-to-phase voltages U'21 and U'32.


## Readout

The measurements may be accessed via:

- the Sepam display via the $x+x$ key

■ the display of a PC with the SFT2841 software

- the communication link.


## Characteristics

| Measurement range | 0.05 to 1.2 Vnp $^{(1)}$ |
| :--- | :--- |
| Units | V or kV |
| Resolution | 1 V |
| Accuracy | $\pm 2 \%$ at Vnp |
| Display format | 3 significant digits |
| Refresh interval | 1 second (typical) |
| (1) Vnp: praty rated phase |  |

(1) Vnp: primary rated phase-to-neutral voltage (Vnp $=$ Unp/ $\sqrt{3}$ ).

## Operation

This function calculates the value of the main negative sequence voltage Vi: - from the 3 main phase-to-neutral voltages:
$\square$ phase rotation direction 1-2-3: $\overrightarrow{\mathbf{V}} \mathbf{i}=\frac{\mathbf{1}}{\mathbf{3}} \times\left(\overrightarrow{\mathbf{V}} \mathbf{1}+\mathrm{a}^{2} \overrightarrow{\mathbf{V}} \mathbf{2}+\mathrm{a} \overrightarrow{\mathbf{V}} \mathbf{3}\right)$
$\square$ phase rotation direction 1-3-2: $\overrightarrow{\mathbf{V}} \mathbf{i}=\frac{\mathbf{1}}{\mathbf{3}} \times\left(\overrightarrow{\mathbf{V}} \mathbf{1}+\mathrm{a} \overrightarrow{\mathbf{V}} \mathbf{2}+\mathbf{a}^{2} \overrightarrow{\mathbf{V}} \mathbf{3}\right)$
■ or from the 2 main phase-to-phase voltages:
ㅁ phase rotation direction 1-2-3: $\overrightarrow{\mathbf{V}} \mathbf{i}=\frac{\mathbf{1}}{\mathbf{3}} \times(\overrightarrow{\mathbf{U}} 21-\mathbf{a} \overrightarrow{\mathbf{U}} 32)$
$\square$ phase rotation direction 1-3-2: $\overrightarrow{\mathbf{V}} \mathbf{i}=\frac{\mathbf{1}}{\mathbf{3}} \times\left(\overrightarrow{\mathbf{U}} 21-\mathbf{a}^{2} \overrightarrow{\mathbf{U}} 32\right)$
with $a=e^{j \frac{2 \pi}{3}}$
The additional negative sequence voltage $V^{\prime} i$ is calculated in the same way: - from the 3 additional phase-to-neutral voltages $\mathrm{V}^{\prime} 1, \mathrm{~V}^{\prime} 2$ and $\mathrm{V}^{\prime} 3$

■ or from the 2 additional phase-to-phase voltages U'21 and U'32.

## Readout

The measurements may be accessed via:

- the Sepam display via the key
- the display of a PC with the SFT2841 software

■ the communication link.

## Characteristics

| Measurement range | 0.05 to 1.2 Vnp ${ }^{(1)}$ |
| :--- | :--- |
| Units | V or kV |
| Resolution | 1 V |
| Accuracy | $\pm 2 \%$ at Vnp |
| Display format | 3 significant digits |
| Refresh interval | 1 second (typical) |
| (1) Vnp: primary rated phase-to-neutral voltage $($ Vnp $=$ Unp $/ \sqrt{3})$. |  |

## Operation

This function gives the frequency value.
Frequency is measured via the following
■ based on U21 or V1, if only one phase-to-phase voltage is connected to the Sepam

- based on positive sequence voltage in other cases.

Frequency is not measured if:

- the voltage U21 (or V1) or positive sequence voltage Vd is less than $40 \%$ of Un ■ the frequency $f$ is outside the measurment range.
The measurement of the frequency $f^{\prime}$ is calculated according to the same principle, from V'd or U'21 or V'1


## Readout

The measurements may be accessed via:

- the Sepam display via the $\times x$ key

■ the display of a PC with the SFT2841 software

- the communication link

■ an analog converter with the MSA141 option.

## Characteristics

| Main channels | $50 \mathrm{~Hz}, 60 \mathrm{~Hz}$ |
| :--- | :--- |
| Rated frequency | 25 to 65 Hz |
| Range | $0.01 \mathrm{~Hz}{ }^{(1)}$ |
| Resolution | $\pm 0.01 \mathrm{~Hz}$ |
| Accuracy ${ }^{(2)}$ | 3 significant digits |
| Display format | 1 second (typical) |
| Refresh interval | $50 \mathrm{~Hz}, 60 \mathrm{~Hz}$ |
| Additional channels | 45 to $55 \mathrm{~Hz} \mathrm{(fn=50} \mathrm{Hz)}$ |
| Rated frequency fn | 55 to $65 \mathrm{~Hz} \mathrm{(fn}=60 \mathrm{~Hz})$ |
| Range | 0.01 Hz |
| Resolution ${ }^{(1)}$ | $\pm 0.05 \mathrm{~Hz}$ |
| Accuracy ${ }^{(2)}$ | 3 significant digits |
| Display format | 1 second (typical) |
| Refresh interval |  |
| (1) On SFT2841. |  |
| (2) At Unp, under reference conditions (IEC 60255-6). |  |

## Operation

Power values are calculated from the phase currents I1, I2 and I3:
■ active power $=\sqrt{3} . U . I \cos \varphi$
■ reactive power $=\sqrt{3}$.U.I. $\sin \varphi$
■ apparent power $=\sqrt{3}$.U.I.
According to the sensors used, power calculations may be based on the 2 or 3 wattmeter method (see table below).
The 2 wattmeter method is only accurate when there is no residual current, but it is not applicable if the neutral is distributed.
The 3 wattmeter method gives an accurate calculation of 3-phase and phase by phase powers in all cases, regardless of whether or not the neutral is distributed.

| Connection of voltage channels | Connection of main current channels | P, Q, S calculation method | Power per phase P1, P2, P3 <br> Q1, Q2, Q3 <br> S1, S2, S3 |
| :---: | :---: | :---: | :---: |
| 3 V | I1, I2, I3 | 3 wattmeters | Available |
|  | 11, 13 | 2 wattmeters | Not available |
| U32, U21 + V0 | I1, I2, I3 | 3 wattmeters | Available |
|  | 11, I3 | 2 wattmeters | Not available |
| U32, U21 without V0 | 11, I2, I3 or I1, I3 | 2 wattmeters | Not available |
| U21 | I1, I2, I3 or I1, I3 | 2 wattmeters <br> The system voltage is considered to be balanced | Not available |
| V1 | I1, I2, I3 or I1, I3 | No calculation | P1, Q1, S1 only |

## Power calculation

- by 3 wattmeter method:
$P=\vec{V} 1 \overrightarrow{1} \cos (\vec{V} 1, \overrightarrow{1})+\vec{V} 2 \overrightarrow{12} \cos (\vec{V} 2, \overrightarrow{12})+\vec{V} 3 \vec{l} \overrightarrow{3} \cos (\vec{V} 3, \overrightarrow{3})$
$Q=\vec{V} 1 \overrightarrow{1} 1 \sin (\vec{V} 1, \overrightarrow{1})+\vec{V} 2 \vec{l} \mathbf{2} \sin (\vec{V} 2, \overrightarrow{2})+\vec{V} 3 \vec{l} \sin (\vec{V} 3, \overrightarrow{3})$
- by 2 wattmeter method:
$P=\vec{U} 21 \overrightarrow{1} \cos (\vec{U} 21, \overrightarrow{1})-\vec{U} 32 \vec{I} \overrightarrow{3} \cos (\vec{U} 32, \overrightarrow{3})$
$Q=\vec{U} 21 \overrightarrow{11} \sin (\vec{U} 21, \overrightarrow{1} \mathbf{1})-\vec{U} 322 \vec{l} \sin (\vec{U} 32, \overrightarrow{3})$
- $S=\sqrt{P^{2}+Q^{2}}$.

According to standard practice, it is considered that:
■ for the outgoing circuit ${ }^{(1)}$ :
$\square$ power supplied by the busbars is positive
$\square$ power supplied to the busbars is negative


- for the incoming circuit ${ }^{(1)}$ :
$\square$ power supplied to the busbars is positive
$\square$ power supplied by the busbars is negative.

(1) Choice to be set in the general settings.


## Active, reactive and apparent power

## Readout

The measurements may be accessed via:

- the Sepam display via the $\mathrm{N}^{1 \times 2}$ key
- the display of a PC with the SFT2841 software
- the communication link

■ an analog converter with the MSA141 option.

## Characteristics

|  | Active power P, P1, P2, P3 | Reactive power Q, Q1, Q2, Q3 | Apparent power S, S1, S2, S3 |
| :---: | :---: | :---: | :---: |
| Measurement range | $\pm(0.8 \% \mathrm{Sn} \text { at } 999 \mathrm{MW})^{(1)}$ | $\pm\left(0.8\right.$ \% Sn at 999 Mvar) ${ }^{(1)}$ | 0.8 \% Sn at 999 MVA ${ }^{(1)}$ |
| Units | kW, MW | kvar, Mvar | kVA, MVA |
| Resolution | 0.1 kW | 0.1 kvar | 0.1 kVA |
| Accuracy | $\begin{aligned} & \pm 1 \% \text { from } 0.3 \text { to } 1.5 \mathrm{Sn}^{(2)} \\ & \pm 3 \% \text { from } 0.1 \text { to } 0.3 \mathrm{Sn}^{(2)} \end{aligned}$ | $\begin{aligned} & \pm 1 \% \text { from } 0.3 \text { to } 1.5 \mathrm{Sn}^{(3)} \\ & \pm 3 \% \text { from } 0.1 \text { to } 0.3 \mathrm{Sn}^{(3)} \end{aligned}$ | $\begin{aligned} & \pm 1 \% \text { from } 0.3 \text { to } 1.5 \mathrm{Sn} \\ & \pm 3 \% \text { from } 0.1 \text { to } 0.3 \mathrm{Sn} \end{aligned}$ |
| Display format | 3 significant digits | 3 significant digits | 3 significant digits |
| Refresh interval | 1 second (typical) | 1 second (typical) | 1 second (typical) |

(1) $\operatorname{sn} \sqrt{3}$ Inpin.
(1) $S n=\sqrt{3}$ Unp.In.
(2) In, Unp, $\operatorname{Cos} \varphi>0.8$ under reference conditions (IEC 60255-6).
(3) In, Unp, $\operatorname{Cos} \varphi<0.6$ under reference conditions (IEC 60255-6).

## Peak demand active and reactive power

## Operation

This function gives the greatest demand active or reactive power value since the last reset.
The values are refreshed after each "integration interval", an interval that may be set from 5 to 60 min (common interval with peak demand phase currents). The values are saved in the event of a power failure.

## Readout

The measurements may be accessed via:

- the Sepam display via the key
- the display of a PC with the SFT2841 software
- the communication link.


## Resetting to zero

■ via the clear key on the Sepam display if a peak demand is displayed
■ via the clear command in the SFT2841 software
■ via the communication link (remote control order TC5).

## Characteristics

|  | Demand active power | Demand reactive power |
| :--- | :--- | :--- |
| Measurement range | $\pm(1.5 \% \mathrm{Sn} \text { at } 999 \mathrm{MW})^{(1)}$ | $\pm(1.5 \% \mathrm{Sn} \text { at } 999 \mathrm{Mvar})^{(1)}$ |
| Units | $\mathrm{kW}, \mathrm{MW}$ | $\mathrm{kvar}, \mathrm{Mvar}$ |
| Resolution | 0.1 kW | 0.1 kvar |
| Accuracy | $\pm 1 \%$, typical ${ }^{(2)}$ | $\pm 1 \%$ typical ${ }^{(3)}$ |
| Display format | 3 significant digits | 3 significant digits |
| Integration period | $5,10,15,30,60 \mathrm{~min}$ | $5,10,15,30,60 \mathrm{~min}$ |

(1) $S n=\sqrt{3}$ Unp.In.
(2) At In, Unp, $\cos \varphi>0.8$ under reference conditions (IEC 60255-6).
(3) At In, Unp, $\cos \varphi<0.6$ under reference conditions (IEC 60255-6).

TS/TC equivalence for each protocol

| Modbus | DNP3 | IEC 60870-5-103 | IEC 61850 |
| :--- | :--- | :--- | :--- |
| TC | Binary Output | ASDU, FUN, INF | LN.DO.DA |
| TC5 | BO14 | - | MSTA1.RsMaxPwr.ctIVal |




CEI Convention.

## Power factor $(\cos \varphi)$

## Operation

The power factor is defined by: $\boldsymbol{\operatorname { c o s }} \varphi=\mathbf{P} / \sqrt{\mathbf{P}^{\mathbf{2}}+\mathbf{Q}^{\mathbf{2}}}$.
It expresses the phase displacement between the phase currents and phase-toneutral voltages.
The + and - signs and IND (inductive) and CAP (capacitive) indications give the direction of power flow and the type of load.

## Readout

The measurements may be accessed via:

- the Sepam display via the key
- the display of a PC with the SFT2841 software
- the communication link.


## Characteristics

| Measurement range | -1 at 1 IND/CAP |
| :--- | :--- |
| Resolution | 0.01 |
| Accuracy ${ }^{(1)}$ | 0.01 typical |
| Display format | 3 significant digits |
| Refresh interval | 1 second (typical) |
| (1) At In, Unp, $\cos \varphi>0.8$ under reference conditions $($ IEC $60255-6)$. |  |

## Accumulated active and reactive energy

## Operation

This function gives the following for the active and reactive energy values, calculated according to voltages and phase currents I1, I2 and I3:
■ accumulated energy conveyed in one direction

- accumulated energy conveyed in the other direction.

It is based on measurement of the fundamental component.
The accumulated energy values are saved in the event of a power failure.

## Readout

The measurements may be accessed via:

- the Sepam display via the key

■ the display of a PC with the SFT2841 software

- the communication link.


## Characteristics

|  | Active energy | Reactive energy |
| :--- | :--- | :--- |
| Metering capacity | 0 to $2.110^{8} \mathrm{MW.h}$ | 0 to $2.110^{8}$ Mvar.h |
| Units | MW.h | Mvar.h |
| Resolution | 0.1 MW.h | 0.1 Mvar.h |
| Accuracy | $\pm 1$ \% typical ${ }^{(1)}$ | $\pm 1$ \% typical ${ }^{(1)}$ |
| Display format | 10 significant digits | 10 significant digits |
| (1) At In, Unp, $\cos \varphi>0.8$ under reference conditions (IEC $60255-6)$. |  |  |

## Accumulated active and reactive energy by pulse metering

## Operation

This function is used for energy metering via logic inputs. Energy incrementing is associated with each input (one of the general parameters to be set). Each input pulse increments the meter. 4 inputs and 4 accumulated energy metering options are available:

- positive and negative active energy
- positive and negative reactive energy.

The accumulated active and reactive energy values are saved in the event of a power failure.

## Readout

■ the display of a PC with the SFT2841 software

- the communication link.


## Characteristics

|  | Active energy | Reactive energy |
| :--- | :--- | :--- |
| Metering capacity | 0 to $2.110^{8} \mathrm{MW} . \mathrm{h}$ | 0 to $2.110^{8}$ Mvar.h |
| Units | MW.h | Mvar.h |
| Resolution | $0.1 \mathrm{MW} . \mathrm{h}$ | 0.1 Mvar.h |
| Display format | 10 significant digits | 10 significant digits |
| Increment | $0.1 \mathrm{~kW} . \mathrm{h}$ to 5 MW | $0.1 \mathrm{kvar.h} \mathrm{to} 5 \mathrm{Mvar} . \mathrm{h}$ |
| Pulse | 15 ms min. | 15 ms min. |

## Operation

This function gives the temperature value measured by resistance temperature detectors (RTDs):
■ platinum Pt100 ( $100 \Omega$ at $0^{\circ} \mathrm{C}$ or $32{ }^{\circ} \mathrm{F}$ ) in accordance with the IEC 60751 and DIN 43760 standards
■ nickel $100 \Omega$ or $120 \Omega\left(\right.$ at $0^{\circ} \mathrm{C}$ or $32^{\circ} \mathrm{F}$ ).
Each RTD channel gives one measurement:
tx = RTD $x$ temperature.
The function also indicates RTD faults:

- RTD disconnected ( $\mathrm{t}>205^{\circ} \mathrm{C}$ or $\mathrm{t}>401^{\circ} \mathrm{F}$ )
- RTD shorted ( $\mathrm{t}<-35^{\circ} \mathrm{C}$ or $\mathrm{t}<-31^{\circ} \mathrm{F}$ ).

In the event of a fault, display of the value is inhibited.
The associated monitoring function generates a maintenance alarm.

## Readout

The measurements may be accessed via:

- the Sepam display via the key, in ${ }^{\circ} \mathrm{C}$ or ${ }^{\circ} \mathrm{F}$

■ the display of a PC with the SFT2841 software

- the communication link
- an analog converter with the MSA141 option.


## Characteristics

| Range | $-30^{\circ} \mathrm{C}$ to $+200^{\circ} \mathrm{C}$ | $-22^{\circ} \mathrm{F}$ to $+392^{\circ} \mathrm{F}$ |
| :--- | :--- | :--- |
| Resolution | $1{ }^{\circ} \mathrm{C}$ | $1{ }^{\circ} \mathrm{F}$ |
| Accuracy | $\pm 1^{\circ} \mathrm{C}$ from $+20{ }^{\circ} \mathrm{C}$ to $+140^{\circ} \mathrm{C}$ | $\pm 1.8^{\circ} \mathrm{F}$ from $+68^{\circ} \mathrm{F}$ to $+284^{\circ} \mathrm{F}$ |
|  | $\pm 2{ }^{\circ} \mathrm{C}$ from $-30^{\circ} \mathrm{C}$ to $+20^{\circ} \mathrm{C}$ | $\pm 3.6^{\circ} \mathrm{F}$ from $-22^{\circ} \mathrm{F}$ to $+68{ }^{\circ} \mathrm{F}$ |
|  | $\pm 2^{\circ} \mathrm{C}$ from $+140^{\circ} \mathrm{C}$ to $+200^{\circ} \mathrm{C}$ | $\pm 3.6^{\circ} \mathrm{F}$ from $+284^{\circ} \mathrm{F}$ to $+392^{\circ} \mathrm{F}$ |
| Refresh interval | 5 seconds (typical) |  |

## Accuracy derating according to wiring

$\square$ connection in 3-wire mode: the error $\Delta t$ is proportional to the length of the connector and inversely proportional to the connector cross-section:
$\Delta t\left({ }^{\circ} \mathbf{C}\right)=\mathbf{2} \times \frac{\mathbf{I}\left(\mathbf{k m}^{2}\right)}{\mathbf{S}\left(\mathbf{m m}^{2}\right)}$
$\square \pm 2.1^{\circ} \mathrm{C} / \mathrm{km}$ for a cross-section of $0.93 \mathrm{~mm}^{2}$ (AWG 18)
ㅁ $\pm 1^{\circ} \mathrm{C} / \mathrm{km}$ for a cross-section of $1.92 \mathrm{~mm}^{2}$ (AWG 14).

## Operation

This function gives the rotation speed of a motor or generator rotor. It is calculated by measurement of the time between two pulses transmitted by a proximity sensor at each passage of a cam driven by the rotation of the motor or generator shaft. The number of pulses per rotation is set in the "particular characteristics" screen of the SFT2841 software. The proximity sensor is connected to logic input I104.


1 Rotor with 2 cams.
2 Proximity sensor.

## Readout

The measurements may be accessed via:

- the display of a PC with the SFT2841 software
- the communication link.


## Characteristics

| Range |  | 0 to 7200 rpm |
| :---: | :---: | :---: |
| Resolution |  | 1 rpm |
| Accuracy |  | $\pm 1 \mathrm{rpm}$ |
| Refresh interval |  | 1 second (typical) |
| Pulses per rotation (R) |  | 1 to 1800 with $\Omega$ R $\mathrm{R} / 60 \leqslant 1500$ ( $\Omega$ : rated speed in rpm) |
| Proximity sensor | Pass-band (in Hz) | > 2. $\mathrm{Sn}_{\text {R R/60 }}$ |
|  | Output | 24 to 250 V DC, 3 mA minimum |
|  | Leakage current in open status | $<0.5 \mathrm{~mA}$ |
|  | Voltage dip in closed status < 4 V (with 24 V DC power supply) |  |
|  | Pulse duration | 0 status $>120 \mu \mathrm{~s}$ |
|  |  | 1 status $>200 \mu \mathrm{~s}$ |

## Operation

This function displays a phasor diagram of the fundamental component of the current and voltage measurements as acquired by Sepam without any correction. It provides effective assistance in the checking of cables and the implementation of directional and differential protection functions.
It is fully parameterizable and the following choices are proposed to adapt the phasor diagram according to requirements:

- choice of measurements to be displayed in the phasor diagram

■ choice of reference phasor

- choice of display mode.


## Measurements to be displayed

- phase currents on main and additional channel
- residual currents measured or with sum on main and additional channels

■ symmetrical components of current Id, Ii, IO $0 / 3$
■ phase-to-neutral voltages on main and additional channels

- phase-to-phase voltages on main and additional channels
- residual voltages on main and additional channels

■ symmetrical components of voltage Vd , $\mathrm{Vi}, \mathrm{V} 0 / 3$.

## Reference phasor

The reference phasor according to which the phase shifts of the other phasors displayed are calculated may be chosen from the phase or residual current or voltage phasors. When the reference phasor is too small (<2 \% In for currents or 5 \% Un for voltages), display is impossible.


Phasor diagram on SFT2841

## Display mode

■ Display as true values: the measurements are displayed without any modification in a scale chosen in relation to the respective rated values:
$\square 0$ to 2 Max (In, I'n) for currents

- 0 to 2 Max (Unp, U'np) for voltages.

■ Display as values normalized in relation to the maximum, i.e. the measurements are normalized in relation to the greatest measurement of the same type. The greatest measurement is displayed full scale with a modulus equal to 1 , and the others are displayed as relative values compared to the modulus 1 value. This display provides maximum angular resolution, regardless of the measured values, while maintaining the relative values between measurements.
■ Display as values normalized to 1: all the measurements are normalized in relation to themselves and displayed with a modulus of 1 , equal to full scale. This mode provides optimal display of the angles between phasors but does not allow moduli to be compared.
■ Display of phase-to-phase voltage values in a triangle arrangement: for a more common display of phase-to-phase voltage phasors.
■ Display / elimination of the scale: for more convenient reading of the displayed phasors.

## Readout

All of the possibilities described above may be accessed via the SFT2841 setting and operating software.
Two predefined displays are available on the mimic-based UMI:
■ display of the three phase currents and three phase-to-neutral voltages of the main channels

- display of the three phase currents of the main channels and the three phase currents of the additional channels


## Characteristics

Diagram display options of an SFT2841 phasor diagram
Measurements to be displayed
Multiple selection from
Reference phasor
Single choice from:
I1, I2, I3, IO, IOE, Id, Ii, IOE/3, I'1, I'2, I'3, I'0, I'OL
V1, V2, V3, V0, U21, U32玉, U13, Vd, Vi, V0/3
V'1, V'2, V'3, V'0, U'21, U'32, U'13

I1, I2, I3, IO, IOL, I'0, I'OL
V1, V2, V3, V0, U21, U32, U13
V'1, V'2, V'3, V'0, U'21, U'32, U'13
Display mode
true (true value)
/ max (value normalized in relation to maximum)
$=1$ (normalized to 1 )
Voltage display
true (true value)
/ max (value normalized in relation to maximum)
$=1$ (normalized to 1 )
Phase-to-phase voltage star/delta

Display of scale

## Tripping context

## Operation

This function gives the values at the time of tripping (activation of the tripping contact on output O1) to enable analysis of the cause of the fault.
Values available on the Sepam display:
■ tripping currents TRIPI et TRIPI'

- residual currents 10,1 'O, $10 \Sigma$ and $I^{\prime} O \Sigma$
- differential and through currents
- phase-to-phase voltages

■ residual voltage
■ neutral point voltage

- third harmonic neutral point or residual voltage
- frequency
- active power
- reactive power
- apparent power.

■ phase rotation direction 1-2-3/1-3-2
In addition to the values available on the Sepam display, the following values are available with the SFT2841 software:
■ phase-to-neutral voltages

- negative sequence voltage

■ positive sequence voltage.
The values for the last five trips are stored with the date and time of tripping.
They are saved in the event of a power failure.
Once 5 tripping contexts have been stored, the following new tripping value overwrites the oldest tripping context in the memory.

## Readout

The measurements may be accessed via:

- the Sepam display via the
- the display of a PC with the SFT2841 software
- the communication link.


Tripping current (TRIPI1) acquisition.

## Tripping current

## Operation

This function gives the RMS value of currents at the prospective time of the last trip:

- TRIPI1: phase 1 current (main channels)
- TRIPI2: phase 2 current (main channels)
- TRIPI3: phase 3 current (main channels)
- TRIPI'1: phase 1 current (additional channels)
- TRIPI'2: phase 2 current (additional channels)
- TRIPI'3: phase 3 current (additional channels).

It is based on measurement of the fundamental component.
This measurement is defined as the maximum RMS value measured during a 30 ms interval after the activation of the tripping contact on output O 1.

## Readout

The measurements may be accessed via:

- the Sepam display via the key
- the display of a PC with the SFT2841 software
- the communication link.


## Characteristics

| Measurement range | 0.1 to $40 \ln { }^{(1)}$ |
| :--- | :--- |
| Units | A or kA |
| Resolution | 0.1 A |
| Accuracy | $\pm 5 \% \pm 1$ digit |
| Display format | 3 significant digits |
| (1) In, rated current set in the general settings. |  |

## Number of phase fault trips

## Operation

This function counts the network phase faults that have caused circuit breaker tripping.
It counts only trips triggered by protection functions $50 / 51,50 \mathrm{~V} / 51 \mathrm{~V}$ and 67 when the circuit breaker is closed.
If there is discrimination between several circuit breakers, the fault is only counted by the Sepam that issues the trip order.
Transient faults cleared by the recloser are counted.
The number of phase fault trips is saved in the event of an auxiliary power failure. It may be reinitialized using the SFT2841 software.

## Readout

The measurements may be accessed via:

- the Sepam display via the key
- the display of a PC with the SFT2841 software
- the communication link.


## Characteristics

| Measurement range | 0 to 65535 |
| :--- | :--- |
| Units | None |
| Resolution | 1 |
| Refresh interval | 1 second (typical) |

## Number of earth fault trips

## Operation

This function counts earth faults on the network that have caused circuit breaker tripping.
It counts only trips triggered by protection functions $50 \mathrm{~N} / 51 \mathrm{~N}$ and 67 N when the circuit breaker is closed.
If there is discrimination between several circuit breakers, the fault is only counted by the Sepam that issues the trip order.
Transient faults cleared by the recloser are counted.
The number of earth fault trips is saved in the event of an auxiliary power failure. It may be reinitialized using the SFT2841 software.

## Readout

The measurements may be accessed via:

- the Sepam display via the key

■ the display of a PC with the SFT2841 software

- the communication link.

Characteristics

| Measurement range | 0 to 65535 |
| :--- | :--- |
| Units | None |
| Resolution | 1 |
| Refresh interval | 1 second (typical) |

## Operation

This function gives the negative sequence component: $\mathbf{T}=\mathbf{l} \mathbf{i} / \mathbf{l} \mathbf{b}$ or $\mathbf{T}^{\prime}=\mathbf{l}^{\prime} \mathbf{i} / \mathbf{l}^{\prime} \mathbf{b}$. The negative sequence current is determined based on the phase currents:
$\square 3$ phases:
$\square$ phase rotation direction $1-2-3: \overrightarrow{\mathbf{i}}=\frac{\mathbf{1}}{\mathbf{3}} \times\left(\overrightarrow{\mathbf{1}}+a^{2} \overrightarrow{\mid 2}+a \overrightarrow{\mathbf{3}}\right)$
$\square$ phase rotation direction $1-3-2: \overrightarrow{\mathbf{I}}=\frac{1}{3} \times\left(\overrightarrow{\mathbf{1}}+a \overrightarrow{\mathrm{I}} \mathbf{X}+\mathrm{a}^{2} \overrightarrow{\mathbf{I} 3}\right)$
$\square 2$ phases:
$\square$ phase rotation direction 1-2-3: $|\overrightarrow{\mathbf{I}}|=\frac{\mathbf{1}}{\sqrt{\mathbf{3}}} \times\left|\overrightarrow{\mathbf{I} \mathbf{1}}-\mathbf{a}^{2} \overrightarrow{\mathbf{I} \mathbf{3}}\right|$
$\square$ phase rotation direction 1-3-2: $|\overrightarrow{\mathbf{I} \mathbf{i}}|=\frac{\mathbf{1}}{\sqrt{3}} \times|\overrightarrow{\mathbf{l} 1}-\mathbf{a} \overrightarrow{\mathbf{3}}|$
with $a=e^{j \frac{2 \pi}{3}}$
When there are no earth faults, the formulas for 2 phase currents are equivalent to those for 3 phase currents.

## Readout

The measurements may be accessed via:

- the Sepam display via the key

■ the display of a PC with the SFT2841 software

- the communication link.


## Characteristics

| Measurement range | 10 to $500 \%$ |
| :--- | :--- |
| Units | $\% \mathrm{lb}$ or $\%$ l'b |
| Resolution | $1 \%$ |
| Accuracy | $\pm 2 \%$ |
| Display format | 3 significant digits |
| Refresh interval | 1 second (typical) |

## Current total harmonic distortion

## Operation

Current total harmonic distortion Ithd may be used to assess the quality of the current. It is calculated based on phase I1, taking into account harmonics up to the 13th.

Ithd is calculated over 50 periods using the following formula:
Ithd $=100 \% \sqrt{\left(\frac{\mathrm{RMS}}{\mathrm{H} 1}\right)^{2}-1}$
with:
RMS = RMS value of current I1 up to the 13th harmonic
H1 = value of the fundamental of current I1
Readout
The measurements may be accessed via:
$\square$ the Sepam display via the key
■ the display of a PC with the SFT2841 software

- the communication link.


## Characteristics

| Measurement range | 0 to $100 \%$ |
| :--- | :--- |
| Units | $\%$ |
| Resolution | $0.1 \%$ |
| Accuracy ${ }^{(1)}$ | $\pm 1 \%$ at In for Ithd $>2 \%$ |
| Display format | 3 significant digits |
| Refresh interval | 1 second (typical) |
| (1) Under reference conditions (IEC 60255-6). |  |

(1) Under reference conditions (IEC 60255-6).

## Voltage total harmonic distortion

## Operation

Voltage total harmonic distortion Uthd may be used to assess the quality of the voltage. It is calculated based on the measurement of U21 or V1 according to the configuration, taking into account harmonics up to the 13th.

Uthd is calculated over 50 periods using the following formula:
Uthd $=100 \% \sqrt{\left(\frac{\text { RMS }}{\mathrm{H} 1}\right)^{2}-1}$
with:
RMS = RMS value of voltage U21 or V1 up to the 13th harmonic
H1 = value of the fundamental of voltage U21 or V1

## Readout

The measurements may be accessed via:

- the Sepam display via the key

■ the display of a PC with the SFT2841 software

- the communication link.


## Characteristics

| Measurement range | 0 to $100 \%$ |
| :--- | :--- |
| Units | $\%$ |
| Resolution | $0.1 \%$ |
| Accuracy ${ }^{(1)}$ | $\pm 1 \%$ at Un or Vn for Uthd $>2 \%$ |
| Display format | 3 significant digits |
| Refresh interval | 1 second (typical) |

(1) Under reference conditions (IEC 60255-6).


Phase displacement $\varphi 1$.

## Phase displacement $\varphi 0, \varphi^{\prime} 0, \varphi 0 \Sigma$

## Operation

This function gives the phase displacement measured between the residual voltage and residual current in the trigonometric (counter-clockwise) direction (see diagram). The measurement is useful during commissioning to check that the directional earth fault protection unit is connected correctly.
Three values are available:

- $\varphi 0$, angle between VO and measured IO
- $\varphi$ '0, angle between V0 and measured l'0
- $\varphi 0 \Sigma$, angle between V 0 and $10 \Sigma$ calculated as the sum of the phase currents.


## Readout

The measurements may be accessed via:

- the Sepam display via the key

■ the display of a PC with the SFT2841 software

- the communication link.


## Characteristics

| Measurement range | 0 to $359^{\circ}$ |
| :--- | :--- |
| Resolution | $1^{\circ}$ |
| Accuracy | $\pm 2^{\circ}$ |
| Refresh interval | 2 seconds (typical) |

## Phase displacement $\varphi 1, \varphi 2, \varphi 3$

## Operation

This function gives the phase displacement between the V1, V2, V3 voltages and I1, I2, I3 currents respectively, in the trigonometric (counter-clockwise) direction (see diagram).
The measurements are used when Sepam is commissioned to check that the voltage and current inputs are wired correctly. When the phase-to-phase voltages U21 and U32 are connected to Sepam and there is no measurement of residual voltage V0, the residual voltage is presumed to be zero. The function does not operate when only the voltage U21 or V1 is connected to Sepam.
This function takes into account the convention regarding the direction of flow of energy in the outgoing and incoming circuits (see "Power measurements"). Therefore, the angles $\varphi 1, \varphi 2$ and $\varphi 3$ are adjusted by $180^{\circ}$ with respect to the values acquired by Sepam for the incoming circuits.

## Readout

The measurements may be accessed via:

- the Sepam display via the key
- the display of a PC with the SFT2841 software
- the communication link.


## Characteristics

| Measurement range | 0 to $359^{\circ}$ |
| :--- | :--- |
| Resolution | $1^{\circ}$ |
| Accuracy | $\pm 2^{\circ}$ |
| Refresh interval | 2 seconds (typical) |

## Operation

This function is used to record analog signals and logical states.
The storage of recordings is activated by one or more events set using the SFT2841 software.
The stored event begins before the event and continues afterwards.
Recordings comprise the following information:
■ values sampled from the different signals

- date
- characteristics of the recorded channels.

The names of the logic input and output data used in Logipam are also used in disturbance recording for ease of reading.
The duration and number of recordings may be set using the SFT2841 software tool. The files are recorded in FIFO (First In First Out) type shift storage: when the maximum number of recordings is reached, the oldest recording is erased when a new recording is triggered.

## Transfer

Files may be transferred locally or remotely:
■ locally: using a PC which is connected to the front panel and includes the SFT2841 software tool
■ remotely: using a software tool specific to the remote monitoring and control system.

Recovery
The signals are recovered from a recording by means of the Wavewin-SE software tool.

## Block diagram



Characteristics

| Recording content | Set-up file: <br> date, channel characteristics, measuring chain <br> transformer ratio |
| :--- | :--- |
|  | Sample file: |
| recorded signals |  |

(1) To be set using the SFT2841 software.
(2) According to type and connection of sensors.
(3) According to Sepam hardware configuration.


- Back up any existing files before changing the DLG function parameter settings as this will result in loss of the existing files.
- Any change to the Sepam time affects the Data logs because the time system in which they operate will have changed.
If a Data log (in Circular or Limited mode) is in progress, the corresponding operating mode is as follows: $\square$ the Data log is stopped $\square$ the user must explicitly reset the command he has triggered before being able to trigger another one.


## Operation

This function is used to record and back up a set of measurements available in the Sepam relay, in the form of a COMTRADE file. The number of backed-up files and the number of measurements per file depend on the type of cartridge installed. The recording mode and selection of measurements can be configured by the user via the SFT2841 software.
The files are saved in a FIFO memory (First In First Out): when the maximum number of files is reached, a new file replaces the oldest.
Using the DLG function does not affect the quality of service of Sepam's active protection functions.

## Transfer

The files can be retrieved on a medium external to the Sepam locally or remotely:
■ Locally: using a PC connected to the programming port and running the SFT2841 software
■ Remotely: when the Sepam has the ACE850 and ACE969 communication modules (TP and FO) and a dedicated supervision system program. Only completed files can be transferred. A remote indication data item is created at the end of recording.

## Read

The files can be viewed after being transferred to a PC using software compatible with the COMTRADE format.

## Operating modes

After starting up the DLG function, the measurements are captured continuously. The stop condition and file management differ according to which of the following 2 modes is used:
$\square$ Limited (default mode): the DLG function stops automatically when the end of recording time is reached or on receipt of an external event (a logic input for example). However, the method used to stop must be the same as that used for startup. Thus, it is not possible to start a Data log using the SFT2841 software and stop it with a remote control order (TC)

- Circular: the file content is managed in a FIFO memory: when the file is full, the write operation continues and starts again at the start of the file. Stopping the write operation only results from an external event. In the absence of the stop command, recording is continuous.

These 2 modes are exclusive: it is not possible to have a Data log configured in Limited mode simultaneously with a Data log configured in Circular mode.


The figure below illustrates the principle of padding on a short-lived interruption and a prolonged interruption for a Data log configured in Circular mode.


Circular mode: stopping recording

## Downgraded operation

In the event of loss of the power supply during execution of the Data log function, storage is interrupted then automatically restarted when the power supply returns. In both Limited and Circular configuration modes, on restarting the value $0 \times 8000$ is recorded in the file as a padding value for the period of non-operation.
The figure below illustrates the principle of padding on a short-lived interruption and a prolonged interruption for a Data log configured in Limited mode.
The principle of padding does not apply to a Data log configured in Limited mode and deliberately stopped by the user prior to completion.


Limited mode: padding after interruption of the recording.


Circular mode: padding after interruption of the recording.
Characteristics
Configuration parameters
Content of a COMTRADE file
Configuration file (*.CFG):
date, variable characteristics, transformation ratio of the selected variable values
Samples file (*.DAT):
recorded variables

| Total file duration | 1 s to 30 days |
| :--- | :--- |
| Sampling period | 1 s to 24 hours |
| Variables available for recording | See the table of available data below. |
| Number of files | 1 to 20 |
| Number of variables per file | 1 to 15 |
| Source of starting and stopping | $\square$ SFT 2841 software |
|  | $\square$ Logic equation or Logipam |
|  | $\square$ Remote communication |
| File format | Logic or GOOSE input |

Note: These parameters are configured with the SFT2841 software.

The following measurements, when available in the Sepam relay, can be selected using the SFT2841 software.

| Available measurements | Designation | Units |
| :---: | :---: | :---: |
| Current |  |  |
| Phase current (main inputs) | $\begin{aligned} & 11 \\ & 12 \\ & 13 \\ & \hline \end{aligned}$ | A |
| Phase current (additional inputs) | $\begin{aligned} & \hline \text { '1 } \\ & \text { l'2 } \\ & \text { l'3 } \\ & \hline \end{aligned}$ | A |
| Measured residual current | $10 \mathrm{~m}, \mathrm{l}$ '0m | A |
| Calculated residual current | IOc, l'0c | A |
| Demand current | Ilave, I2ave, I3ave | A |
| Peak demand current |  | A |


| Available data | Designation | Units |
| :---: | :---: | :---: |
| Voltage |  |  |
| Phase-to-neutral voltages (main inputs) | $\begin{aligned} & \text { V1 } \\ & \text { V2 } \\ & \text { V3 } \end{aligned}$ | V |
| Phase-to-neutral voltages (additional inputs) | $\begin{aligned} & \text { V'1 } \\ & \text { V'2 }^{\prime} \end{aligned}$ | V |
| Phase-to-phase voltages (main inputs) | $\begin{aligned} & \text { U21 } \\ & \text { U32 } \\ & \text { U13 } \end{aligned}$ | V |
| Phase-to-phase voltages (additional inputs) | $\begin{aligned} & \hline \text { U'21 } \\ & \text { U'32 } \\ & \text { U'13 } \end{aligned}$ | V |
| Residual voltage | $\begin{aligned} & \hline \text { Vo } \\ & \text { V'0 } \end{aligned}$ | V |
| Neutral-point voltage | Vnt | V |
| Positive-sequence voltage | $\begin{aligned} & \hline \mathrm{Vd} \\ & \text { V'd } \end{aligned}$ | V |
| Negative-sequence voltage | $\begin{aligned} & \hline \mathrm{Vi} \\ & \mathrm{~V}^{\prime} \mathrm{i} \end{aligned}$ | V |
| Frequency | $\begin{aligned} & \mathrm{F} \\ & \mathrm{~F} \end{aligned}$ | Hz |
| Energy |  |  |
| Active power | P | MW |
| Active peak demand power | Pmax | MW |
| Active power per phase | $\begin{aligned} & \hline \text { P1 } \\ & \text { P2 } \\ & \text { P3 } \end{aligned}$ | MW |
| Reactive power | Q | Mvar |
| Reactive peak demand power | Qmax | Mvar |
| Reactive power per phase | $\begin{aligned} & \text { Q1 } \\ & \text { Q2 } \\ & \text { Q3 } \end{aligned}$ | Mvar |
| Apparent power | S | MVA |
| Apparent power per phase | $\begin{aligned} & \text { S1 } \\ & \text { S2 } \\ & \text { S3 } \end{aligned}$ | MVA |
| Power factor ( $\cos \varphi$ ) | cosPhi |  |
| Active energy meter (+ and -) | Eam+ Eam- | MW.h |
| Calculated active energy meter (+ and -) | Eac+ Eac- | MW.h |
| Reactive energy meter (+ and -) | Erm+ Erm- | Mvar.h |
| Calculated reactive energy meter (+ and -) | $\begin{aligned} & \hline \text { Erc+ } \\ & \text { Erc- } \end{aligned}$ | Mvar.h |
| Other |  |  |
| Rotor speed of rotation | meas.speed | rpm |
| Temperature | T1 to T16 | ${ }^{\circ} \mathrm{C} /{ }^{\circ} \mathrm{F}$ |
| Network diagnosis |  |  |
| Unbalance ratio | li / lb | \% lb or \% |
| Current THD | Ithd | \% |
| Voltage THD | Uthd | \% |
| Phase displacement $\varphi 0, \varphi^{\prime} 0, \varphi 0 \Sigma$ | $\varphi 0, \varphi{ }^{\prime} 0, \varphi 0 \Sigma$ | 。 |
| Phase displacement $\varphi 1, \varphi 2, \varphi 3$ | $\varphi 1, \varphi 2, \varphi 3$ | 。 |

Network diagnosis Data log (DLG)
functions


# Synchro-check: voltage comparison and out-of-sync context 

## Operation

## Voltage comparison

For the synchro-check function (ANSI 25), the MCS025 module continuously measures the amplitude, frequency and phase differences between the 2 voltages to be checked, Usynch1 and Usynch2.
The measurement of the differences between the 2 voltages is useful to implement the function and identify the value that is impeding synchronization. The differences are calculated in the following order: amplitude, frequency and phase. As soon as a difference is greater than the threshold set in the synchro-check function, the following differences are not calculated.

## Out-of-sync context

Out-of-sync context gives a precise indication of the cause of the failure of a synchronization request.
It is only provided when the switchgear control function with the "closing with synchro-check" option is activated.

When a synchronization request fails, the amplitude, frequency and phase differences of the Usynch1 and Usynch2 voltages measured by the MCS025 module are recorded, with the date and time, at the end of the switchgear control function "closing request time" delay.

## Readout

The amplitude, frequency and phase differences and out-of-sync context may be accessed via:

- the Sepam display via the key
- the display of a PC with the SFT2841 software

■ the communication link.

## Characteristics

| Amplitude difference | 0 to $120 \%$ of Usynch1 (or Vsynch1) |
| :--- | :--- |
| Measurement range | $\%$ of Usynch1 (or Vsynch1) |
| Unit | $0.1 \%$ |
| Resolution | $\pm 2 \%$ |
| Accuracy | 1 second (typical) |
| Refresh interval | 0 to 10 Hz |
| Frequency difference | Hz |
| Measurement range | 0.01 Hz |
| Unit | 0.05 Hz |
| Resolution | 1 second (typical) |
| Accuracy | 0 to $359^{\circ}$ |
| Refresh interval | ${ }^{\circ}$ |
| Phase difference | $1^{\circ}$ |
| Measurement range | $\pm 2^{\circ}$ |
| Unit | 1 second (typical) |
| Resolution |  |

## Thermal capacity used

## Operation

The thermal capacity used is calculated by the thermal overload protection function for cables, capacitors or machines.
The thermal capacity used is related to the load. The thermal capacity used measurement is given as a percentage of the rated thermal capacity.

## Saving of thermal capacity used

The thermal capacity used is saved in the event of a Sepam power outage. The saved value is used again after the outage.

## Readout

The measurements may be accessed via:

- the Sepam display via the key
- the display of a PC with the SFT2841 software
- the communication link
- an analog converter with the MSA141 option.


## Resetting to zero

The thermal capacity used may be reset to zero, after entry of a password, on:

- the Sepam display via the craar key
- the display of a PC with the SFT2841 software.


## Characteristics

| Measurement range | 0 to $800 \%$ |
| :--- | :--- |
| Units | $\%$ |
| Display format | 3 significant digits |
| Resolution | $1 \%$ |
| Refresh interval | 1 second (typical) |

## Cooling time constant

## Operation

The machine thermal overload protection function (49 RMS machine) uses a cooling time constant (T2) that may be entered by the user, according to the data given by the machine manufacturer or automatically learnt by Sepam.
T2 is estimated:

- after a heating/cooling sequence:
- heating period detected by ES > 70 \%
- followed by a shutdown detected by l < $10 \%$ of lb

■ when the machine temperature is measured by RTDs connected to MET148-2 module no. 1:
$\square$ RTD 1, 2 or 3 assigned to motor/generator stator temperature measurement $\square$ RTD 1, 3 or 5 assigned to transformer temperature measurement.
After each new heating/cooling sequence is detected, a new T2 value is estimated and displayed in the related SFT2841 screen. Measurement accuracy may be improved by using RTD 8 to measure the ambient temperature.
The machine thermal overload function has 2 groups of thermal settings for cases such as natural or forced ventilation or 2-speed motors. A time constant is estimated for each group of thermal settings.

## Readout

The measurements may be accessed via:

- the Sepam display via the key
- the display of a PC with the SFT2841 software
- the communication link.

Characteristics

| Measurement range | 5 to 600 min |
| :--- | :--- |
| Units | min |
| Resolution | 1 min |
| Accuracy | $\pm 5 \%$ |
| Display format | 3 significant digits |

## Remaining operating time before overload tripping

## Operation

The thermal capacity used is calculated by the thermal overload protection function for cables, capacitors or machines. The time depends on the thermal capacity used.

## Readout

The measurements may be accessed via:

- the Sepam display via the key
- the display of a PC with the SFT2841 software
- the communication link.


## Characteristics

| Measurement range | 0 to 999 min |
| :--- | :--- |
| Units | min |
| Display format | 3 significant digits |
| Resolution | 1 min |
| Refresh interval | 1 second (typical) |

## Waiting time before authorization of overload closing

## Operation

This period corresponds to the time it takes the motor to have cooled down enough to allow restarting without tripping again.

## Readout

The measurements may be accessed via:

- the Sepam display via the key
- the display of a PC with the SFT2841 software
- the communication link.


## Characteristics

| Measurement range | 0 to 999 min |
| :--- | :--- |
| Units | min |
| Display format | 3 significant digits |
| Resolution | 1 min |
| Refresh interval | 1 second (typical) |

## Running hours and operating time counter

The counter gives the running total time during which the protected device (motor, generator or transformer) has been operating, i.e. whenever a phase current is $10 \%$ over lb.
For capacitor applications, up to 4 counters are available for the running time of steps 1 to 4. These counters total the time that a capacitor step has been connected to the network (capacitor step switch closed).
The initial counter value may be modified using the SFT2841 software.
The counters are saved in the event of an auxiliary power failure

## Readout

The measurements may be accessed via:
■ the Sepam display via the key

- the display of a PC with the SFT2841 software
- the communication link.


## Characteristics

| Range | 0 to 65535 |
| :--- | :--- |
| Units | hours |

## Starting current and starting time

## Operation

The starting time is defined as follows:
■ If the locked rotor/excessive starting time protection (ANSI code 48/51LR) is active, the starting time is the time separating the moment when one of the 3 phase currents exceeds is and the moment when the 3 currents drop back below Is, Is being the value of the current set point for protection function 48/51LR.

- If the locked rotor/excessive starting time protection (ANSI code 48/51LR) is not active, the starting time is the time separating the moment when one of the 3 phase currents exceeds 1.2 lb and the moment when the 3 currents drop back below 1.2 lb . The maximum phase current obtained during this time corresponds to the starting current.
Both values are saved in the event of an auxiliary power failure.


## Readout

The measurements may be accessed via:

- the Sepam display via the key
- the display of a PC with the SFT2841 software
- the communication link.


## Characteristics

Starting time

| Measurement range |  | 0 to 300 s |
| :---: | :---: | :---: |
| Units |  | s or ms |
| Display format |  | 3 significant digits |
| Resolution |  | 10 ms or 1 digit |
| Refresh interval |  | 1 second (typical) |
| Starting current |  |  |
| Measurement range | 48/51LR active | Is to $24 \mathrm{In}{ }^{(1)}$ |
|  | 48/51LR inactive | 1.2 lb to $24 \ln { }^{(1)}$ |
| Units |  | A or kA |
| Display format |  | 3 significant digits |
| Resolution |  | 0.1 A or 1 digit |
| Refresh interval |  | 1 second (typical) |
| (1) Or 65.5 kA . |  |  |

## Number of starts before inhibition

## Operation

The number of starts allowed before inhibition is calculated by the number of starts protection function (ANSI code 66).
The number of starts depends on the thermal state of the motor.

## Readout

The measurement may be accessed via:
$\square$ the Sepam display via the key

- the display of a PC with the SFT2841 software
- the communication link.


## Resetting to zero

The number of starts counters may be reset to zero, after entry of a password, on:
$\square$ the Sepam display via the (clear) key

- the display of a PC with the SFT2841 software.


## Characteristics

| Measurement range | 0 to 60 |
| :--- | :--- |
| Units | None |
| Display format | 3 significant digits |
| Resolution | 1 |
| Refresh interval | 1 second (typical) |

## Start inhibit time

## Operation

The start inhibit time only applies to motor applications (M81, M87 and M88). It depends on both the starts per hour protection (ANSI code 66) and the machine thermal overload protection (ANSI code 49RMS) if they have been activated. This time expresses the waiting time until another start is allowed.

If at least one of these functions picks up, a "START INHIBIT" message informs the user that starting is not allowed.

## Readout

The number of starts and waiting time may be accessed via:
$\square$ the Sepam display via the key
■ the display of a PC with the SFT2841 software

- the communication link


## Characteristics

| Measurement range | 0 to 360 min |
| :--- | :--- |
| Units | min |
| Display format | 3 significant digits |
| Resolution | 1 min |
| Refresh interval | 1 second (typical) |

## Differential current Through current



## Differential current

## Operation

The differential current id is calculated to facilitate the implementation of the ANSI 87T and ANSI 87M differential protection functions:
■ for a rotating machine (ANSI 87M), it is calculated for each phase by:
$|\overrightarrow{\mathbf{I d}}|=|\overrightarrow{\mathbf{I}}+\overrightarrow{\mathbf{I}}|$

- when a transformer is used (ANSI 87T), the Id calculation takes into account the vector shift and transformation ratio:
$|\overrightarrow{\mathrm{I} d}|=\left|\overrightarrow{\mathrm{Irec}}+\overrightarrow{I^{\prime} \text { rec }}\right|$
The Id value is expressed with respect to $\ln 1$, the rated current of the main channels.


## Readout

The measurements may be accessed via:

- the Sepam display via the key
- the display of a PC with the SFT2841 software

■ the communication link.

## Characteristics

| Measurement range | 0.015 to 40 In |
| :--- | :--- |
| Units | A or kA |
| Resolution | 0.1 A |
| Accuracy ${ }^{(1)}$ | $\pm 5 \%$ |
| Display format | 3 significant digits |
| Refresh interval | 1 second (typical) |
| (1) AA ( und |  |

(1) At In, under reference conditions (IEC 60255-6).

## Through current

## Operation

The through current It is calculated to facilitate the implementation of the ANSI 87T and ANSI 87M differential protection functions:
■ for a rotating machine (ANSI 87M), it is calculated for each phase by:
$|\overrightarrow{r t}|=\left|\frac{\vec{r}-\vec{r}}{2}\right|$

- when a transformer is used (ANSI 87T), the It calculation takes into account the vector shift and transformation ratio:
$|\overrightarrow{\mathbf{l}}|=\max \left(|\overrightarrow{\mid \mathbf{r e c}}|,\left|\overrightarrow{\mathbf{I}^{\prime} \text { rec }}\right|\right)$
The It value is expressed with respect to $\ln 1$, the rated current of the main channels.


## Readout

The measurements may be accessed via:

- the Sepam display via the key
- the display of a PC with the SFT2841 software
- the communication link.

Characteristics

| Measurement range | 0.015 to 40 In |
| :--- | :--- |
| Units | A or kA |
| Resolution | 0.1 A |
| Accuracy ${ }^{(1)}$ | $\pm 5 \%$ |
| Display format | 3 significant digits |
| Refresh interval | 1 second (typical) |
| (1) At In, under reference conditions (IEC $60255-6)$. |  |



## Operation

Current phase displacement between the main phase currents (I) and additional phase currents ( $l^{\prime}$ ) $(\theta 1, \theta 2, \theta 3)$ is calculated for each phase.
The measurements are corrected by taking account of the connection and the direction of rotation of the phases to create an image of the vector shift, which must be set in order to use the ANSI 87T differential protection: $\theta \mathrm{i} / 30=$ vector shift.

## Readout

The measurements may be accessed via:

- the Sepam display via the key

■ the display of a PC with the SFT2841 software

- the communication link.


## Characteristics

| Measurement range | 0 to $359^{\circ}$ |
| :--- | :--- |
| Units | $\circ$ |
| Resolution | $1^{\circ}$ |
| Accuracy ${ }^{(1)}$ | $\pm 2^{\circ}$ |
| Display format | 3 significant digits |
| Refresh interval | 1 second (typical) |
| (1) At In, under reference conditions (IEC $60255-6)$. |  |

Machine operation assistance functions

## Apparent positive sequence impedance <br> Apparent phase-to-phase impedances

## Apparent positive sequence impedance

## Operation

Apparent positive sequence impedance is used to facilitate the implementation of the underimpedance field loss protection function (ANSI 40).
$\mathbf{Z d}=\frac{|\mathbf{V d}|}{|\mathbf{d}|}$

## Readout

The measurement may be accessed via:
■ the display of a PC with the SFT2841 software

- the communication link.


## Characteristics

| Measurement range | 0 to $200 \mathrm{k} \Omega$ |
| :--- | :--- |
| Units | $\Omega$ |
| Resolution | $0.001 \Omega$ |
| Accuracy ${ }^{(1)}$ | $\pm 5 \%$ |
| Refresh interval | 1 second (typical) |
| $(1)$ At $n$, Un, under rencer |  |

(1) At In, Un, under reference conditions (IEC 60255-6).

## Apparent phase-to-phase impedances

## Operation

Apparent phase-to-phase impedances are used to facilitate the implementation of the backup underimpedance protection function (ANSI 21B). They are expressed as the ratio of phase-to-phase voltage to phase-to-phase current.
$\mathbf{Z 2 1}=\frac{\left|\overrightarrow{\mathbf{U}}_{21}\right|}{|\overrightarrow{\mathbf{I}} 21|}$ with $\overrightarrow{\mathbf{I 2 1}}=\overrightarrow{\mathbf{1 1}}-\overrightarrow{\mathbf{I 2}}$
$\mathrm{Z}_{32}=\frac{\mid \overrightarrow{\vec{U}_{32}}}{\left|\vec{I}_{32}\right|}$ with $\overrightarrow{132}=\overrightarrow{12}-\overrightarrow{13}$
$Z_{13}=\frac{|\overrightarrow{\mathbf{u}} 13|}{|\vec{i} 13|}$ with $\overrightarrow{113}=\overrightarrow{\mid 3}-\overrightarrow{11}$

## Readout

The measurement may be accessed via:
■ the display of a PC with the SFT2841 software

- the communication link.


## Characteristics

| Measurement range | 0 to $200 \mathrm{k} \Omega$ |
| :--- | :--- |
| Units | $\Omega$ |
| Resolution | $0.001 \Omega$ |
| Accuracy ${ }^{(1)}$ | $\pm 5 \%$ |
| Refresh interval | 1 second (typical) |
| (1) At In, Un, under reference conditions (IEC 60255-6). |  |

## Third harmonic neutral point voltage

## Operation

Measurement of the 3rd harmonic component of the zero sequence voltage measured at the neutral point of a generator or motor (V3nt).
The value is used for the implementation of the third harmonic undervoltage protection function (ANSI 27TN/64G2).

## Readout

The measurements may be accessed via:

- the Sepam display via the key
$\square$ the display of a PC with the SFT2841 software
- the communication link.


## Characteristics

| Measurement range | 0.2 to $30 \%$ of Vntp |
| :--- | :--- |
| Units | $\%$ of Vntp |
| Resolution | $0.1 \%$ |
| Accuracy ${ }^{(1)}$ | $\pm 1 \%$ |
| Refresh interval | 1 second (typical) |
| $(1)$ Under reference conditions (IEC $60255-6)$ |  |

## Third harmonic residual voltage

## Operation

Measurement of the 3rd harmonic component of the residual voltage, the residual voltage being calculated by the vector sum of the phase-to-neutral voltages.

The value is used for the implementation of the third harmonic undervoltage protection function (ANSI 27TN/64G2).

## Readout

The measurements may be accessed via:
$\square$ the Sepam display via the key
■ the display of a PC with the SFT2841 software

- the communication link.

Characteristics

| Measurement range | 0.2 to $90 \%$ of Vnp |
| :--- | :--- |
| Units | $\%$ fo Vnp |
| Resolution | $0.1 \%$ |
| Accuracy ${ }^{(1)}$ | $\pm 1 \%$ |
| Refresh interval | 1 second (typical) |
| (1) Under reference conditions (IEC $60255-6)$ |  |

(1) Under reference conditions (IEC 60255-6).

## Operation

This operation gives the total capacitance for each phase of the connected capacitor bank steps to allow the condition of the capacitors to be monitored. It covers star and delta connections (parameter set in the "Particular characteristics" screen of the SFT2841 setting and operating software). For this measurement, the installation is considered a perfect capacitance, without any consideration of the resistances added by the connection of the capacitor bank steps.
■ Capacitances measured for star-connected capacitor bank steps:

- C1: total capacitance phase 1
- C2: total capacitance phase 2
$\square$ C3: total capacitance phase 3
- Capacitances measured for delta-connected capacitor bank steps:
- C21: total capacitance between phases 1 and 2
- C32: total capacitance between phases 2 and 3
$\square$ C13: total capacitance between phases 3 and 1 .


## Readout

The capacitance measurements may be accessed via:

- the display of a PC with the SFT2841 software
- the communication link.


## Characteristics

| Measurement range | 0 to 30 F |
| :--- | :--- |
| Unit | $\mu \mathrm{F}, \mathrm{mF}$ or F |
| Resolution | $0.1 \mu \mathrm{~F}$ |
| Accuracy | $\pm 5 \%$ |
| Refresh interval | 1 second (typical) |

## Accuracy

The measurement accuracy is valid if the resistance and inductance per phase of the capacitor bank connecting cable (cable between the Sepam CT and the capacitor bank) respect the following conditions:

- for a star-connected bank:

| $L \omega<0.05 \times\left\|\frac{1}{\mathrm{C} \omega}\right\|$ | where R is the resistance per phase in $\Omega$ <br> L is the inductance per phase in H |
| :--- | :--- |
| $\mathbf{R}<\mathbf{0 . 0 2 7} \times\left\|\frac{1}{\mathrm{C} \omega}\right\|$ | فis the angular frequency in radians/s <br> C is the total capacitance per phase in F |

■ for a delta-connected bank:

$\mathbf{L} \omega<\mathbf{0 . 0 1 7 \times} \times\left|\frac{\mathbf{1}}{\mathbf{C} \omega}\right|$| whereR is the resistance per phase in $\Omega$ |
| :--- |
| L is the inductance per phase in H |


$\mathbf{R}<\mathbf{0 . 0 0 9 \times} \times\left|\frac{\mathbf{1}}{\mathbf{C} \omega}\right| \quad$| $\omega$ is the angular frequency in radians/s |
| :--- |
| C is the total capacitance between phases in F |



## Operation

This function measures the unbalance current of double star-connected capacitor bank steps. This type of current is characteristic of capacitor module damage.

The measurement is carried out via the additional phase and zero sequence current channels:
■ I'1: capacitor step 1 unbalance current measurement

- I'2: capacitor step 2 unbalance current measurement
- I'3: capacitor step 3 unbalance current measurement
- I'0: capacitor step 4 unbalance current measurement.


## Readout

The measurements may be accessed via:

- the Sepam display via the key

■ the screen of a PC with the SFT2841 software

- the communication link


## Characteristics

| Measurement range | 0.02 to 20 l'n |
| :--- | :--- |
| Unit | A |
| Resolution | 0.1 A |
| Accuracy | $\pm 5 \%$ |
| Refresh interval | 1 second (typical) |



Back up any existing files before changing the MSR function parameter settings as this will result in loss of the existing files.

1 Time tagging of the selected file and file selection zone
2 Name of the 1st variable associated with the Y -axis
3 Selection zone for the variable to be associated with the Y -axis
4 Maximum value observed for the recorded variable
5 Duration of read time

## Operation

This Data log function, available only in motor applications, is used to view in the form of curves how some measurements change during motor starting.
The number of measurements and recording duration can be configured using the SFT2841 software.
The files are saved in a FIFO memory (First In First Out): when the maximum number of files is reached, a new file replaces the oldest.
Using the Motor start report function does not affect the quality of service of Sepam's active protection functions.

A Motor start report in progress cannot be interrupted by another motor start. In the event of loss of the power supply or changes to parameters apart from the duration, the sampling frequency and/or the selected variables, the file currently being recorded is still saved (it is however ignored when calculating the MST), but the completed files are backed up using the battery.

## Transfer

The files are transferred locally or remotely:
■ Locally: using a PC connected to the programming port and running the SFT2841
software

- Remotely: using a ACE850 and ACE969 communication module (TP and FO) and a dedicated supervision system program.
Only completed files can be transferred.


## Read

The files can be viewed:
■ after downloading, on a PC screen, using the WaveWin software
■ on the Sepam display using the key then the Diagnosis menu.

In the latter case, depending on the type of Sepam display (integrated advanced UMI or integrated mimic-based UMI), up to three graphics can be viewed. Each graphic is used to display 2 curves corresponding to the selected variables using the SFT2841 software.


View of 3 graphics relating to 1 MSR on an integrated mimic-based UMI.

Machine operation help functions

## Motor start report (MSR)

## Configuring the display

1 To select the MSR file to be viewed:
Press the key as many times as necessary, with the current file selection zone active (item 1).
The file number in the series is briefly displayed before giving way to the timetagged data.
2 To associate one of the selected variables with each $Y$-axis:

- Select the axis to be configured by moving to the symbol using the (go to the previous axis) and $\circledast$ (go to the next axis) keys.
■ Once the axis has been selected, use the key to modify the variable to be used. The screen is automatically refreshed.
Pressing the clear key can briefly hide the values appearing on the graphics. This option is only found on the integrated advanced UMI.
Note: The curve display on Sepam should be used with caution because it does not achieve the accuracy obtained with COMTRADE file viewing software.


## Characteristics

(1) The value used is that provided by the 49RMS motor thermal overload protection if this has been activated.
(2) The value used is that for input I104 if the 49RMS generic thermal overload protection has been activated.
(3) The value used is that provided by the 49RMS motor thermal overload protection if this has been activated. The value is 0 if the 49RMS generic thermal overload protection has been activated.
(4) The value used is that for the active 49RMS protection: motor thermal overload or generic thermal overload. (5) Only available for the main voltage channels.

| Configuration parameters | Configuration file ( ${ }^{*}$.CFG): <br> date, variable characteristics, transformation ratio of the <br> selected variable values <br> Samples file (*.DAT): <br> recorded variables |
| :--- | :--- |
| Total file duration | 2 s to 144 s |
| Sampling frequency | Depends on the configured duration (144 s maximum). <br> Example: For a duration of 144 s the frequency is 1 Hz, <br> for a duration of 2 s the frequency is 72 Hz. |
| Variables available for recording | See the table of available data below. |
| Number of files | 1 to 5 with standard cartridge <br> 1 to 20 with extended cartridge |
| Number of variables per file | 1 to 5 with standard cartridge <br> 1 to 10 with extended cartridge |
| File format | COMTRADE - IEC60255-24 Ed $1-2001$ |

Note: These parameters are configured with the SFT 2841 software.

| Available data | Designation | Units |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Phase-to-phase voltages U21, U32, U13 | u21_fund u32_fund u13_fund | V |  |  |
| 11, I2, I3 | i1 fund <br> i2 fund <br> i3 fund | A |  |  |
| Temperature | T1_to_T16 | ${ }^{\circ} \mathrm{C} /{ }^{\circ} \mathrm{F}$ |  |  |
| Rotor speed of rotation ${ }^{(1)}$ | calc.speed | rpm |  |  |
| Rotor speed of rotation ${ }^{(2)}$ | meas.speed | rpm |  |  |
| Rotor resistance ${ }^{(3)}$ | Rr+ | $\Omega$ |  |  |
| Rotor thermal capacity used ${ }^{(3)}$ | Rotor_temp | pu |  |  |
| Stator resistance ${ }^{(3)}$ | Rs | $\Omega$ |  |  |
| Stator thermal capacity used (4) | Stator_temp | pu |  |  |
| Motor thermal capacity used ${ }^{(3)}$ | Motor_temp | pu |  |  |
| Positive-sequence current | Id_fund | A |  |  |
| Negative-sequence current | li_fund | A |  |  |
| Positive-sequence voltage | Vd_fund | V |  |  |
| Negative-sequence voltage | Vi_fund | V |  |  |
| Measured residual current | lo_fund | A |  |  |
| Calculated residual current | Sum_lo | A |  |  |
| Residual voltage | Vo_fund | V |  |  |
| Motor torque ${ }^{(3)}$ | C | pu |  |  |
| Slip ${ }^{(1)}$ | g | pu |  |  |
| Frequency ${ }^{(5)}$ | F | Hz |  |  |
| Input |  |  |  |  |
| Designation | Syntax | Equations Logipam |  |  |
| Triggering MSR | V_MSR_START | ■ ■ |  |  |
| Output |  |  |  |  |
| Designation | Syntax | Equations | Logipam | Matrix |
| MSR in progress | V_MSR_TRIGGED | ■ | $\square$ |  |

## Operation

This function, only available for motor applications, is related to the Motor start trend function. It is used to calculate and display in the form of curves the minimum, demand and maximum values for each value recorded by the Motor start report function (MSR).
These recalculated values which are stored in a file of 144 samples covering a 30day period, can be viewed on the Sepam screen. When the current 30-day period has ended, it is automatically archived in COMTRADE format and will no longer be able to be viewed on the Sepam display (see the Read section).
The files are saved in a FIFO memory (First In First Out): when the maximum number of files is reached, a new file replaces the oldest. The number of files available varies between 12 and 18 depending on the type of memory cartridge installed on Sepam. The trends are only recalculated at the end of each Motor start report.


Calculating an MST using the available MSRs.
A Motor start report interrupted prior to completion is not taken into account when calculating the Motor start trend function.
Using the Motor start report function does not affect the quality of service of Sepam's active protection functions.

## Comment on managing date changes:

On changing to a date prior to the start date of the current MST, this MST is not closed and any new MSR will be taken into account in its calculation.
On changing to a date after the end date of the current MST, this MST is closed and a new MST is created.

## Transfer

The files are transferred locally or remotely:
■ Locally: using a PC connected to the programming port and running the SFT2841 software
■ Remotely: using a ACE850 and ACE969 communication module (TP and FO) and a dedicated supervision system program.
Only completed files can be transferred.
Downloading an MST file for the current period is automatically cancelled in the following cases:

- Triggering an MSR
- Triggering calculation of an MST at the end of an MSR.

Downloading an MST file for another period is automatically cancelled when this file is the oldest and needs to be replaced by a new file due to the FIFO memory being full.

Machine operation help functions

## Read

- The current file and all completed files can be downloaded and viewed on a PC screen, using software compatible with the COMTRADE format.
- Only the current file can be viewed on the Sepam display:

1 Press the key
2 Select the Diagnosis menu
3 Press the key
Depending on the type of Sepam display (integrated advanced UMI or integrated mimic-based UMI), 1 to 3 graphics can be viewed simultaneously. Each graphic can be used to restore curves representing the change in the minimum, demand and maximum values for the values recorded by the Motor start report function (MSR).
Note: The curve display on Sepam should be used with caution because it does not achieve the accuracy obtained with COMTRADE file viewing software.

1 Time tagging of the current file
2 Selection of the variable to be associated with the Y-axis
3 Name of the analyzed variable
4 Duration of read time for each file


View of 3 graphics relating to an MST on an integrated mimic-based UMI.

## Block diagrams


MST calculated
on a base of 4 MSRs


Taking account of the MSRs when calculating an MST.

The current MST file is only refreshed when recording of the MSR file is complete. The current MST file is archived 30 days after its creation. A new MST file is initiated after the 1st restart in the following period.


Evolution of an MST file during the operating time of the observed motor starts.

| Characteristics |  |
| :--- | :--- |
| Content of a COMTRADE file | Configuration file (*.CFG): <br> date, variable characteristics, transformation ratio of the <br> selected variable values <br> Samples file e ${ }^{*}$.DAT): <br> recorded variables |
| Total file duration | 30 days/144 samples |
| Sampling period | 5 hours |
| Variables available for recording | See table of available data for the MST function. |
| Number of files | 1 to 12 with standard cartridge <br> 1 to 18 with extended cartridge |
| File format | COMTRADE - IEC60255-24 Ed 1-2001 |

Note: These parameters are configured with the SFT 2841 software.

Switchgear diagnosis functions

VT supervision ANSI code 60FL

## Operation

The VT (Voltage Transformer) supervision function is used to supervise the complete phase and residual voltage measurement chain:

- voltage transformers
- VT connection to Sepam
- Sepam voltage analog inputs.

There are two units for the function, one for supervision of the main voltage channel VTs and the other for supervision of the additional voltage channel VTs.
The function processes the following failures: - partial loss of phase voltages, detected by: - presence of negative sequence voltage $\square$ and absence of negative sequence current - loss of all phase voltages, detected by: - presence of current on one of the three phases $\square$ and absence of all measured voltages - tripping of the phase VT (and/or residual VT) protection relay, detected by the acquisition on a logic input of the fuse blown contact or auxiliary contact of the circuit breaker protecting the VTs

- other types of failures may be processed using the logic equation editor.
The "Phase voltage fault" and "Residual voltage fault" information disappears automatically when the situation returns to normal, i.e. as soon as: - the cause of the fault has disappeared - and all of the measured voltages are present.


## Use of circuit breaker closed information

The "circuit breaker closed" information is used to detect the loss of one, two or three voltages, if it is connected to a logic input.
In certain applications, the position of the circuit breaker is not sufficient to determine the presence of voltages. In such cases, the equation editor can be used to precisely define the conditions for voltage presence.

Block diagram: phase voltage fault detection.
Partial loss of phase voltages (main voltage channels only)


Block diagram: residual voltage fault detection.


## Consequences of a VT fault on protection functions

A "Phase voltage fault" affects the following protection functions:
■ 21B, 27, 27D, 27TN, 32P, 32Q, 37P, 40, 47, 50/27, 51V, 78PS
■ 59, only in cases where the protection function is set up for phase-to-neutral overvoltage, when the voltages are measured by two phase VTs + V0VTs - 67.

A "residual voltage fault" affects the following protection functions:

- 59 N
- 67N/67NC.

The behavior of the protection functions in the event of a "Phase voltage fault" or Residual voltage fault" is to be set up and the following choices are proposed: ■ for protection functions 21B, 27, 27D, 27TN, 32P, 32Q, 37P, 40, 47, 50/27, 51V, $59 \mathrm{~N}, 59,78 \mathrm{PS}$ : inhibition or no inhibition
■ for protection function 67: inhibition or non-directional operation (50/51)

- for protection function 67N/67NC: inhibition or non-directional operation
(50N/51N).


# Switchgear diagnosis functions 

## VT supervision ANSI code 60FL

## Setting advice

The partial loss of voltages is based on the detection of the presence of negative sequence voltage and the absence of negative sequence current.
By default:

- the presence of negative sequence voltage is detected when: Vi>10\% Vnp (Vsi)
- the absence of negative sequence current is detected when: li < $5 \% \ln$ (Isi)
- time delay T1 is 1 s .

These default settings ensure the stability of the VT supervision function in the event of short-circuits or transient phenomena on the network.
The Isi set point may be raised for highly unbalanced networks.
Time delay T 1 is to be set shorter than the voltage and power protection function tripping times.
Time delay T2 for the detection of the loss of all voltages must be longer than the time it takes for a short-circuit to be cleared by the protection function 50/51 or 67 , to avoid the detection of a VT loss of voltage fault triggered by a 3-phase short-circuit.

The time delay for the 51 V protection function must be longer than the T1 and T2 time delays used for the detection of voltage losses.

## Characteristics

| Validation of the detection of partial loss of phase voltages |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Setting | Yes / No |  |  |  |
| Vsi set point |  |  |  |  |
| Setting | 10 \% to 100 \% of Vnp |  |  |  |
| Accuracy | $\pm 5$ \% |  |  |  |
| Resolution | 1 \% |  |  |  |
| Pick-up / drop-out ratio | 95 \% $\pm 2.5$ \% |  |  |  |
| Isi set point |  |  |  |  |
| Setting | $5 \%$ to $100 \%$ of $\ln$ |  |  |  |
| Accuracy | $\pm 5$ \% |  |  |  |
| Resolution | 1 \% |  |  |  |
| Pick-up / drop-out ratio | $105 \% \pm 2.5$ \% or > (1 + 0.01 $\mathrm{ln} / \mathrm{lsi}) \times 100 \%$ |  |  |  |
| Time delay T1 (partial loss of phase voltages) |  |  |  |  |
| Setting | 0.1 s to 300 s |  |  |  |
| Accuracy | $\pm 2 \%$ or $\pm 25 \mathrm{~ms}$ |  |  |  |
| Resolution | 10 ms |  |  |  |
| Validation of the detection of the loss of all phase voltages |  |  |  |  |
| Setting | Yes/No |  |  |  |
| Detection of the loss of all voltages with verification of the presence of current |  |  |  |  |
| Setting | Yes / No |  |  |  |
| Voltage presence detected by |  |  |  |  |
| Setting | Breaker closed / Logic equation or Logipam |  |  |  |
| Time delay T2 (loss of all voltages) |  |  |  |  |
| Setting | 0.1 s to 300 s |  |  |  |
| Accuracy | $\pm 2$ \% or $\pm 25 \mathrm{~ms}$ |  |  |  |
| Resolution | 10 ms |  |  |  |
| Voltage and power protection behavior |  |  |  |  |
| Setting | No action / inhibition |  |  |  |
| Protection 67 behavior |  |  |  |  |
| Setting | Non-directional / inhibition |  |  |  |
| Protection 67N/67NC behavior |  |  |  |  |
| Setting | Non-directional / inhibition |  |  |  |
| Inputs |  |  |  |  |
| Designation | Syntax | Equations | Logipam |  |
| Phase VT fault | PVTS_x_103 | ■ | $\square$ |  |
| Inhibition of function | PVTS_x_113 | ■ | $\square$ |  |
| Voltage presence | PVTS_x_117 | $\square$ | $\square$ |  |
| Outputs |  |  |  |  |
| Designation | Syntax | Equations | Logipam | Matrix |
| Function output | PVTS_x_3 | ■ | $\square$ | $\square$ |
| Function inhibited | PVTS_x_16 | $\square$ | ■ |  |

Note: $x=$ unit number: $x=1$ : main channels $(V)$.
$x=2$ : additional channels $\left(V^{\prime}\right)$

Switchgear diagnosis functions

CT supervision
ANSI code 60

## Operation

The CT (Current Transformer) supervision function is used to supervise the complete phase current measurement chain:
■ phase current sensors (1 A/5 A CTs or LPCTs)

- phase current sensor connection to Sepam
- Sepam phase current analog inputs.

There are two units for the function, one for supervision of the main current channel CTs (I) and the other for supervision of the additional current channel CTs (l').
The function is inactive if only 2 phase current sensors are connected.
The "Main CT fault" or "Additional CT fault" information disappears automatically when the situation returns to normal, i.e. as soon as the three phase currents are measured and have values greater than $10 \%$ of In.
In the event of the loss of a phase current, the following protection functions may be inhibited to avoid nuisance tripping
■ 21B, 46, 40, 32P, 37P, 32Q, 78PS, 64REF
■ 51 N and 67 N , if IO is calculated by the sum of the phase currents.

## Block diagram



## Characteristics

| Time delay |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Setting |  | 0.15 s to 300 s |  |  |
| Accuracy |  | $\pm 2 \%$ or $\pm 25 \mathrm{~ms}$ |  |  |
| Resolution |  | 10 ms |  |  |
| Inhibition of protection functions 21B, 32P, 32Q, 37P, 40, 46, 51N, 64REF, 67N, 78PS |  |  |  |  |
| Setting |  | No action / inhibition |  |  |
| Inputs |  |  |  |  |
| Designation | Syntax | Equations | Logipam |  |
| Inhibition of function | PCTS_x_113 | - | ■ |  |
| Outputs |  |  |  |  |
| Designation | Syntax | Equations | Logipam | Matrix |
| Delayed output | PCTS_x_3 | ■ | $\square$ | $\square$ |
| Phase 1 fault | PCTS_x_7 | - | - |  |
| Phase 2 fault | PCTS_x_8 | ■ | $\square$ |  |
| Phase 3 fault | PCTS_x_9 | - | - |  |
| Function inhibited | PCTS_x_16 | - | $\square$ |  |

## Switchgear diagnosis functions

## Trip and closing circuit <br> supervision <br> ANSI code 74

## Trip circuit supervision and open / closed matching



Connection for shunt trip unit supervision.


## Operation

This supervision function is designed for trip circuits:
■ with shunt trip units
The function detects:
a circuit continuity
loss of supply

- mismatching of position indication contacts.

The function inhibits closing of the breaking device.

- with undervoltage trip units

The function detects:
$\square$ only mismatching of position indication contacts, trip unit supervision being unnecessary in this case.
The information is accessible in the matrix ("trip circuit" message) and via remote indication TS1.

## Block diagram



Outputs

| Designation | Syntax | Equations | Logipam | Matrix |
| :--- | :--- | :--- | :--- | :--- |
| Trip circuit supervision fault | V_TCS |  | $\square$ | $■$ |

TS/TC equivalence for each protocol

| Modbus | DNP3 | IEC 60870-5-103 | IEC 61850 |
| :--- | :--- | :--- | :--- |
| TS | Binary Input | ASDU, FUN, INF | LN.DO.DA |
| TS1 | BI17 | $1,160,36$ | XCBR1.EEHealth.stVal |

Switchgear diagnosis functions

## Trip and closing circuit supervision ANSI code 74



Connection for closing circuit supervision.

## Closing circuit supervision

## Operation

This function monitors closing coil continuity. It calls for the wiring diagram opposite, connected to a logic input configured with the "Closing coil supervision" function.
The information is accessible in the matrix ("closing circuit" message) and via remote indication TS234.

## Block diagram



| Outputs |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- |
| Designation | Syntax | Equations | Logipam | Matrix |
| Closing circuit supervision fault | V_CCS |  | $■$ | $■$ |

TS/TC equivalence for each protocol

| Modbus | DNP3 | IEC 60870-5-103 | IEC 61850 |
| :--- | :--- | :--- | :--- |
| TS | Binary Input | ASDU, FUN, INF | LN.DO.DA |
| TS234 | Bl121 | $2,21,23$ | XCBR1.EEHealth.stVal |

## Open and close order supervision

 OperationFollowing a circuit breaker open or close order, the system checks whether, after a 200 ms time delay, the circuit breaker has actually changed status. If the circuit breaker status does not match the last order sent, a "Control fault" message and remote indication TS2 are generated.

| Outputs |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- |
| Designation | Syntax | Equations | Logipam | Matrix |
| Control fault <br> (circuit breaker monitoring) | V_CTRLFAUT |  | $\square$ | $\square$ |

TS/TC equivalence for each protocol

| Modbus | DNP3 | IEC 60870-5-103 | IEC 61850 |
| :--- | :--- | :--- | :--- |
| TS | Binary Input | ASDU, FUN, INF | LN.DO.DA |
| TS2 | Bl16 | $1,20,5$ | Command Termination - |

## Operation

The auxiliary power supply is an important factor in cubicle operation. This function monitors it by measuring the Sepam power supply voltage and comparing the measured value to a low and high threshold. If the value is outside the thresholds, an alarm is generated. The related information is available in the matrix and in Logipam.

## Block diagram



## Readout

The measurements may be accessed via:
■ the Sepam display via the key

- the display of a PC with the SFT2841 software
- the communication link.


## Characteristics

Measured auxiliary voltage Vaux, Low threshold alarm, High threshold alarm


TS/TC equivalence for each protocol

| Modbus | DNP3 | IEC 60870-5-103 | IEC 61850 |
| :--- | :--- | :--- | :--- |
| TS | Binary Input | ASDU, FUN, INF | LN.DO.DA |
| TS217 | Bl13 | $2,20,10$ | LPHD1.PwrSupAlm.stVal |
| TS218 | Bl14 | $2,20,11$ | LPHD1.PwrSupAlm.stVal |

## Cumulative breaking current Number of operations

## Cumulative breaking current monitoring

## Operation

This function gives the cumulative breaking current in (kA) ${ }^{2}$ for five current ranges. It is based on measurement of the fundamental component on main channels (I).
The current ranges displayed are:

- $0<1<2$ ln
- 2 In $<1<5$ In
- 5 In $<1<10$ In
- $10 \mathrm{ln}<\mathrm{l}<40 \mathrm{ln}$
- l > 40 ln .

This function gives the cumulative breaking current in $(k A)^{2}$ for five current ranges. This value is monitored by an adjustable set point. When the set point is overrun, an alarm is sent and is available in the matrix and via remote indication TS235.
Each value is saved in the event of an auxiliary power failure.
The initial values may be introduced using the SFT2841 software tool to take into account the real state of a breaking device used.
Refer to switchgear documentation for use of this information.

## Readout

The measurements may be accessed via:

- the Sepam display via the key
- the display of a PC with the SFT2841 software
- the communication link.

Characteristics

| Cumulative breaking current measured |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Range |  | 0 to $65535(\mathrm{kA})^{2}$ |  |  |
| Units |  | primary (kA) ${ }^{2}$ |  |  |
| Resolution |  | 1(kA) ${ }^{2}$ |  |  |
| Accuracy ${ }^{(1)}$ |  | $\pm 10 \% \pm 1$ digit |  |  |
| Alarm set point |  |  |  |  |
| Setting |  | 0 to 65535 (kA) ${ }^{2}$ |  |  |
| Resolution |  | 1(kA)2 |  |  |
| Accuracy ${ }^{(1)}$ |  | $\pm 10 \% \pm 1$ digit |  |  |
| Outputs |  |  |  |  |
| Designation | Syntax | Equations | Logipam | Matrix |
| Cumulative breaking current threshold overrun | V_MAX |  | $\square$ | - |

threshold overrun
(1) At In, under reference conditions (IEC 60255-6).

TS/TC equivalence for each protocol

| Modbus | DNP3 | IEC 60870-5-103 | IEC 61850 |
| :--- | :--- | :--- | :--- |
| TS | Binary Input | ASDU, FUN, INF | LN.DO.DA |
| TS235 | BI135 | $2,21,40$ | XCBR1.SumSwAAIm.stVal |

## Number of operations

## Operation

The function also gives the total number of breaking device operations.
It is activated by tripping orders (O1 relay).
The number of operations is saved in the event of an auxiliary power failure.
It may be reinitialized using the SFT2841 software.

## Readout

The measurements may be accessed via:

- the Sepam display via the key
- the display of a PC with the SFT2841 software
- the communication link.


## Characteristics

| Range | 0 to $4.10^{9}$ |
| :--- | :--- |
| Units | None |
| Resolution | 1 |
| Refresh interval | 1 second (typical) |

## Operating time

## Operation

This function gives the value of the opening operating time of a breaking device (1)v defined with the open command (O1 relay) and change of status of the device open position contact connected to the 1102 input ${ }^{(2)}$.
The value is saved in the event of an auxiliary power failure.

## Readout

The measurements may be accessed via:

- the Sepam display via the key
- the display of a PC with the SFT2841 software
- the communication link.
(1) Refer to switchgear documentation for use of this information.
(2) Optional MES120 module.


## Characteristics

| Measurement range | 20 to 300 |
| :--- | :--- |
| Units | ms |
| Resolution | 1 ms |
| Accuracy | $\pm 1 \mathrm{~ms}$ typical |
| Display format | 3 significant digits |

## Charging time

## Operation

This function gives the value of the breaking device ${ }^{(1)}$ operating mechanism charging time, determined according to the device closed position status change contact and the end of charging contact connected to the Sepam logic inputs ${ }^{(2)}$.
The value is saved in the event of an auxiliary power failure.

## Readout

The measurements may be accessed via:

- the Sepam display via the key
- the display of a PC with the SFT2841 software
- the communication link.
(1) Refer to switchgear documentation for use of this information.
(2) Optional MES120 module.

Characteristics

| Measurement range | 1 to 20 |
| :--- | :--- |
| Units | s |
| Resolution | 1 s |
| Accuracy | $\pm 0.5 \mathrm{~s}$ |
| Display format | 3 significant digits |

## Operation

This function keeps a count of circuit breaker or contactor rackouts.
The information may be used for breaking device maintenance.
The breaking device "racked out" or "disconnected" position must be wired to a logic input and set up in the SFT2841 software in order for rackouts to be counted.
The number of rackouts is saved in the event of an auxiliary power failure. It may be reinitialized using the SFT2841 software.

## Readout

The measurements may be accessed via:
■ the display of a PC with the SFT2841 software

- the communication link.


## Characteristics

| Measurement range | 0 to 65535 |
| :--- | :--- |
| Units | None |
| Resolution | 1 |
| Refresh interval | 1 second (typical) |

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| Functions | Settings |  | Time delays |
| :---: | :---: | :---: | :---: |
| ANSI 12 - Overspeed |  |  |  |
|  | 100 to $160 \%$ of $\Omega$ n |  | 1 to 300 s |
| ANSI 14 - Underspeed |  |  |  |
|  | 10 to $100 \%$ of $\Omega n$ |  | 1 to 300 s |
| ANSI 21B - Underimpedance |  |  |  |
| Impedance Zs | 0.05 to $2.00 \mathrm{Vn} / \mathrm{lb}$ |  |  |
| ANSI 24 - Overfluxing (V/Hz) |  |  |  |
| Tripping curve | Definite time |  |  |
|  | IDMT type A, B or C |  |  |
| Gs set point | 1.03 to 2 pu | Definite time | 0.1 to 20000 s |
|  |  | IDMT | 0.1 to 1250 s |
| ANSI 25 - Synchro-check |  |  |  |
| Measured voltages | Phase-to-phase | Phase-to-neutral |  |
| Rated primary phase-to-phase voltage |  |  |  |
| Unp sync1 (Vnp sync1 = Unp sync1/ $\sqrt{3}$ ) | 220 V to 250 kV | 220 V to 250 kV |  |
| Unp sync2 (Vnp sync2 = Unp sync2/ $\sqrt{3}$ ) | 220 V to 250 kV | 220 V to 250 kV |  |
| Rated secondary phase-to-phase voltage |  |  |  |
| Uns sync1 | 90 V to 120 V | 90 V to 230 V |  |
| Uns sync2 | 90 V to 120 V | 90 V to 230 V |  |
| Synchro-check setpoints |  |  |  |
| dUs set point | $3 \%$ to $30 \%$ of Unp sync1 | 3 \% to $30 \%$ of Vnp sync1 |  |
| dfs set point | 0.05 to 0.5 Hz | 0.05 to 0.5 Hz |  |
| dPhi set point | 5 to $80^{\circ}$ | 5 to $80^{\circ}$ |  |
| Us high set point | 70 \% to 110 \% Unp sync1 | 70 \% to 110 \% Vnp sync1 |  |
| Us low set point | 10 \% to 70 \% Unp sync1 | 10 \% to 70 \% Vnp sync1 |  |
| Other settings |  |  |  |
| Lead time | 0 to 0.5 s | 0 to 0.5 s |  |
| Operating modes: no-voltage conditions for which coupling is allowed | Dead1 AND Live2 | Dead1 AND Live2 |  |
|  | Live1 AND Dead2 | Live1 AND Dead2 |  |
|  | Dead1 XOR Dead2 | Dead1 XOR Dead2 |  |
|  | Dead1 OR Dead2 | Dead1 OR Dead2 |  |
|  | Dead1 AND Dead2 | Dead1 AND Dead2 |  |

## Protection functions

| Functions | Settings | Time delays |
| :---: | :---: | :---: |
| ANSI 27 - Undervoltage (L-L) or (L-N) |  |  |
| Tripping curve | Definite time |  |
|  | IDMT |  |
|  | Definite time with a curve that can be customiz |  |
| Set point | 5 to $100 \%$ of Unp | 0.05 to 300 s |
| Measurement origin | Main channels (U) or additional channels (U') |  |
| ANSI 27D - Positive sequence undervoltage |  |  |
| Set point and time delay | 15 to $60 \%$ of Unp | 0.05 to 300 s |
| Measurement origin | Main channels (U) or additional channels (U') |  |
| ANSI 27R - Remanent undervoltage |  |  |
| Set point and time delay | 5 to $100 \%$ of Unp | 0.05 to 300 s |
| Measurement origin | Main channels (U) or additional channels (U') |  |
| ANSI 27TN/64G2 - Third harmonic undervoltage |  |  |
| Vs set point (fixed) | 0.2 to $20 \%$ of Vntp | 0.5 to 300 s |
| K set point (adaptive) | 0.1 to 0.2 | 0.5 to 300 s |
| Positive sequence undervoltage | 50 to $100 \%$ of Unp |  |
| Minimum apparent power | 1 to $90 \%$ of Sb ( $\mathrm{Sb}=\sqrt{3} . \mathrm{Un} . \mathrm{lb}$ ) |  |
| ANSI 32P - Directional active overpower |  |  |
|  | 1 to $120 \%$ of $\mathrm{Sn}{ }^{(2)}$ | 0.1 s to 300 s |
| ANSI 32Q - Directional reactive overpower |  |  |
|  | 5 to $120 \%$ of $\mathrm{Sn}{ }^{(2)}$ | 0.1 s to 300 s |
| ANSI 37-Phase undercurrent |  |  |
|  | 0.05 to 1 lb | 0.05 s to 300 s |
| ANSI 37P - Directional active underpower |  |  |
|  | 5 to $100 \%$ of $\mathrm{Sn}{ }^{(2)}$ | 0.1 s to 300 s |
| ANSI 38/49T - Temperature monitoring |  |  |
| Alarm set point TS1 | $0^{\circ} \mathrm{C}$ to $180^{\circ} \mathrm{C}$ or $32{ }^{\circ} \mathrm{F}$ to $356{ }^{\circ} \mathrm{F}$ |  |
| Trip set point TS2 | $0^{\circ} \mathrm{C}$ to $180^{\circ} \mathrm{C}$ or $32{ }^{\circ} \mathrm{F}$ to $356^{\circ} \mathrm{F}$ |  |
| ANSI 40 - Field loss (underimpedance) |  |  |
| Common point: Xa | $0.02 \mathrm{Vn} / \mathrm{lb}$ to $0.2 \mathrm{Vn} / \mathrm{lb}+187.5 \mathrm{k} \Omega$ |  |
| Circle 1: Xb | $0.2 \mathrm{Vn} / \mathrm{lb}$ to $1.4 \mathrm{Vn} / \mathrm{lb}+187.5 \mathrm{k} \Omega$ | 0.05 to 300 s |
| Circle 2: Xc | $0.6 \mathrm{Vn} / \mathrm{lb}$ to $3 \mathrm{Vn} / \mathrm{lb}+187.5 \mathrm{k} \Omega$ | 0.1 to 300 s |
| (1) $S n=$ В $3 . I n . U n \mathrm{p}$. |  |  |



## Protection functions

| Functions | Settings |  | Time delays |
| :---: | :---: | :---: | :---: |
| ANSI 49RMS - Transformer thermal overload |  |  |  |
| Measurement origin Choice of thermal model | I1, I2, I3 / l'1, l'2, I'3 |  |  |
|  | Dry-type transformer Immersed transformer Generic |  |  |
| Type of dry-type transformer | Natural ventilation (AN) / Forced ventilation (AF) |  |  |
| Type of oil-filled transformer | Distribution ONAN / Power ONAN / ONAF / OF / OD |  |  |
| Alarm set point ( $\theta$ alarm) | Immersed transformer: 98 to $160^{\circ} \mathrm{C}\left( \pm 1^{\circ} \mathrm{C}\right)$ or 208 to $320^{\circ} \mathrm{F}\left( \pm 1^{\circ} \mathrm{F}\right)$ |  |  |
|  | Dry-type transformer: 95 to $245{ }^{\circ} \mathrm{C}\left( \pm 1^{\circ} \mathrm{C}\right.$ ) or 203 to $473{ }^{\circ} \mathrm{F}\left( \pm 1^{\circ} \mathrm{F}\right)$ |  |  |
| Tripping set point ( $\theta$ trip) | Immersed transformer: 98 to $160^{\circ} \mathrm{C}\left( \pm 1^{\circ} \mathrm{C}\right)$ or 208 to $320^{\circ} \mathrm{F}\left( \pm 1^{\circ} \mathrm{F}\right)$ |  |  |
|  | Dry-type transformer: 95 to $245^{\circ} \mathrm{C}\left( \pm 1^{\circ} \mathrm{C}\right.$ ) or 203 to $473{ }^{\circ} \mathrm{F}\left( \pm 1^{\circ} \mathrm{F}\right)$ |  |  |
| Time constant for dry-type transfo ( $\tau$ ) | 1 to $600 \mathrm{mn} \pm 1 \mathrm{mn}$ |  |  |
| Time constant for oil-filled transfo | winding ( $\tau$ wdg) 1 to 600 mn | 1 to $600 \mathrm{mn} \pm 1 \mathrm{mn}$ |  |
|  | oil ( $\tau$ oil) | 5 to 600 mn |  |
| ANSI 50BF - Breaker failure |  |  |  |
| Presence of current | 0.2 to 2 ln |  |  |
| Operating time | 0.05 s to 3 s |  |  |
| ANSI 50/27- Inadvertent energization |  |  |  |
| Is set point | 0.05 to 4 ln |  |  |
| Vs set point | 10 to 100 \% Unp |  | T1: 0 to 10 s |
|  |  |  | T2: 0 to 10 s |
| ANSI 50/51 - Phase overcurrent |  |  |  |
| Tripping curve | Tripping time delay Timer hold |  |  |
|  | Definite time DT |  |  |
|  | SIT, LTI, VIT, EIT, UIT ${ }^{(1)}$ | DT |  |
|  | RI DT |  |  |
|  | IEC: SIT/A, LTI/B, VIT/B, EIT/C DT or IDMT |  |  |
|  | IEEE: MI (D), VI (E), El (F) DT or IDMT |  |  |
|  | IAC: I, VI, EI DT or IDMT |  |  |
|  | Customized DT |  |  |
| Is set point | 0.05 to 24 In | Definite time | Inst; 0.05 s to 300 s |
|  | 0.05 to 2.4 ln IDMT |  | 0.1 s to 12.5 s at 10 ls |
| Timer hold | Definite time (DT; timer hold) |  | Inst; 0.05 s to 300 s |
|  | IDMT (IDMT; reset time) |  | 0.5 s to 20 s |
| Measurement origin | Main channels (I) or additional channels (l) |  |  |
| Harmonic 2 restraint | 5 to 50 \% |  |  |
| Min short-circuit current Isc | In to 999 kA |  |  |
| Confirmation | None |  |  |
|  | By negative sequence overvoltage |  |  |
|  | By phase-to-phase undervoltage |  |  |

ANSI 50/27 - Inadvertent energization
(1) Tripping as of 1.2 Is .

| Functions | Settings |  | Time delays |
| :---: | :---: | :---: | :---: |
| ANSI 50N/51N or 50G/51G - Earth fault |  |  |  |
| Tripping curve | Tripping time delay | Timer hold |  |
|  | Definite time | DT |  |
|  | SIT, LTI, VIT, EIT, UIT ${ }^{(1)}$ | DT |  |
|  | RI | DT |  |
|  | CEI: SIT/A,LTI/B, VIT/B, EIT/C | DT or IDMT |  |
|  | IEEE: MI (D), VI (E), El (F) | DT or IDMT |  |
|  | IAC: I, VI, EI | DT or IDMT |  |
|  | EPATR-B, EPATR-C | DT |  |
|  | Customized | DT |  |
| Is0 set point | 0.01 to $15 \mathrm{In0}(\mathrm{~min} .0 .1 \mathrm{~A})$ | Definite time | Inst; 0.05 s to 300 s |
|  | 0.01 to $1 \mathrm{ln} 0(\mathrm{~min} .0 .1 \mathrm{~A})$ | IDMT | 0.1 s to 12.5 s at 10 ls 0 |
|  | 0.6 to 5 A | EPATR-B | 0.5 to 1 s |
|  | 0.6 to 5 A | EPATR-C | 0.1 to 3 s |
| Timer hold | Definite time (DT; timer hold) |  | Inst; 0.05 s to 300 s |
|  | IDMT (IDMT; reset time) |  | 0.5 s to 20 s |
| Measurement origin | 10 input, l'O input, sum of phase currents l0£ or sum of phase currents l'OE |  |  |
| ANSI 50V/51V - Voltage-restrained overcurrent |  |  |  |
| Tripping curve | Tripping time delay | Timer hold |  |
|  | Definite time | DT |  |
|  | SIT, LTI, VIT, EIT, UIT ${ }^{(1)}$ | DT |  |
|  | RI | DT |  |
|  | IEC: SIT/A, LTI/B, VIT/B, EIT/C | DT or IDMT |  |
|  | IEEE: MI (D), VI (E), El (F) | DT or IDMT |  |
|  | IAC: I, VI, EI | DT or IDMT |  |
|  | Customized | DT |  |
| Is set point | 0.5 to 24 ln | Definite time | Inst; 0.05 s to 300 s |
|  | 0.5 to 2.4 In | IDMT | 0.1 s to 12.5 s at 10 ls |
| Timer hold | Definite time (DT; timer hold) |  | Inst; 0.05 s to 20 s |
|  | IDMT (IDMT; reset time) |  | 0.5 s to 300 s |
| Measurement origin Main channels (I) or additional channels (l') |  |  |  |
| ANSI 51C - Capacitor bank unbalance |  |  |  |
| Is set point | 0.05 A to 2 l 'n | Definite time | 0.1 to 300 s |
| ANSI 59 - Overvoltage (L-L) or (L-N) |  |  |  |
| Set point and time delay | 50 to $150 \%$ of Unp or Vnp |  | 0.05 to 300 s |
| Set point and time delay for additional channels of the B83 application | 1.5 to 150 \% of Unp or Vnp |  | 0.05 to 300 s |
| Measurement origin | Main channels (U) or additional channels (U') |  |  |
| ANSI 59N - Neutral voltage displacement |  |  |  |
| Tripping curve | Definite time |  |  |
|  | IDMT |  |  |
| Set point | 2 to $80 \%$ of Unp | Definite time | 0.05 to 300 s |
|  | 2 to $10 \%$ of Unp | IDMT | 0.1 to 100 s |
| Measurement origin Main channels (U), additional channels ( $U^{\prime}$ ') or neutral-point voltage VntANSI 64REF - Restricted earth fault differential |  |  |  |
|  |  |  |  |
| Is0 set point | 0.05 to $0.8 \mathrm{ln}(\mathrm{ln} \geqslant 20 \mathrm{~A})$ |  |  |
|  | 0.1 to $0.8 \ln (\ln <20 \mathrm{~A})$ |  |  |
| Measurement origin | Main channels (I, IO) or additional channels ( $\mathrm{I}^{\prime}$, $\mathrm{I}^{\prime} 0$ ) |  |  |
| ANSI 66 - Starts per hour |  |  |  |
| Permitted number of consecutive cold starts (Nc) | 1 to 5 | Delay between consecutive starts | 1 to 90 mn |
| Permitted number of consecutive hot starts (Nh) | 1 to ( $\mathrm{Nc}-1$ ) | Delay between stop/start | 0 to 90 mn |

## Protection functions

| Functions | Settings |  | Time delays |
| :---: | :---: | :---: | :---: |
| ANSI 67 - Directional phase overcurrent |  |  |  |
| Characteristic angle | $30^{\circ}, 45^{\circ}, 60^{\circ}$ |  |  |
|  | Tripping time delay | Timer hold delay |  |
| Tripping curve | Definite time | DT |  |
|  | SIT, LTI, VIT, EIT, UIT ${ }^{(1)}$ | DT |  |
|  | RI | DT |  |
|  | IEC: SIT/A, LTI/B, VIT/B, EIT/C | DT or IDMT |  |
|  | IEEE: MI (D), VI (E), El (F) | DT or IDMT |  |
|  | IAC: I, VI, EI | DT or IDMT |  |
|  | Customized | DT |  |
| Is set point | 0.1 to 24 In | Definite time | Inst; 0.05 s to 300 s |
|  | 0.1 to 2.4 In | IDMT | 0.1 s to 12.5 s at 10 ls |
| Timer hold | Definite time (DT; timer hold) |  | Inst; 0.05 s to 300 s |
|  | IDMT (IDMT; reset time) |  | 0.5 s to 20 s |
| ANSI 67N/67NC type 1 - Directional earth fault, according to IO projection |  |  |  |
| Characteristic angle | -45 ${ }^{\circ}, 0^{\circ}, 15^{\circ}, 30^{\circ}, 45^{\circ}, 60^{\circ}, 90^{\circ}$ |  |  |
| Is0 set point | 0.01 to 15 ln 0 (mini. $0,1 \mathrm{~A})$ | Definite time | Inst; 0.05 s to 300 s |
| Vs0 set point | 2 to $80 \%$ of Unp |  |  |
| Memory time | TOmem time | 0; 0.05 s to 300 s |  |
|  | VOmem validity set point | 0; 2 to $80 \%$ of Unp |  |
| Measurement origin | 10 input, l'0 input |  |  |

ANSI 67N/67NC type 2 - Directional earth fault, according to 10 vector magnitude directionalized on a tripping half-plane

| Characteristic angle | $-45^{\circ}, 0^{\circ}, 15^{\circ}, 30^{\circ}, 45^{\circ}, 60^{\circ}, 90^{\circ}$ |  |  |
| :---: | :---: | :---: | :---: |
|  | Tripping time delay | Timer hold delay |  |
| Tripping curve | Definite time | DT |  |
|  | SIT, LTI, VIT, EIT, UIT ${ }^{(1)}$ | DT |  |
|  | RI | DT |  |
|  | IEC: SIT/A,LTI/B, VIT/B, EIT/C | DT or IDMT |  |
|  | IEEE: MI (D), VI (E), El (F) | DT or IDMT |  |
|  | IAC: I, VI, EI | DT or IDMT |  |
|  | Customized | DT |  |
| Is0 set point | 0.01 to $15 \mathrm{In} 0(\mathrm{~min} .0 .1 \mathrm{~A})$ | Definite time | Inst; 0.05 s to 300 s |
|  | 0.01 to $1 \mathrm{ln} 0(\mathrm{~min} .0 .1 \mathrm{~A})$ | IDMT | 0.1 s to 12.5 s at 10 ls 0 |
| Vs0 set point | 2 to 80 \% of Unp |  |  |
| Timer hold | Definite time (DT; timer hold) |  | Inst; 0.05 s to 300 s |
|  | IDMT (IDMT; reset time) |  | 0.5 s to 20 s |


| ANSI 67N/67NC type 3 - Directional earth fault, according to 10 vector magnitude directionalized on a tripping sector |  |  |  |
| :---: | :---: | :---: | :---: |
| Tripping sector start angle |  | $0^{\circ}$ to $359^{\circ}$ |  |
| Tripping sector end angle |  | $0^{\circ}$ to $359^{\circ}$ |  |
| Is0 set point | CSH core balance CT (2 A rating) | 0.1 A to 30 A | Definite time Inst; 0.05 to 300 s |
|  | 1 ACT | 0.005 to $15 \ln 0(\mathrm{~min} .0 .1 \mathrm{~A})$ |  |
|  | Core balance CT + ACE990 (range 1) | 0.01 to $15 \mathrm{In0}(\mathrm{~min} .0 .1 \mathrm{~A})$ |  |
| Vs0 set point |  | Calculated V0 (sum of 3 voltages) | 2 to 80\% of Unp |
|  |  | Measured V0 (external VT) | 0.6 to 80\% of Unp |
| Measurement origin |  | 10 input or l'0 input |  |

(1) Tripping from 1.2 Is.

| Functions | Settings | Time delays |
| :---: | :---: | :---: |
| ANSI 78PS - Pole slip |  |  |
| Stabilization delay | 1 to 300 s |  |
| Maximum variation of internal angle | 100 to $1000{ }^{\circ}$ |  |
| Confirmation delay | 0 to 300 ms |  |
| Equal-area criterion |  |  |
| Confirmation delay | 0.1 to 300 s |  |
| Power swings |  |  |
| Number of turns | 1 to 30 |  |
| Maximum time between 2 turns | 1 to 300 s |  |
| ANSI 81H-Overfrequency |  |  |
| Set point and time delay | 49 to 55 Hz or 59 to 65 Hz | 0.1 to 300 s |
| Measurement origin | Main channels (U) or additio |  |
| ANSI 81L - Underfrequency |  |  |
| Set point and time delay | 40 to 51 Hz or 50 to 61 Hz | 0.1 to 300 s |
| Measurement origin | Main channels (U) or additi |  |
| ANSI 81R - Rate of change of frequency |  |  |
|  | 0.1 to $10 \mathrm{~Hz} / \mathrm{s}$ | 0.15 to 300 s |
| ANSI 87M - Machine differential |  |  |
| Ids set point | 0.05 to $0.5 \mathrm{ln}(\mathrm{ln} \geqslant 20 \mathrm{~A})$ |  |
|  | 0.1 to $0.5 \mathrm{ln}(\mathrm{ln}<20 \mathrm{~A})$ |  |
| ANSI 87T - Transformer differential |  |  |
| High set point | 3 to $18 \ln 1$ |  |
| Percentage-based curve |  |  |
| Ids set point | 30 to $100 \% \ln 1$ |  |
| Slope Id/It | 15 to 50 \% |  |
| Slope Id/It2 | Without, 50 to 100 \% |  |
| Slope change point | 1 to $18 \ln 1$ |  |
| Restraint on energization |  |  |
| Isinr set point | 1 to 10 \% |  |
| Delay | 0 to 300 s |  |
| Restraint on CT loss |  |  |
| Activity | On / Off |  |
| Harmonic restraints | Conventional |  |
| Selection of restraint | Conventional |  |
| Harmonic 2 percentage set point | Off, 5 to 40 \% |  |
| Harmonic 2 restraint | Phase-specific/Global |  |
| Harmonic 5 percentage set point | Off, 5 to 40 \% |  |
| Harmonic 5 restraint | Phase-specific/Global |  |

## Protection functions

Overspeed
ANSI code 12

Detection of excessive machine speeds to protect generators and processes.

## Description

Detection of machine overspeed to detect synchronous generator racing due to loss of synchronism, or for process monitoring, for example.
The rotation speed is calculated by measuring the time between pulses transmitted by a proximity sensor at each passage of one or more cams driven by the rotation of the motor or generator shaft (see a more in-depth description in the "Metering functions" chapter).
The speed acquisition parameters must be set on the "Particular characteristics" screen of the SFT2841 software.
The "Rotor speed measurement" function must be assigned to logic input I104 for the function to work.
The protection picks up if the speed measured exceeds the speed set point. The protection includes a definite time delay T .

## Block diagram



## Characteristics

| Settings |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Set point $\Omega$ s |  |  |  |  |
| Setting range | 100 to $160 \%$ of $\Omega$ n |  |  |  |
| Accuracy ${ }^{(1)}$ | $\pm 2$ \% |  |  |  |
| Resolution | $1 \%$ |  |  |  |
| Drop out/pick up ratio | 95 \% |  |  |  |
| Time delay T |  |  |  |  |
| Setting range | 1 s to 300 s |  |  |  |
| Accuracy ${ }^{(1)}$ | $\pm 25 \mathrm{~ms}$ or $\pm\left(60000 /\left(\Omega \mathrm{s}^{(2)} \times \mathrm{R}^{(3)}\right)\right) \mathrm{ms}$ |  |  |  |
| Resolution | 1 s |  |  |  |
| Inputs |  |  |  |  |
| Designation | Syntax | Equations | Logipam |  |
| Protection reset | P12_x_101 | - | ■ |  |
| Protection inhibition | P12_x_113 | $\square$ | ■ |  |
| Outputs |  |  |  |  |
| Designation | Syntax | Equations | Logipam | Matrix |
| Instantaneous output (pick-up) | P12_x_1 | $\square$ | ■ |  |
| Delayed output | P12_x_3 | $\square$ | ■ | ■ |
| Protection inhibited | P12_x_16 | $\square$ | $\square$ |  |

x: unit number.
(1) Under reference conditions (IEC 60255-6).
(2) $\Omega s$ in $r p m$.
(3) R: Number of pulses (cam) per rotation.

## Protection functions

## Underspeed <br> ANSI code 14



## Description

Monitoring of machine speed:

- detection of machine underspeed after starting, for process monitoring, for example
- zero-speed data for detection of locked rotor.

The rotation speed is calculated by measuring the time between pulses transmitted by a proximity sensor at each passage of one or more cams driven by the rotation of the motor or generator shaft (see a more in-depth description in the "Metering functions" chapter).
The speed-acquisition and zero-speed detection parameters must be set on the "Particular characteristics" screen of the SFT2841 software.
The "Rotor speed measurement" function must be assigned to logic input I104 for the function to work.
The protection function picks up if the speed measured drops below the speed set point after having first exceeded the set point by $5 \%$. Zero speed is detected by unit 1 and is used by protection function $48 / 51$ LR to detect rotor locking.
The protection includes a definite (DT) time delay $T$.

## Block diagram



## Characteristics

| Settings |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Set point $\Omega$ s |  |  |  |  |
| Setting range | 10 to $100 \%$ of $\Omega$ n |  |  |  |
| Accuracy ${ }^{(1)}$ | $\pm 2$ \% |  |  |  |
| Resolution | 1 \% |  |  |  |
| Drop out/pick up ratio | 105 \% |  |  |  |
| Time delay T |  |  |  |  |
| Setting range | 1 s to 300 s |  |  |  |
| Accuracy ${ }^{(1)}$ | $\pm 25 \mathrm{~ms}$ or $\pm\left(60000 /\left(\Omega \mathrm{s}^{(2)} \times \mathrm{R}^{(3)}\right)\right) \mathrm{ms}$ |  |  |  |
| Resolution | 1 s with $\mathrm{T} \times\left(60 /\left(\Omega \mathrm{s}{ }^{(2)} \times \mathrm{R}^{(3)}\right)\right.$ ) |  |  |  |
| Inputs |  |  |  |  |
| Designation | Syntax Equations Logipam |  |  |  |
| Protection reset | P14_x_101 ■ ■ |  |  |  |
| Protection inhibition | P14_x_113 ■ ■ |  |  |  |
| Outputs |  |  |  |  |
| Designation | Syntax | Equations | Logipam | Matrix |
| Instantaneous output (pick-up) | P14_x_1 | - | $\square$ |  |
| Delayed output | P14_x_3 | - | $\square$ | - |
| Protection inhibited | P14_x_16 | - | $\square$ |  |
| Zero speed | P14_x_38 | - | $\square$ |  |
| x: unit number. <br> (1) Under reference conditions <br> (2) $\Omega s$ in rpm. <br> (3) R: Number of pulses (cam) |  |  |  |  |

## Protection functions

Underimpedance ANSI code 21B

Phase-to-phase short-circuit protection for generators.


## Example: synchronous generator

Synchronous generator data:
■ S = 3.15 MVA

- Un1 $=6.3 \mathrm{kV}$
- $\mathrm{Xd}=233 \%$
- $X^{\prime} \mathrm{d}=21 \%$


## Description

The protection function is made up of a circular tripping characteristic on the impedance plane ( $R, X$ ), with a definite time delay (constant, DT). It picks up when one of the apparent, phase-to-phase impedances enters the circular tripping characteristic.
Apparent impedances:
$\overrightarrow{\mathbf{Z}}_{21}=\frac{\overrightarrow{\mathbf{U}}_{21}}{\overrightarrow{\mathbf{I} 1}-\overrightarrow{\mathbf{I} 2}}, \overrightarrow{\mathbf{Z}}_{32}=\frac{\overrightarrow{\mathbf{U}}_{32}}{\overrightarrow{\mathbf{I} 2}-\overrightarrow{\mathbf{I} 3}}, \overrightarrow{\mathbf{Z}}_{13}=\frac{\overrightarrow{\mathbf{U}}_{13}}{\overrightarrow{\overrightarrow{\mathbf{I}} 3-\overrightarrow{\mathbf{I}} \mathbf{1}} .}$.

## Block diagram



## Characteristics

| Settings |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Set point $\Omega$ s |  |  |  |  |
| Setting range | $0.05 \mathrm{Vn} / \mathrm{lb} \leqslant \mathrm{Zs} \leqslant 2 \mathrm{Vn} / \mathrm{lb}$ or $0.001 \Omega$ |  |  |  |
| Accuracy ${ }^{(1)}$ | $\pm 2$ \% |  |  |  |
| Resolution | $0.001 \Omega$ or 1 digit |  |  |  |
| Drop out/pick up ratio | 105 \% |  |  |  |
| Time delay T |  |  |  |  |
| Setting range | $200 \mathrm{~ms} \leqslant \mathrm{~T} \leqslant 300 \mathrm{~s}$ |  |  |  |
| Accuracy ${ }^{(1)}$ | $\pm 2 \%$ or from -10 ms to +25 ms |  |  |  |
| Resolution | 10 ms or 1 digit |  |  |  |
| Characteristic times ${ }^{(1)}$ |  |  |  |  |
| Operation time | pick-up < 35 ms from infinite to $\mathrm{Zs} / 2$ (typically 25 ms ) |  |  |  |
| Overshoot time | $<40 \mathrm{~ms}$ |  |  |  |
| Reset time | $<50 \mathrm{~ms}$ |  |  |  |
| Inputs |  |  |  |  |
| Designation | Syntax | Equations Logipam |  |  |
| Protection reset | P21B_1_101 | $\square$ |  |  |
| Protection inhibition | P21B_1_113 | $\square$ |  |  |
| Outputs |  |  |  |  |
| Designation | Syntax | Equations | Logipam | Matrix |
| Instantaneous output (pick-up) | P21B_1_1 | ■ | ■ |  |
| Delayed output | P21B_1_3 | $\square$ | $\square$ | - |
| Protection inhibited | P21B_1_16 | - | ■ |  |

(1) Under reference conditions (IEC 60255-6).

## Protection setting

To set the protection function, it is necessary to calculate the rated generator impedance:
■ $\mathrm{Ib}=\mathrm{S} /(\sqrt{3}$ Un1 $)=289 \mathrm{~A}$

- $\mathrm{Zn}=U n 1 /(\sqrt{3} \mathrm{lb})=12.59 \Omega$

The tripping parameter is typically set to $30 \%$ of the rated generator impedance:
$\mathrm{Zs}=0.30 \times \mathrm{Zn}=3.77 \Omega$
This protection function is used to back up other protection functions. Its setting must therefore ensure discrimination with the other protection functions.
$\mathrm{T}=0.9 \mathrm{~s}$, for example, for a network where faults are cleared in 0.6 s .

## Overfluxing (V/Hz) <br> ANSI code 24

Protection of magnetic circuits in transformers and generators.

## Description

Protection which detects overfluxing of transformer or generator magnetic circuits by calculating the ratio between the greatest phase-to-neutral or phase-to-phase voltage divided by the frequency.
Overfluxing of magnetic circuits is caused by machine operation with excessive voltage or insufficient frequency. It provokes saturation of the magnetic materials and results in temperature rise. In severe cases, a major leakage flux may occur and seriously damage the materials around the magnetic circuit.
The protection function picks up when the U/f or V/f ratio, depending on machine coupling, exceeds the set point. The function is delayed (definite time (DT) or IDMT) according to three curves (see tripping curve equation on page 226).
The typical tripping set point is 1.05 pu .

where $\mathrm{G}=\mathrm{U} / \mathrm{f}$ or $\mathrm{V} / \mathrm{f}$ depending on machine coupling
$G n=U n / f n$ or $V n / f n$ depending on the voltage
Gs = the set point
(1) phase-to-neutral voltage, see the table below.
(2) phase-to-phase voltage, see the table below.

## Machine coupling

This setting adapts the function voltage measurement to the coupling of the magnetic circuit, depending on the measurements made possible by Sepam wiring.

| Voltage used by the protection function |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| VT wiring | $3 V$ | $2 \mathrm{U}+\mathrm{V} 0$ | 2 U | $1 \mathrm{U}+\mathrm{V} 0$ | 10 | $1 \mathrm{~V}+\mathrm{V} 0$ | 1V |
| Delta coupling | (2) | (2) | (2) | (2) | (2) | (1) | (1) |
| Star coupling | (1) | (1) | (2) | (2) | (2) | (1) | (1) |

## Protection functions

## Overfluxing (V / Hz) <br> ANSI code 24



Voltage/frequency ratio IDMT tripping curves



Characteristics

| Settings |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Machine coupling |  |  |  |  |
| Setting range | Delta / star |  |  |  |
| Tripping curve |  |  |  |  |
| Setting range | Definite time <br> IDMT: type A, type B, type C |  |  |  |
| Gs set point |  |  |  |  |
| Setting range | 1.03 to $2.0 \mathrm{pu}{ }^{(2)}$ |  |  |  |
| Accuracy ${ }^{(1)}$ | $\pm 2$ \% |  |  |  |
| Resolution | $0.01 \mathrm{pu}^{(2)}$ |  |  |  |
| Drop out/pick up ratio | $98 \% \pm 1$ \% |  |  |  |
| Time delay $\mathbf{T}$ (operation time at 2 pu ) |  |  |  |  |
| Definite time Setting range | 0.1 to 20000 s |  |  |  |
| Accuracy ${ }^{(1)}$ | $\pm 2 \%$ or from -10 ms to +25 ms |  |  |  |
| IDMT Setting range | 0.1 to 1250 s |  |  |  |
| Accuracy ${ }^{(1)}$ | $\pm 5 \%$ or from -10 ms to +25 ms |  |  |  |
| Resolution | 10 ms or 1 digit |  |  |  |
| Characteristic times ${ }^{(1)}$ |  |  |  |  |
| Operation time | pick-up < 40 ms from 0.9 Gs to 1,1 Gs at fn |  |  |  |
| Overshoot time | $<40 \mathrm{~ms}$ from 0.9 Gs to 1.1 Gs at fn |  |  |  |
| Reset time | $<50 \mathrm{~ms}$ from 1.1 Gs to 0.9 Gs at fn |  |  |  |
| Inputs |  |  |  |  |
| Designation | Syntax Equations Logipam |  |  |  |
| Protection reset | P24_x_101 ■ |  | ■ |  |
| Protection inhibition P24_x_113 ■ - |  |  |  |  |
|  |  |  |  |  |
| Designation | Syntax | Equations | Logipam | Matrix |
| Instantaneous output (pick-up) | P24_x_1 | ■ | - |  |
| Delayed output | P24_x_3 | $\square$ | - | - |
| Protection inhibited | P24_x_16 | $\square$ | - |  |

x: unit number.
(1) Under reference conditions (IEC 60255-6)
(2) 1 pu represents $1 x$ Gn.

## Example 1. synchronous generator

A generator is often protected with two tripping set points:
■ an IDMT set point, set to 1.05 Gn with a long delay.
Example: type B curve, Gs1 = 1.05 and $\mathrm{T} 1=8 \mathrm{~s}$

- a definite time (DT) set point, set to approximately 1.2 Gn with a tripping time of approximately ten seconds.
For example: DT, Gs2 = 1.2 and $\mathrm{T} 2=5 \mathrm{~s}$.


## Example 2. transformer

A transformer is generally protected by an IDMT set point, set to 1.05 Gn with a long delay.
For example: type C curve, $\mathrm{Gs}=1.05$ and $\mathrm{T}=4 \mathrm{~s}$.

## Synchro-check ANSI code 25

Protection function which checks the synchronization of the electrical networks upstream and downstream of a circuit breaker and allows closing when the differences in voltage, frequency and phase are within authorized limits.

## Operation

The synchro-check function is designed to allow circuit breaker closing without any risk of dangerous coupling between two voltages Usync1 and Usync2. The voltages compared may be two phase-to-phase voltages or two phase-to-neutral voltages.

The function is activated when there is a phase, frequency or amplitude difference, within set limits, between the voltages that are compared.

The function is available in the optional MCS025 module. The "Close enable" logic data must be cabled to a logic input on the Sepam. All other data and measurements are transmitted to the Sepam base unit via the CCA785 connection cord.

Block diagram


## Anticipation

It is possible to anticipate the function by a time Ta, taking into account the frequency difference and the circuit breaker closing time, in order for the voltages to be synchronized at the time of coupling.

## Voltage checking

When one of the two voltages is absent, coupling may be authorized according to one of five voltage checking modes.
■ Usync1 absent and Usync2 present (Dead1 AND Live2)
■ Usync1 present and Usync2 absent (Live1 AND Dead2)

- One voltage is present and the other is absent (Dead1 XOR Dead2)

■ One or both of the two voltages are absent (Dead1 OR Dead2)

- Both voltages are absent (Dead1 AND Dead2).

The presence of each of the voltages is detected by comparing the voltage to the high set point (Us high). The absence of either of the voltages is detected by comparing the voltage to the low set point (Us low).

## Protection functions

## Synchro-check ANSI code 25

## User information

The following measurements are available:
■ voltage difference

- frequency difference
- phase difference.


## Characteristics

| Settings <br> dUs set point <br> Setting range | $3 \%$ Unsync1 to $30 \%$ Unsync1 |
| :--- | :--- |
| Accuracy ${ }^{(1)}$ | $\pm 2.5 \%$ or 0,003 Unsync1 |
| Resolution | $1 \%$ |
| Drop out/pick up ratio <br> dfs set point | $106 \%$ |
| Setting range | 0.05 Hz to 0.5 Hz |
| Accuracy ${ }^{(1)}$ | $\pm 10 \mathrm{mHz}$ |
| Resolution | 0.01 Hz |
| Drop out/pick up | $<15 \mathrm{mHz}$ |
| dPhis set point | $5^{\circ}$ to $50^{\circ}$ |
| Setting range | $\pm 2^{\circ}$ |
| Accuracy ${ }^{(1)}$ | $1^{\circ}$ |
| Resolution | $120 \%$ |
| Drop out/pick up ratio | $70 \%$ Unsync1 to $110 \%$ Unsync1 |
| Us high set point | $\pm 1 \%$ |
| Setting range | $1 \%$ |
| Accuracy ${ }^{(1)}$ | $93 \%$ |
| Resolution | $10 \%$ Unsync1 to $70 \%$ Unsync1 |
| Drop out/pick up ratio | $\pm 1 \%$ |
| Us low set point | $1 \%$ |
| Setting range | $106 \%$ |
| Accuracy ${ }^{(1)}$ | Resolution |

Drop out/pick up ratio 106 \%
Anticipation of circuit breaker closing time

| Setting range | 0 to 500 ms |
| :---: | :---: |
| Accuracy ${ }^{(1)}$ | $\pm 2$ \% or $\pm 25 \mathrm{~ms}$ |
| Resolution | 10 ms or 1 digit |
| Voltage checking |  |
| Setting range | In service / Out of service |
| Operating mode with no voltage |  |
| Setting range | Dead1 AND Live2 Live1 AND Dead2 Dead1 XOR Dead2 Dead1 OR Dead2 Dead1 AND Dead2 |

Characteristic times ${ }^{(1)}$

| Operation time | $<190 \mathrm{~ms}$ |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| dU operation time | $<120 \mathrm{~ms}$ |  |  |  |
| df operation time | $<190 \mathrm{~ms}$ |  |  |  |
| dPhi operation time | $<190 \mathrm{~ms}$ |  |  |  |
| Reset time | $<50 \mathrm{~ms}$ |  |  |  |
| Outputs ${ }^{(1)}$ |  |  |  |  |
| Designation | Syntax | Equations | Logipam | Matrix |
| Close enable |  |  |  |  |
| Synchro-check | P25_1_46 | - | - |  |
| No voltage | P25_1_47 | $\square$ | ■ |  |
| Phase difference | P25_1_49 | $\square$ | ■ |  |
| Frequency difference | P25_1_50 | - | - |  |
| Voltage difference | P25_1_51 | - | - |  |
| No Usync1 | P25_1_52 | $\square$ | ■ |  |
| No Usync2 | P25_1_53 | $\square$ | $\square$ |  |

## Protection against phase-to-neutral or

 phase-to-phase voltage dips.
## Operation

Protection against voltage dips or detection of abnormally low voltage in order to:

- Trigger automatic load shedding
- Trigger a source transfer
- Disconnect a generator, in conformity with a "Grid code".
It includes a time delay $T$ with:
- definite time (DT)
- inverse definite minimum time (see the tripping curve equation on page 226)
■ definite time with a curve $T(U / U n)$ that can be customized point by point.
Whether operation is phase-to-neutral or phase-tophase voltage depends on the connection chosen for the voltage inputs.


## Custom "Grid code" curve

Production installations must stay connected to the grid whenever the voltage is higher than that defined by the "Grid code" curve. The custom curve is defined point by point, with the disconnection time Tc in seconds on the X -axis and the voltage $\mathrm{U} / \mathrm{Un}$ in pu on the Y -axis.

"Grid code" curve.
Connection conditions

| Connection type | $\mathrm{V} 1, \mathrm{~V} 2, \mathrm{~V} 3^{(1)}$ | $\begin{aligned} & \text { U21, U32 } \\ & + \text { Vo } \\ & \hline \end{aligned}$ | U21, U32 |
| :---: | :---: | :---: | :---: |
| Operation in phase-to-neutral voltage | YES | YES | NO |
| Operation in phase-to-phase voltage | YES | YES | YES |
| Connection type | U21 ${ }^{(1)}$ | V1 ${ }^{(1)}$ |  |
| Operation in phase-toneutral voltage | NO | On V1 | only |
| Operation in phase-tophase voltage | On U21 only | NO |  |

(1) With or without $V O$.


Characteristics

| Settings |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Measurement origin |  |  |  |  |
| Setting range | Main channels (U) / Additional channels (U') |  |  |  |
| Voltage acquisition mode |  |  |  |  |
| Setting range | Phase-to-phase voltage / Phase-to-neutral voltage |  |  |  |
| Tripping curve |  |  |  |  |
| Setting range | Definite time / IDMT / Customizable |  |  |  |
| Us (or Vs) set point |  |  |  |  |
| Setting range | $5 \%$ of Unp (or Vnp) to $100 \%$ of Unp (or Vnp) |  |  |  |
| Accuracy ${ }^{(1)}$ | $\pm 2$ \% or $\pm 0,005$ Unp |  |  |  |
| Resolution | 1 \% |  |  |  |
| Drop-out/pick-up ratio | 103 \% $\pm 2$ \% |  |  |  |
| Time delay $\mathbf{T}$ (tripping time for zero voltage) |  |  |  |  |
| Setting range | 50 ms to 300 s |  |  |  |
| Accuracy ${ }^{1)}$ | $\pm 2 \%$ or $\pm 25 \mathrm{~ms}$ |  |  |  |
| Resolution | 10 ms or 1 digit |  |  |  |
| Characteristic times |  |  |  |  |
| Operating time | Pick-up < 40 ms from 1.1 Us (Vs) to 0.9 Us (Vs) ( 25 ms typical) |  |  |  |
| Overshoot time | $<40 \mathrm{~ms}$ from 1.1 Us (Vs) to 0.9 Us (Vs) |  |  |  |
| Reset time | < 50 ms from 0.9 Us (Vs) to 1.1 Us (Vs) |  |  |  |
| Inputs |  |  |  |  |
| Designation | Syntax Equations Logipam |  |  |  |
| Reset protection | P27_x_101 ■ ■ |  |  |  |
| Inhibit protection | P27_x_113 | - | ■ |  |
| Outputs |  |  |  |  |
| Designation | Syntax | Equations | Logipam | Matrix |
| Instantaneous output (pick-up) | P27_x_1 | - | - |  |
| Time-delayed output | P27_x_3 | - | - | ■ |
| Phase 1 fault ${ }^{(2)}$ | P27_x_7 | - | ■ |  |
| Phase 2 fault ${ }^{(2)}$ | P27_x_8 | $\square$ | $\square$ |  |
| Phase 3 fault ${ }^{(2)}$ | P27_x_9 | $\square$ | $\square$ |  |
| Protection inhibited | P27_x_16 | - | - |  |
| Instantaneous output V1 or U21 | P27_x_23 | - | $\square$ |  |
| Instantaneous output V2 or U32 | P27_x_24 | - | - |  |
| Instantaneous output V3 or U13 | P27_x_25 | - | - |  |
| Delayed output V1 or U21 | P27_x_26 | $\square$ | $\square$ |  |
| Delayed output V2 or U32 | P27_x_27 | - | $\square$ |  |
| Delayed output V3 or U13 | P27_x_28 | $\square$ | ■ |  |

$x$ : Unit number.
(1) Under reference conditions (IEC 60255-6)
(2) When the protection in used is phase-to-neutral voltage.

# Protection functions <br> Positive sequence <br> undervoltage and phase rotation <br> direction check <br> ANSI code 27D 

## Description

Protection of motors against faulty operation due to insufficient or unbalanced network voltage. It is based on measurement of the positive sequence voltage Vd. It includes a definite time delay $T$.
It does not operate when only a single phase-to-neutral or phase-to-phase voltage is connected.
This protection also detects the phase rotation direction. The protection function considers that the phase rotation direction is reversed when the positive sequence voltage is less than 10 \% of Unp and when the phase-to-phase voltage is greater than $80 \%$ of Unp. When this is the case, the alarm message "ROTATION -" is generated.

## Block diagram



## Characteristics

## Settings

Measurement origin

| Setting range | Main channels (U) / Additional channels (U') |
| :---: | :---: |
| Vsd set point |  |
| Setting range | 15 \% Unp to 60 \% Unp |
| Accuracy ${ }^{(1)}$ | $\pm 2$ \% or $\pm 0.005$ Unp |
| Resolution | 1 \% |
| Drop out/pick up ratio | $103 \% \pm 2$ \% |
| Time delay T |  |
| Setting range | 50 ms to 300 s |
| Accuracy ${ }^{(1)}$ | $\pm 2 \%$ or $\pm 25 \mathrm{~ms}$ |
| Resolution | 10 ms or 1 digit |
| Characteristic times |  |
| Operation time | Pick-up < 40 ms from 1.1 Vsd to 0.9 Vsd |
| Overshoot time | $<40 \mathrm{~ms}$ from 1.1 Vsd to 0.9 Vsd |
| Reset time | $<50 \mathrm{~ms}$ from 0.9 Vsd to 1.1 Vsd |
| Inputs |  |
| Designation | Syntax Equations Logipam |
| Protection reset | P27D_x_101 ■ ■ |
| Protection inhibition | P27D_x_113 ■ ■ |
| Outputs |  |
| Designation | Syntax Equations Logipam Matrix |
| Instantaneous output (pick-up) | P27D_x_1 ■ ■ |
| Delayed output | P27D_x_3 ■ ■ ■ |
| Protection inhibited | P27D_x_16 ■ ■ |

$x$ : unit number
(1) Under reference conditions (IEC 60255-6).

## Remanent undervoltage ANSI code 27R

Detection of the remanent voltage sustained by rotating machines.

## Description

Protection used to check that remanent voltage sustained by rotating machines has been cleared before allowing the busbars supplying the machines to be reenergized, to avoid electrical and mechanical transients.
This protection is single-phase. It picks up when the U21 or V1 voltage is less than the Us set point. The protection includes a definite time delay (constant).

Block diagram


## Characteristics

## Settings

| Measurement origin |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Setting range | Main channels (U) / Additional channels (U') |  |  |  |
| Us set point |  |  |  |  |
| Setting range | 5 \% Unp to 100 \% Unp |  |  |  |
| Accuracy ${ }^{(1)}$ | $\pm 5 \%$ or 0.005 Unp |  |  |  |
| Resolution | 1 \% |  |  |  |
| Drop out/pick up ratio | $103 \% \pm 2$ \% |  |  |  |
| Time delay T |  |  |  |  |
| Setting range | 50 ms to 300 s |  |  |  |
| Accuracy ${ }^{(1)}$ | $\pm 2 \%$ or $\pm 25 \mathrm{~ms}$ |  |  |  |
| Resolution | 10 ms or 1 digit |  |  |  |
| Characteristic times |  |  |  |  |
| Operation time | Pick-up < 45 ms from 1.1 Us to 0.9 Us |  |  |  |
| Overshoot time | $<35 \mathrm{~ms}$ from 1.1 Us to 0.9 Us |  |  |  |
| Reset time | $<35 \mathrm{~ms}$ from 0.9 Us to 1.1 Us |  |  |  |
| Inputs |  |  |  |  |
| Designation | Syntax | Equations Logipam |  |  |
| Protection reset | P27R_x_101 ■ |  | ■ |  |
| Protection inhibition | P27R_x_113 | ■ | - |  |
| Outputs |  |  |  |  |
| Designation | Syntax | Equations | Logipam | Matrix |
| Instantaneous output (pick-up) | P27R_x_1 | ■ | ■ |  |
| Delayed output | P27R_x_3 | $\square$ | $\square$ | $\square$ |
| Protection inhibited | P27R_x_16 | $\square$ | $\square$ |  |

$x$ : unit number.
(1) Under reference conditions (IEC 60255-6).

## Protection functions

Generator protection against insulation faults. This function should be combined with 59 N or 51 N to ensure $100 \%$ stator earth fault protection (64G).

## Description

Protection of generators against phase-to-earth insulation faults, by the detection of a reduction of the third harmonic residual voltage. This function protects 10 to $20 \%$ of the stator winding on the neutral point end. Complete protection of the stator winding is ensured by combining this function with function 59 N or 51 N , which protects 85 to $95 \%$ of the winding on the terminal end.

Due to their geometric characteristics, generators produce third-order harmonic voltages $(\mathrm{H} 3)$ in addition to the fundamental electromotive force. The amplitude of the H 3 voltage may vary from 0 to $10 \%$ of Vn , as a function of:

- network and generator characteristics

■ the load on the generator. It is generally higher under full-load conditions than under no-load conditions.
In the absence of a fault, the H 3 voltage must be at least $0.2 \%$ of Vn for protection function 27TN.

## H3 voltage with no fault

During normal operation, the H 3 voltage is measured at each end of the windings.


H3 voltage with a fault on the neutral point end
When a single-phase fault occurs in the stator winding near the machine neutral point, the neutral point impedance is short-circuited which leads to a drop in the H3 voltage on the neutral point end.


H3 voltage with a fault on the terminal end
When a single-phase fault occurs in the stator winding near the machine terminals, the H3 voltage increases on the neutral point end.


The third harmonic undervoltage protection function detects the drop in the H3 voltage caused by a single-phase fault on the neutral-point end.
Two types of tripping set points are available according to the sensors connected: $\square$ fixed set point: tripping for H 3 neutral point undervoltage. The setting requires preliminary measurements.
■ adaptive set point: tripping for H 3 neutral point undervoltage depending on a set point whose value depends on the H 3 residual voltage. The setting does not require preliminary measurements.
Availability of set points depending on the sensors used

| Voltage measurements |  | Available types |  |
| :--- | :--- | :--- | :--- |
| VT neutral point | VT terminals | 27TN fixed set point | 27TN adaptive set <br> point |
|  | All wiring | - | - |
| - | V1 or U21 | - | - |
| $\square$ | U21, U32 | $\square$ | - |
| $\square$ | V1, V2, V3 | $\square$ | $\square$ |
| $\square$ |  |  |  |



## Operation (fixed set point)

The DT delayed trip order is issued if the neutral point H3 voltage set point V3nt is less than the Vs set point.
The protection function operates only if the neutral point H3 voltage before the fault is greater than $0.2 \%$ of the network phase-to-neutral voltage.
The protection function is inhibited if the power produced by the generator is low or if the positive sequence voltage is insufficient.

## Adjustment

This function is adjusted according to a series of measurements on the neutral point H3 voltage of the generator. These measurements are used to determine the lowest H3 voltage value under normal operating conditions.
The measurements should be carried out:
■ under no-load conditions, not connected to the network
■ at a number of load levels because the H 3 voltage level depends on the load.
The parameter is set below the lowest H3 voltage value measured. The Sepam unit provides the neutral point H3 voltage measurement to facilitate adjustment of the protection function.

## Block diagram



## Characteristics

| Settings |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Type of set point |  |  |  |  |
| Setting range Fixed |  |  |  |  |
| Third harmonic voltage set point Vs |  |  |  |  |
| Setting range | 0.2 to $20 \%$ of Vntp |  |  |  |
| Accuracy ${ }^{(1)}$ | $\pm 5 \%$ or $\pm 0.05 \mathrm{~V}$ of neutral point Vnts |  |  |  |
| Resolution | 0.1 \% |  |  |  |
| Drop out/pick up ratio | 105 \% |  |  |  |
| Time delay |  |  |  |  |
| Setting range | 0.5 to 300 s |  |  |  |
| Accuracy ${ }^{(1)}$ | $\pm 2 \%$ or from -10 ms to +25 ms |  |  |  |
| Resolution | 10 ms or 1 digit |  |  |  |
| Advanced settings |  |  |  |  |
| Ssmin set point |  |  |  |  |
| Setting range | $1 \%$ to $90 \%$ of $\sqrt{3}$.Unp.lb |  |  |  |
| Accuracy ${ }^{(1)}$ | $\pm 5$ \% |  |  |  |
| Resolution | 1 \% |  |  |  |
| Drop out/pick up ratio | 105 \% |  |  |  |
| Vdsmin positive sequence undervoltage set point |  |  |  |  |
| Setting range | $50 \%$ to $100 \%$ of Unp |  |  |  |
| Accuracy ${ }^{(1)}$ | $\pm 5 \%$ |  |  |  |
| Resolution | 1 \% |  |  |  |
| Drop out/pick up ratio | 105 \% |  |  |  |
| Characteristic times ${ }^{(1)}$ |  |  |  |  |
| Operation time | typically 140 ms from 2 Vs to 0 |  |  |  |
| Overshoot time | < 65 ms |  |  |  |
| Reset time | < 65 ms |  |  |  |
| Inputs |  |  |  |  |
| Designation | Syntax | Equations Logipam |  |  |
| Protection reset | P27TN/64G2_x_101 ■ ■ |  |  |  |
| Protection inhibition |  |  |  |  |
| Outputs |  |  |  |  |
| Designation | Syntax | Equations | Logipam | Matrix |
| Tripping output | P27TN/64G2_x_3 | ■ | - | $\square$ |
| Protection inhibited | P27TN/64G2_x_16 | $\square$ | - |  |
| Instantaneous output | P27TN/64G2_x_23 | $\square$ | $\square$ |  |
| $x$ : unit number. <br> (1) Under reference | 60255-6). |  |  |  |



## Operation (adaptive set point)

The H 3 voltage (terminal end) $\mathrm{V} 3 \mathrm{r} \mathrm{\Sigma}$ is compared to the H 3 voltage V 3 nt measured on the neutral point end. The protection function calculates the H 3 residual voltage using the three phase-to-neutral voltages. Use of the H 3 residual voltage is the means to adapt the tripping set point according to the normal H3 voltage level. Time-delayed definite time (DT) tripping occurs when:


The protection function operates only if the neutral point H 3 voltage before the fault is greater than $0.2 \%$ of the network phase-to-neutral voltage and if the positive sequence voltage is greater than $30 \%$ of the phase-to-neutral voltage.

## Adjustment

This function does not require any particular measurements but, in certain cases, it may be necessary to adjust the K setting.
The Sepam unit measures the neutral point H3 voltage V3nt and the H3 residual voltage $\mathrm{V} 3 \mathrm{r} \sum$ to facilitate adjustment of the protection function.

- V3nt is expressed in \% of the primary voltage of the neutral point sensor Vntp
- V3r $\Sigma$ is expressed in \% of the primary voltage of the terminal-side sensors Vnp. If the primary voltages of the sensors are different, V3nt must be adapted to the terminal-side primary voltage Vnp using the equation:
V3nt (\%Vnp) $=$ V3nt (\%Vntp) $\times \frac{\text { Vntp }}{\text { Vnp }}$
Block diagram



## Characteristics

| Settings |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Type of set point |  |  |  |  |
| Setting range | Adaptive |  |  |  |
| Time delay |  |  |  |  |
| Setting range | 0.5 to 300 s |  |  |  |
| Accuracy ${ }^{(1)}$ | $\pm 2 \%$ or from -10 ms | to +25 ms |  |  |
| Resolution | 10 ms or 1 digit |  |  |  |
| Advanced settings |  |  |  |  |
| K set point |  |  |  |  |
| Setting range | 0.1 to 0.2 |  |  |  |
| Accuracy (1) | $\pm 1$ \% |  |  |  |
| Resolution | 0.01 |  |  |  |
| Drop out/pick up ratio | 105 \% |  |  |  |
| Characteristic times ${ }^{(1)}$ |  |  |  |  |
| Operation time | typically $140 \mathrm{~ms}{ }^{(2)}$ |  |  |  |
| Overshoot time | < 65 ms |  |  |  |
| Reset time | < 65 ms |  |  |  |
| Inputs |  |  |  |  |
| Designation | Syntax | Equations | Logipam |  |
| Protection reset | P27TN/64G2_x_101 | - | $\square$ |  |
| Protection inhibition | P27TN/64G2_x_113 | - | ■ |  |
| Outputs |  |  |  |  |
| Designation | Syntax | Equations | Logipam | Matrix |
| Tripping output | P27TN/64G2_x_3 | ■ | - | - |
| Protection inhibited | P27TN/64G2_x_16 | - | - |  |
| Instantaneous output | P27TN/64G2_x_23 | $\square$ | $\square$ |  |

(1) Under reference conditions (IEC 60255-6).
(2) Measured for a variation of $2 V 3 n$ t to 0 with V3r $\Sigma=30 \%$.

Curves $\frac{K}{3(1-K)} \times \mid$ V3r $\Sigma \mid$
Table with maximum values of V3nt (\%Vnp)

| V3r $\Sigma$ (\%Vnp) | K 0.10 | 0.11 | 0.12 | 0.13 | 0.14 | 0.15 | 0.16 | 0.17 | 0.18 | 0.19 | 0.20 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 0.04 | 0.04 | 0.05 | 0.05 | 0.05 | 0.06 | 0.06 | 0.07 | 0.07 | 0.08 | 0.08 |
| 2 | 0.07 | 0.08 | 0.09 | 0.10 | 0.11 | 0.12 | 0.13 | 0.14 | 0.15 | 0.16 | 0.17 |
| 3 | 0.11 | 0.12 | 0.14 | 0.15 | 0.16 | 0.18 | 0.19 | 0.20 | 0.22 | 0.23 | 0.25 |
| 4 | 0.15 | 0.16 | 0.18 | 0.20 | 0.22 | 0.24 | 0.25 | 0.27 | 0.29 | 0.31 | 0.33 |
| 5 | 0.19 | 0.21 | 0.23 | 0.25 | 0.27 | 0.29 | 0.32 | 0.34 | 0.37 | 0.39 | 0.42 |
| 6 | 0.22 | 0.25 | 0.27 | 0.30 | 0.33 | 0.35 | 0.38 | 0.41 | 0.44 | 0.47 | 0.50 |
| 7 | 0.26 | 0.29 | 0.32 | 0.35 | 0.38 | 0.41 | 0.44 | 0.48 | 0.51 | 0.55 | 0.58 |
| 8 | 0.30 | 0.33 | 0.36 | 0.40 | 0.43 | 0.47 | 0.51 | 0.55 | 0.59 | 0.53 | 0.67 |
| 9 | 0.33 | 0.37 | 0.41 | 0.45 | 0.49 | 0.53 | 0.57 | 0.61 | 0.66 | 0.70 | 0.75 |
| 10 | 0.37 | 0.41 | 0.45 | 0.50 | 0.54 | 0.59 | 0.63 | 0.68 | 0.73 | 0.78 | 0.83 |
| 15 | 0.56 | 0.62 | 0.68 | 0.75 | 0.81 | 0.88 | 0.95 | 1.02 | 1.10 | 1.17 | 1.25 |
| 20 | 0.74 | 0.82 | 0.91 | 1.00 | 1.09 | 1.18 | 1.27 | 1.37 | 1.46 | 1.56 | 1.67 |
| 25 | 0.93 | 1.03 | 1.14 | 1.25 | 1.36 | 1.47 | 1.59 | 1.71 | 1.83 | 1.95 | 2.08 |
| 30 | 1.11 | 1.24 | 1.36 | 1.49 | 1.63 | 1.76 | 1.90 | 2.05 | 2.20 | 2.35 | 2.50 |
| 40 | 1.48 | 1.65 | 1.82 | 1.99 | 2.17 | 2.35 | 2.54 | 2.73 | 2.93 | 3.13 | 3.33 |
| 50 | 1.85 | 2.06 | 2.27 | 2.49 | 2.71 | 2.94 | 3.17 | 3.41 | 3.66 | 3.91 | 4.17 |
| 60 | 2.22 | 2.47 | 2.73 | 2.99 | 3.26 | 3.53 | 3.81 | 4.10 | 4.39 | 4.69 | 4.10 |
| 70 | 2.59 | 2.88 | 3.18 | 3.49 | 3.80 | 4.12 | 4.44 | 4.78 | 5.12 | 5.47 | 5.83 |
| 80 | 2.96 | 3.30 | 3.64 | 3.98 | 4.34 | 4.71 | 5.08 | 5.46 | 5.85 | 6.26 | 6.67 |
| 90 | 3.33 | 3.71 | 4.09 | 4.48 | 4.88 | 5.29 | 5.71 | 6.14 | 6.59 | 7.04 | 7.50 |

V3nt/Vnp $\times 100$


## Protection functions

## Directional active overpower ANSI code 32P

## Protection against reverse power and overloads.

## Description

Two-way protection based on calculated active power, for the following applications:

- active overpower protection to detect overloads and allow load shedding
■ reverse active power protection:
$\square$ against generators running like motors when the generators draw active power $\square$ against motors running like generators when the motors supply active power.


Operating zone.

The protection function picks up if the active power flowing in one direction or the other (supplied or drawn) is greater than the Ps set point.
It includes a definite time delay T .
It is based on the two or three-wattmeter method, depending on the connection conditions:
■ V1, V2, V3 and I1, I2, I3: 3 wattmeters

- V1, V2, V3 and I1, I3: 2 wattmeters
- U21, U32 + V0 and I1, I2, I3: 3 wattmeters

■ U21, U32 + V0 and I1, I3: 2 wattmeters
■ U21, U32 without V0: 2 wattmeters

- other cases: protection function unavailable.

The function is enabled only if the following condition is met:
$P \geqslant 3.1 \% Q$ which provides a high level of sensitivity and high stability in the event of short-circuits.
The power sign is determined according to the general feeder or incomer parameter, according to the convention:

- for the feeder circuit:
- power supplied by the busbars is positive
$\square$ power supplied to the busbar is negative
- for the incomer circuit:
- power supplied to the busbar is positive
$\square$ power supplied by the busbars is negative.


## Block diagram



## Characteristics

| Settings |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Tripping direction |  |  |  |  |
| Setting range | Overpower/reverse power |  |  |  |
| Ps set point |  |  |  |  |
| Setting range | $1 \%$ of $\mathrm{Sn}^{(2)}$ to $120 \%$ of $\mathrm{Sn}{ }^{(2)}$ |  |  |  |
| Accuracy ${ }^{(1)}$ | $\pm 0.3 \% \mathrm{Sn}$ for Ps between $1 \% \mathrm{Sn}$ and $5 \% \mathrm{Sn}$ <br> $\pm 5 \%$ for Ps between $5 \% \mathrm{Sn}$ and $40 \% \mathrm{Sn}$ <br> $\pm 3 \%$ for Ps between $40 \% \mathrm{Sn}$ and $120 \% \mathrm{Sn}$ |  |  |  |
| Resolution | 0.1 kW |  |  |  |
| Drop out/pick up ratio | $93.5 \% \pm 5 \%$ or > (1-0.004 Sn/Ps) x $100 \%$ |  |  |  |
| Time delay T |  |  |  |  |
| Setting range | 100 ms to 300 s |  |  |  |
| Accuracy ${ }^{(1)}$ | $\pm 2 \%$ or -10 ms to +25 ms |  |  |  |
| Resolution | 10 ms or 1 digit |  |  |  |
| Characteristic times |  |  |  |  |
| Operation time | $<90 \mathrm{~ms}$ at 2 Ps |  |  |  |
| Overshoot time | $<40 \mathrm{~ms}$ at 2 Ps |  |  |  |
| Reset time | $<105 \mathrm{~ms}$ at 2 Ps |  |  |  |
| Inputs |  |  |  |  |
| Designation | Syntax | Equations | Logipam |  |
| Protection reset | P32P_x_101 | - | $\square$ |  |
| Protection inhibition | P32P_x_113 | - | $\square$ |  |
| Outputs |  |  |  |  |
| Designation | Syntax | Equations | Logipam | Matrix |
| Instantaneous output (pick-up) | P32P_x_1 | ■ | $\square$ |  |
| Delayed output | P32P_x_3 | $\square$ | $\square$ | - |
| Protection inhibited | P32P_x_16 | - | $\square$ |  |
| Positive active power | P32P_x_19 | $\square$ | $\square$ |  |
| Negative active power | P32P_x_20 | - | $\square$ |  |
| $x$ : unit number. <br> (1) Under reference conditions <br> (2) $S n=\sqrt{3} U n I n$. |  |  |  |  |

## Protection against field loss on synchronous

 machines.
## Description

Two-way protection based on calculated reactive power to detect field loss on synchronous machines: - reactive overpower protection for motors which consume more reactive power following field loss - reactive power feedback protection for protecting generators which consume more reactive power following field loss.

The protection function picks up if the reactive power flowing in one direction or the other (supplied or drawn) is greater than the Qs set point.
It includes a definite time delay T .
It is based on the two or three-wattmeter method, depending on the connection conditions:
■ V1, V2, V3 and I1, I2, I3: 3 wattmeters

- V1, V2, V3 and I1, I3: 2 wattmeters
- U21, U32 + V0 and I1, I2, I3: 3 wattmeters
- U21, U32 + V0 and I1, I3: 2 wattmeters
- U21, U32 without V0: 2 wattmeters
- other cases: protection function unavailable.

The function is enabled only if the following condition is met:
$Q \geqslant 3.1 \% \mathrm{P}$ which provides a high level of sensitivity and high stability in the event of short-circuits.
Assuming the wiring is the same, the power sign is determined according to the general feeder or incomer parameter, according to the convention:

- for the feeder circuit:
- power supplied by the busbars is positive
- power supplied to the busbar is negative
- for the incomer circuit:
- power supplied to the busbar is positive
$\square$ power supplied by the busbars is negative.


Block diagram


Characteristics

| Settings |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Tripping direction |  |  |  |  |
| Setting range | Overpower/reverse power |  |  |  |
| Qs set point |  |  |  |  |
| Setting range | $5 \%$ of $\mathrm{Sn}{ }^{(2)}$ to $120 \%$ of $\mathrm{Sn}{ }^{(2)}$ |  |  |  |
| Accuracy ${ }^{1{ }^{1}}$ | $\pm 5 \%$ for Qs between $5 \% \mathrm{Sn}$ and $40 \% \mathrm{Sn}$ <br> $\pm 3 \%$ for Qs between $40 \% \mathrm{Sn}$ and $120 \% \mathrm{Sn}$ |  |  |  |
| Resolution | 0.1 kW |  |  |  |
| Drop out/pick up ratio | $93.5 \% \pm 5 \%$ or > (1-0.004 Sn/Qs) $\times 100 \%$ |  |  |  |
| Time delay T |  |  |  |  |
| Setting range | 100 ms to 300 s |  |  |  |
| Accuracy ${ }^{(1)}$ | $\pm 2 \%$ or -10 ms to +25 ms |  |  |  |
| Resolution | 10 ms or 1 digit |  |  |  |
| Characteristic times |  |  |  |  |
| Operation time | $<90 \mathrm{~ms}$ at 2 Qs |  |  |  |
| Overshoot time | $<95 \mathrm{~ms}$ at 2 Qs |  |  |  |
| Reset time | $<95 \mathrm{~ms}$ at 2 Qs |  |  |  |
| Inputs |  |  |  |  |
| Designation | Syntax Equations Logipam |  |  |  |
| Protection reset | P32Q_1_101 | ■ | $\square$ |  |
| Protection inhibition | P32Q_1_113 ■ ■ |  |  |  |
| Outputs |  |  |  |  |
| Designation | Syntax | Equations | Logipam | Matrix |
| Instantaneous output (pick-up) | P32Q_1_1 | ■ | $\square$ |  |
| Delayed output | P32Q_1_3 | $\square$ | $\square$ | ■ |
| Protection inhibited | P32Q_1_16 | $\square$ | $\square$ |  |
| Positive reactive power | P32Q_1_54 | $\square$ | $\square$ |  |
| Negative reactive power | P32Q_1_55 | $\square$ | $\square$ |  |

(1) Under reference conditions (IEC 60255-6).
(2) $S n=\sqrt{3}$.Un.In.

## Protection functions

Phase undercurrent ANSI code 37

Protection for pumps.

## Description

Protection of pumps against the consequences of a loss of priming by detection of motor no-load operation.

This protection is single-phase.
■ it picks up when phase 1 current (I1) drops below the Is set point.


■ it is inactive when the current is less than $1.5 \%$ of $\ln$.

- it is insensitive to current drops due to circuit breaker tripping.


Pick-up
signal $=0$
Delayed
output =
Circuit breaker tripping.

- the protection function includes a definite time delay.


This protection function may be inhibited by a logic input. It can be remotely reset by a remote control order (TC32).

Block diagram


| Characteristics |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Settings |  |  |  |  |
| Is set point |  |  |  |  |
| Setting range | 5 \% lb to 100 \% lb |  |  |  |
| Accuracy ${ }^{(1)}$ | $\pm 5 \%$ |  |  |  |
| Resolution | 1 \% |  |  |  |
| Drop out/pick up ratio | $106 \% \pm 3$ \% |  |  |  |
| Time delay $\mathbf{T}$ |  |  |  |  |
| Setting range | 50 ms to 300 s |  |  |  |
| Accuracy ${ }^{(1)}$ | $\pm 2 \%$ or $\pm 25 \mathrm{~ms}$ |  |  |  |
| Resolution | 10 ms or 1 digit |  |  |  |
| Characteristic times |  |  |  |  |
| Operation time | pick-up < 55 ms from 2 Is to 0.02 ln |  |  |  |
| Overshoot time | $<40 \mathrm{~ms}$ from 2 Is to 0.02 ln |  |  |  |
| Reset time | $<45 \mathrm{~ms}$ from 0.02 In to 2 Is |  |  |  |
| Inputs |  |  |  |  |
| Designation | Syntax | Equations Logipam |  |  |
| Protection reset | P37_1_101 | ■ |  |  |
| Protection inhibition | P37_1_113 | ■ |  |  |
| Outputs |  |  |  |  |
| Designation | Syntax | Equations | Logipam | Matrix |
| Instantaneous output (pick-up) | P37_1_1 | ■ | - |  |
| Delayed output | P37_1_3 | $\square$ | $\square$ | - |
| Protection inhibited | P37_1_16 | $\square$ | $\square$ |  |
| (1) Under reference conditions (IEC 60255-6). |  |  |  |  |
| TS/TC equivalence for each protocol |  |  |  |  |
| Modbus DNP3 | IEC 60870-5-103 | IEC 61 |  |  |
| TC Binary Output | ASDU, FUN, INF | LN.DO |  |  |
| TC32 BO13 | 20, 105, 101 | A37_P | UC.ProRs.c | tlVal |

## Protection functions

## Directional active underpower

 ANSI code 37PCheck on active power flow.


Tripping zone (normal direction).


Tripping zone (reverse direction).

## Description

Two-way protection based on active power. The function monitors the calculated active power flows:

- to adapt the number of parallel sources to fit the network load power demand
- to create an isolated system in an installation with its own generating unit.

The protection function picks up if the active power flowing in one direction or the other (supplied or drawn) is less than the Ps set point.
It includes a definite (DT) time delay T.
It is based on the two or three-wattmeter method, depending on the connection conditions:

- V1, V2, V3 and I1, I2, I3: 3 wattmeters
- V1, V2, V3 and I1, I3: 2 wattmeters
- U21, U32 + V0 and I1, I2, I3: 3 wattmeters

■ U21, U32 + V0 and II, I3: 2 wattmeters
■ U21, U32 without V0: 2 wattmeters

- other cases: protection function unavailable.

The power sign is determined according to the general feeder or incomer parameter, according to the convention:

- for the feeder circuit:
$\square$ power supplied by the busbars is positive (normal direction)
$\square$ power supplied to the busbars is negative



## Block diagram



## Characteristics

| Settings |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Tripping direction |  |  |  |  |
| Setting range | Normal / reverse |  |  |  |
| Ps set point |  |  |  |  |
| Setting range | $5 \%$ of $\mathrm{Sn}{ }^{(2)}$ to $100 \%$ of $\mathrm{Sn}{ }^{(2)}$ |  |  |  |
| Accuracy ${ }^{11}$ | $\pm 5 \%$ for Ps between $5 \% \mathrm{Sn}$ and $40 \% \mathrm{Sn}$ $\pm 3 \%$ for Ps between $40 \% \mathrm{Sn}$ and $120 \% \mathrm{Sn}$ |  |  |  |
| Resolution | 0.1 kW |  |  |  |
| Drop out/pick up ratio | 106 \% |  |  |  |
| Time delay $\mathbf{T}$ |  |  |  |  |
| Setting range | 100 ms to 300 s |  |  |  |
| Accuracy ${ }^{(1)}$ | $\pm 2 \%$ or -10 ms to +25 ms |  |  |  |
| Resolution | 10 ms or 1 digit |  |  |  |
| Characteristic times |  |  |  |  |
| Operation time | $<120 \mathrm{~ms}$ |  |  |  |
| Overshoot time | $<65 \mathrm{~ms}$ |  |  |  |
| Reset time | < 60 ms |  |  |  |
| Inputs |  |  |  |  |
| Designation | Syntax Equations Logipam |  |  |  |
| Protection reset | P37P_x_101 ■ ■ |  |  |  |
| Protection inhibition | P37P_x_113 ■ ■ |  |  |  |
| Outputs |  |  |  |  |
| Designation | Syntax | Equations | Logipam | Matrix |
| Instantaneous output (pick-up) | P37P_x_1 | ■ | - |  |
| Delayed output | P37P_x_3 | - | - | $\square$ |
| Protection inhibited | P37P_x_16 | - | $\square$ |  |

$x$ : unit number.
(1) Under reference conditions (IEC 60255-6).
(2) $S n=\sqrt{3} . U n$.In.

Protection against heat rise in equipment by measuring the temperature with a sensor.

## Description

Protection that detects abnormal heat rise by measuring the temperature inside equipment fitted with sensors:
■ transformer: protection of primary and secondary windings

- motor and generator: protection of stator windings and bearings.

This protection function is associated with an RTD of the Pt100 platinum (100 $\Omega$ at $0^{\circ} \mathrm{C}$ or $32^{\circ} \mathrm{F}$ ) or nickel (Ni100 or Ni120) type, in accordance with the IEC 60751 and DIN 43760 standards.
■ it picks up when the monitored temperature is greater than the Ts set point

- it has two independent set points:
- alarm set point
- tripping set point
- when the protection function is activated, it detects whether the RTD is shorted or disconnected:
ㅁ RTD shorting is detected if the measured temperature is less than $-35^{\circ} \mathrm{C}$ or $-31^{\circ} \mathrm{F}$ (measurement displayed ${ }^{* * * * * *) ~}$
- RTD disconnection is detected if the measured temperature is greater than $+205^{\circ} \mathrm{C}$ or $+401^{\circ} \mathrm{F}$ (measurement displayed "-****").
If an RTD fault is detected, the protection function is inhibited and its output relays are set to zero.
The "RTD fault" item is also made available in the control matrix and an alarm message is generated specifying the number of the MET148-2 module for the faulty RTD.


## Block diagram



Characteristics

| Settings |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Alarm and trip set points TS1, TS2 |  |  |  |  |
| Setting range | $0^{\circ} \mathrm{C}$ to $180^{\circ} \mathrm{C}$ | $32^{\circ} \mathrm{F}$ to $356^{\circ} \mathrm{F}$ |  |  |
| Accuracy ${ }^{(1)}$ | $\pm 1.5^{\circ} \mathrm{C}$ | $\pm 2.7^{\circ} \mathrm{F}$ |  |  |
| Resolution | $1^{\circ} \mathrm{C}$ | $1^{\circ} \mathrm{F}$ |  |  |
| Pick up / drop out difference | $3^{\circ} \mathrm{C}$ | $5.4{ }^{\circ} \mathrm{F}$ |  |  |
| Inputs |  |  |  |  |
| Designation | Syntax | Equations Logipam |  |  |
| Protection reset | P38/49T_x_101 | - |  |  |
| Protection inhibition | P38/49T_x_113 | - ■ |  |  |
| Outputs |  |  |  |  |
| Designation | Syntax | Equations | Logipam | Matrix |
| Protection output | P38/49T_x_3 | - | $\square$ | $\square$ |
| Alarm | P38/49T_x_10 | $\square$ | ■ | ■ |
| RTD fault | P38/49T_x_12 | $\square$ | ■ |  |
| Protection inhibited | P38/49T_x_16 | $\square$ | ■ |  |

x: unit number.
(1) Under reference conditions (IEC 60255-6).

Protection against field loss on synchronous machines or generators.

## Description

The protection function is made up of two circular tripping characteristics on the impedance plane ( $R, X$ ). It picks up when the positive sequence impedance $Z d$ enters one of the circular tripping characteristics.

$$
\vec{Z}_{\mathbf{d}}=\frac{\vec{V}_{\mathbf{d}}}{\overrightarrow{\mathrm{I} \mathbf{d}}}
$$



## Circular tripping characteristics

- Case of a generator incomer or motor feeder

|  | Circle 1 | Circle 2 |
| :--- | :--- | :--- |
| Centre | $\mathrm{C} 1=-(\mathrm{Xa}+\mathrm{Xb}) / 2$ | $\mathrm{C} 2=-(\mathrm{Xa}+\mathrm{Xc}) / 2$ |
| Radius | $\mathrm{R} 1=(\mathrm{Xb}-\mathrm{Xa}) / 2$ | $\mathrm{R} 2=(\mathrm{Xc}-\mathrm{Xa}) / 2$ |

- Case of a generator feeder or motor incomer:
the tripping characteristics are symmetrical with respect to the $R$ axis

|  | Circle 1 | Circle 2 |
| :--- | :--- | :--- |
|  | $\mathrm{C} 1=(\mathrm{Xa}+\mathrm{Xb}) / 2$ | $\mathrm{C} 2=(\mathrm{Xa}+\mathrm{Xc}) / 2$ |
| Centre | $\mathrm{R} 1=(\mathrm{Xb}-\mathrm{Xa}) / 2$ | $\mathrm{R} 2=(\mathrm{Xc}-\mathrm{Xa}) / 2$ |
| Radius |  |  |

## Block diagram




## SFT2841 setting help

The SFT2841 software includes a setting assistance function to calculate the values of $\mathrm{Xa}, \mathrm{Xb}$ and Xc according to the electrical characteristics of the machine (and transformer, when applicable).
Data used:
■ synchronous machine:

- synchronous reactance Xd in \%
- transient synchronous reactance $X^{\prime} d$ in \%
- transformer:
- winding 1 voltage Un1 in V/kV
- short-circuit voltage Usc in \%
- rated power in kVA/MVA
a copper losses in $\mathrm{k} \Omega / \mathrm{M} \Omega$
The proposed settings are circle 1 with a diameter Zn if $\mathrm{Xd} \geqslant 200 \%$ or a diameter $\mathrm{Xd} / 2$ in all other cases, and circle 2 with a diameter Xd .
The two circles are offset from zero by -X'd/2.
$\mathrm{Zn}=$ the rated machine impedance:
$\mathrm{Zn}=\frac{\mathrm{Un} 1}{\sqrt{3} \mathrm{I} b}$.


## Characteristics

| Settings |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Common point: Xa |  |  |  |  |
| Setting range | $0.02 \mathrm{Vn} / \mathrm{lb} \leqslant \mathrm{Xa} \leqslant 0.20 \mathrm{Vn} / \mathrm{lb}+187.5 \mathrm{k} \Omega$ or $0.001 \Omega$ |  |  |  |
| Accuracy ${ }^{(1)}$ | $\pm 5 \%$ |  |  |  |
| Resolution | 1 \% |  |  |  |
| Circle 1: Xb |  |  |  |  |
| Setting range | $0.20 \mathrm{Vn} / \mathrm{lb} \leqslant \mathrm{Xb} \leqslant 1.40 \mathrm{Vn} / \mathrm{lb}+187.5 \mathrm{k} \Omega$ |  |  |  |
| Accuracy ${ }^{(1)}$ | $\pm 5$ \% |  |  |  |
| Resolution | $0.001 \Omega$ or 1 digit |  |  |  |
| Drop out/pick up ratio | $105 \% \pm 3 \%$ of circle 1 diameter |  |  |  |
| Circle 2: Xc |  |  |  |  |
| Setting range | $0.60 \mathrm{Vn} / \mathrm{lb} \leqslant \mathrm{Xc} \leqslant 3 \mathrm{Vn} / \mathrm{lb}+187.5 \mathrm{k} \Omega$ |  |  |  |
| Accuracy ${ }^{(1)}$ | $\pm 5$ \% |  |  |  |
| Resolution | $0.001 \Omega$ or 1 digit |  |  |  |
| Drop out/pick up ratio | $105 \% \pm 3 \%$ of circle 2 diameter |  |  |  |
| T1 time: tripping time delay circle 1 |  |  |  |  |
| Setting range | $50 \mathrm{~ms} \leqslant \mathrm{~T} \leqslant 300 \mathrm{~s}$ |  |  |  |
| Accuracy ${ }^{(1)}$ | $\pm 2 \%$ or from -10 ms to +25 ms |  |  |  |
| Resolution | 10 ms or 1 digit |  |  |  |
| T2 time: tripping time delay circle 2 |  |  |  |  |
| Setting range | $100 \mathrm{~ms} \leqslant \mathrm{~T} \leqslant 300 \mathrm{~s}$ |  |  |  |
| Accuracy ${ }^{(1)}$ | $\pm 2 \%$ or from -10 ms to +25 ms |  |  |  |
| Resolution | 10 ms or 1 digit |  |  |  |
| Characteristic times ${ }^{(1)}$ |  |  |  |  |
| Operation time | Pick-up < 40 ms from 0 to C1 (typically 25 ms ) <br> Pick-up < 40 ms from 0 to C 2 (typically 25 ms ) |  |  |  |
| Overshoot time | $<50 \mathrm{~ms}$ |  |  |  |
| Reset time | $<50 \mathrm{~ms}$ (for T1 = 0) |  |  |  |
| Inputs |  |  |  |  |
| Designation | Syntax | Equations | Logipam |  |
| Protection reset | P40_1_101 | ■ | ■ |  |
| Protection inhibition | P40_1_113 | - | - |  |
| Outputs |  |  |  |  |
| Designation | Syntax | Equations | Logipam | Matrix |
| Instantaneous output (pick-up) | P40_1_1 | ■ | $\square$ |  |
| Delayed output | P40_1_3 | - | ■ | $\square$ |
| Protection inhibited | P40_1_16 | $\square$ | ■ |  |
| Instantaneous protection 1 (circle 1) | P40_1_23 | $\square$ | ■ |  |

(1) Under reference conditions (IEC 60255-6).

## Example 1. Synchronous generator

## Synchronous generator data

■ $\mathrm{S}=3.15 \mathrm{MVA}$

- Un1 $=6.3 \mathrm{kV}$
- $X d=233 \%$

■ X'd=21\%

## Protection setting

To set the protection function, it is necessary to calculate the rated generator impedance Zn:
■ lb $=\mathbf{S} /(\sqrt{3} . U n 1)=289 \mathrm{~A}$
$\square \mathbf{Z n}=$ Un1/ ( $\sqrt{3} . \mathrm{Ib})=12.586 \Omega$
Generally speaking, circle 1 is set with a diameter Zn , offset by $-X^{\prime} \mathrm{d} / 2$, and circle 2 is set with a diameter Xd , offset by $-\mathrm{X}^{\prime} \mathrm{d} / 2$ :
■ $\mathrm{Xa}=(\mathrm{X} \mathrm{d}(\%) / 200) \mathrm{Zn}=1.321 \Omega$
■ $\mathrm{Xb}=(\mathrm{X} \mathrm{d}(\%) / 200+\min (1, \mathrm{Xd} / 200)) \times Z n=15.984 \Omega$
■ $\mathrm{Xc}=(\mathrm{X} \mathrm{d}(\%) / 200+\mathrm{Xd} / 100) \mathrm{Zn}=30.646 \Omega$
The faults detected in circle 1 are violent field-loss faults that must be cleared rapidly. Circle 2 may concern faults other than field-loss faults and its tripping time is longer:

- T1 $=70 \mathrm{~ms}$
- $\mathrm{T} 2=500 \mathrm{~ms}$.


## Example 2. Generator-transformer unit applications

## Synchronous generator data

## - $\mathrm{Sg}=19 \mathrm{MVA}$

- Un2 $=5.5 \mathrm{kV}$
- Xd $=257 \%$
- X'd = 30 \%

Transformer data

- St = 30 MVA
- Un1 = $20 \mathrm{kV} / \mathrm{Un} 2=5.5 \mathrm{kV}$
- Usc $=7 \%$
- Pcu = 191 kW


## Protection setting

To set the protection function, it is necessary to calculate the rated generator impedance at voltage Un1:

- $\mathrm{lb}=\mathrm{Sg} /(\sqrt{3} \mathrm{Un} 1)=548 \mathrm{~A}$
- $\mathrm{Zn}=\mathrm{Un} 1 /(\sqrt{3} \mathrm{Ib})=21.071 \Omega$

The transformer impedance at voltage Un1 is:
$\mathrm{Zt}=\mathrm{Usc} / 100 .(\mathrm{Un} 1)^{2} / \mathrm{St}=0.933 \Omega$
The transformer resistance at voltage Un1 is:
Rt $=$ Pcu. $(\mathrm{Un} 1 / \mathrm{St})^{2}=0.085 \Omega$
The transformer reactance at voltage Un1 is:
$\mathbf{X t}=\sqrt{\mathbf{Z} \mathbf{t}^{2}-\mathbf{R t}^{2}}=\mathbf{0 , 9 2 9} \Omega$
Circle 1 is set with a diameter Zn , offset by $-\mathrm{X} \mathrm{d} / 2$ and the transformer reactance.
Circle 2 is set with a diameter Xd , offset by $-\mathrm{X}^{\prime} \mathrm{d} / 2$ and the transformer reactance.
■ $\mathbf{X a}=(X ' d(\%) / 200) Z n+X t=4.09 \Omega$
■ Xb $=(X ' d(\%) / 200+1) Z n+X t=25.161 \Omega$
■ Xc = (X'd(\%)/200 + Xd(\%)/100)Zn + Xt = $58.243 \Omega$
The faults detected in circle 1 are violent field-loss faults that must be cleared rapidly. Circle 2 may concern faults other than field-loss faults and its tripping time is longer:

- T1 $=70 \mathrm{~ms}$
- $\mathrm{T} 2=500 \mathrm{~ms}$.

Phase unbalance protection for lines and equipment.
$x$ : unit number.
(1) Under reference conditions (IEC 60255-6).
(2) Setting ranges in TMS (Time Multiplier Setting) mode:

Inverse (SIT) and IEC SIT/A: 0.034 to 0.336
Very inverse (VIT) and IEC VIT/B: 0.067 to 0.666
Very inverse (LTI) and IEC LTI/B: 0.008 to 0.075 Ext. inverse (EIT) and IEC EIT/C: 0.124 to 1.237
IEEE moderately inverse: 0.415 to 4.142
IEEE very inverse: 0.726 to 7.255
IEEE extremely inverse: 1.231 to 12.30 .

## Description

Protection against phase unbalance, detected by the measurement of negative sequence current
■ sensitive protection to detect 2-phase faults at the ends of long lines
■ protection of equipment against temperature rise, caused by an unbalanced power supply, phase inversion or loss of phase, and against phase current unbalance. This function picks up if the negative sequence component of phase currents is greater than the operation set point.
It is time-delayed. The time delay may be definite time or IDMT according to a standardized curve, a specially adapted Schneider curve or an $\mathrm{RI}^{2}$ curve for generator protection.

## Tripping curve

Schneider IDMT
IEC inverse time SIT / A
IEC very inverse time VIT or LTI / B
IEC extremely inverse time EIT / C
IEEE moderately inverse (IEC / D)
IEEE very inverse (IEC / E)
IEEE extremely inverse (IEC / F)
RI2 curve

## Block diagram



## Characteristics

Settings

| Measurement origin |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Setting range |  | Main channels (I) Additional channels (l') |  |  |
| Tripping curve |  |  |  |  |
| Setting range |  | See list above |  |  |
| Is set point |  |  |  |  |
| Setting range | definite time | $10 \%$ to $500 \%$ of lb or l'b |  |  |
|  | Schneider IDMT | $10 \%$ to $50 \%$ of lb or l'b |  |  |
|  | IEC or IEEE IDMT | $10 \%$ to $100 \%$ of lb or l'b |  |  |
|  | $\mathrm{RI}^{2}$ curve | $3 \%$ to $20 \%$ of lb or l'b |  |  |
| Accuracy ${ }^{\text {(1) }}$ |  | $\pm 5 \%$ or $\pm 0.004 \mathrm{ln}$ |  |  |
| Resolution |  | 1 \% |  |  |
| Drop out/pick up ratio |  | $93.5 \% \pm 5 \%$ or > (1-0.005 In/ls) $\times 100 \%$ |  |  |
| Time delay T |  |  |  |  |
| Setting range | definite time | $100 \mathrm{~ms} \leqslant \mathrm{~T} \leqslant 300 \mathrm{~s}$ |  |  |
|  | IDMT | $100 \mathrm{~ms} \leqslant \mathrm{~T} \leqslant 1 \mathrm{~s}$ or TMS ${ }^{(2)}$ |  |  |
| Accuracy ${ }^{(1)}$ | definite time | $\pm 2 \%$ or $\pm 25 \mathrm{~ms}$ |  |  |
|  | IDMT | $\pm 5 \%$ or $\pm 35 \mathrm{~ms}$ |  |  |
| Resolution |  | 10 ms or 1 digit |  |  |
| K ( $\mathbf{R}^{2}$ c curve only) |  |  |  |  |
| Setting range |  | 1 to 100 |  |  |
| Resolution |  | 1 |  |  |
| Characteristic times |  |  |  |  |
| Operation time |  | Pick-up $<55 \mathrm{~ms}$ at 2 Is |  |  |
| Overshoot time |  | $<50 \mathrm{~ms}$ at 2 Is |  |  |
| Reset time |  | $<55 \mathrm{~ms}$ at 2 Is |  |  |
| Inputs |  |  |  |  |
| Designation | Syntax | Equations | Logipam |  |
| Protection reset | P46_x_101 | $\square$ | ■ |  |
| Protection inhibition | P46_x_113 | - | ■ |  |
| Outputs |  |  |  |  |
| Designation | Syntax | Equations | Logipam | Matrix |
| Instantaneous output (pick-up) |  | ■ | - |  |
| Delayed output |  | $\square$ | $\square$ | ■ |
| Protection inhibited | P46_x_16 | - | - |  |


$R l^{2}$ curve.


Schneider curve.

## Setting example for $\mathrm{RI}^{2}$ curves

A generator can handle a certain level of negative sequence current on a continuous basis. The Is continuous level, indicated by the manufacturer, is generally between 5 and $10 \%$ of the base current lb.
Typical values are:

| Type of generator |  | li permissible (\% lb) |
| :--- | :--- | :--- |
| Salient poles | with amortisseur windings | 10 |
|  | without amortisseur windings | 5 |
| Cylindrical rotors | Indirectly cooled | 10 |
|  | $\frac{\mathrm{Sn} \leqslant 960 \mathrm{MVA}}{}$ | 8 |
|  | $960 \mathrm{MVA}<\mathrm{Sn} \leqslant 1200 \mathrm{MVA}$ | 6 |
|  | $1200 \mathrm{MVA}<\mathrm{Sn}$ | 5 |

Reference IEEE C37.102-1987.

When this current level is exceeded, the generator can handle a negative sequence current lifor a time td, corresponding to the following equation:

$$
\mathbf{t d}=\frac{K}{\left(\frac{\overrightarrow{\mathbf{i}}}{\mathbf{I b}}\right)^{2}}
$$

The K value is an adjustable constant that depends on the type of generator, generally between 1 and 40 . Typical values of $K$ are:

| Type of generator |  | K |
| :--- | :--- | :--- |
| Salient poles |  | 40 |
| Synchronous condenser |  | 30 |
| Cylindrical rotors | Indirectly cooled | 20 |
|  | $\boxed{S n} \leqslant 800 \mathrm{MVA}$ | 10 |
| $800 \mathrm{MVA}<\mathrm{Sn} \leqslant 1600 \mathrm{MVA}$ | $10-0.00625 .(\mathrm{MVA}-800)$ |  |

Reference IEEE C37.102-1987.

## Schneider IDMT curve

For $\mathrm{li}>\mathrm{Is}$, the time delay depends on the value of $\mathrm{li} / \mathrm{lb}$ ( lb : base current of the protected equipment defined when the general parameters are set).
T corresponds to the time delay for $\mathrm{l} / \mathrm{lb}=5$.
The tripping curve is defined according to the following equations:
■ for $\mathrm{Is} / \mathrm{lb} \leqslant \mathrm{li} / \mathrm{lb} \leqslant 0.5$
$t=\frac{3.19}{(\mathrm{Ii} / \mathrm{Ib})^{1.5}} \times \mathbf{T}$

■ for $0.5 \leqslant \mathrm{li} / \mathrm{lb} \leqslant 5$
$t=\frac{4.64}{(\mathrm{I} / \mathrm{Ib})^{0.96}} \times T$

- for li/lb > 0.5
$t=\mathbf{T}$.


## Determination of tripping time for different negative sequence current

 values for a given Schneider curve Use the table to find the value of $X$ that corresponds to the required negative sequence current. The tripping time is equal to XT .
## Example

given a tripping curve with the setting $\mathrm{T}=0.5 \mathrm{~s}$.
What is the tripping time at 0.6 lb ?
Use the table to find the value of $X$ that corresponds to $60 \%$ of lb.
The table indicates $X=7.55$. The tripping time is equal to: $0.5 \times 7.55=3.755 \mathrm{~s}$.

## Schneider IDMT tripping curve



| $\mathbf{l i}(\%$ lb $)$ | 10 | 15 | 20 | 25 | 30 | 33.33 | 35 | 40 | 45 | 50 | 55 | 57.7 | 60 | 65 | 70 | 75 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| $\mathbf{X}$ | 99.95 | 54.50 | 35.44 | 25.38 | 19.32 | 16.51 | 15.34 | 12.56 | 10.53 | 9.00 | 8.21 | 7.84 | 7.55 | 7.00 | 6.52 | 6.11 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| $\mathbf{l i}(\%$ lb) cont. | 80 | 85 | 90 | 95 | 100 | 110 | 120 | 130 | 140 | 150 | 160 | 170 | 180 | 190 | 200 | 210 |
| $\mathbf{X}$ cont. | 5.74 | 5.42 | 5.13 | 4.87 | 4.64 | 4.24 | 3.90 | 3.61 | 3.37 | 3.15 | 2.96 | 2.80 | 2.65 | 2.52 | 2.40 | 2.29 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| $\mathbf{l i}(\%$ lb) cont. | 220 | 230 | 240 | 250 | 260 | 270 | 280 | 290 | 300 | 310 | 320 | 330 | 340 | 350 | 360 | 370 |
| $\mathbf{X}$ cont. | 2.14 | 2.10 | 2.01 | 1.94 | 1.86 | 1.80 | 1.74 | 1.68 | 1.627 | 1.577 | 1.53 | 1.485 | 1.444 | 1.404 | 1.367 | 1.332 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| $\mathbf{l i}(\%$ lb) cont. | 380 | 390 | 400 | 410 | 420 | 430 | 440 | 450 | 460 | 470 | 480 | 490 | $\geqslant 500$ |  |  |  |
| $\mathbf{X}$ cont. | 1.298 | 1.267 | 1.236 | 1.18 | 1.167 | 1.154 | 1.13 | 1.105 | 1.082 | 1.06 | 1.04 | 1.02 | 1 |  |  |  |

## Description

Protection against phase unbalance resulting from phase inversion, unbalanced supply or distant fault, detected by the measurement of negative sequence voltage Vi.

It includes a definite time delay T .
It does not operate when only one voltage is connected to Sepam.

## Block diagram



## Characteristics

| Settings |
| :--- | :--- | :--- | :--- |
| Measurement origin |
| Setting range |
| Vsi set point |$\quad$ Main channels (U) / Additional channels (U')

x: unit number
(1) Under reference conditions (IEC 60255-6).

## Excessive starting time, locked rotor <br> ANSI code 48/51LR

Detection of excessive starting time and locked rotors for motor protection.


Case of normal starting.



Case of locked rotor.


## Description

Protection against motor overheating caused by:
■ excessive motor starting time due to overloads (e.g. conveyor) or insufficient supply voltage
■ locked rotor due to motor load (e.g. crusher):
$\square$ during normal operation, after a normal start
a directly at motor start, before detection of an excessive starting time.
This function is three-phase.
Starting is detected when the current drawn is greater than $5 \%$ of current lb.
This function comprises two parts:
■ excessive starting time: during starting, the protection picks up when one of the 3 phase currents is greater than the set point Is for a longer period of time than the ST time delay (normal starting time)

- locked rotor:
- during normal operation (after starting), the protection picks up when one of the 3 phase currents is greater than the set point Is for a longer period of time than the LT time delay (DT).
- locked on start: large motors may have very long starting times, due to their inertia or a reduction in the voltage. This starting time may be longer than the permissible rotor locking time. To protect such a motor against rotor locking, an LTS time may be set to initiate tripping if a start is detected ( $\mathrm{I}>\mathrm{Is}$ ) and if the motor speed is zero.
Zero motor speed is detected by one of the three following options:
- Rotor rotation detection logic input from a zero speed sensor
- minimum speed function (ANSI 14)
- motor thermal overload function (ANSI 49)


## Motor re-acceleration

During re-acceleration, the motor draws a level of current similar to the start-up current ( $>$ Is), but in this case the current did not first drop to a level under $5 \%$ of lb. The ST time delay, which corresponds to the normal starting time, can be reinitialised by a logic input or information from a logic equation or the Logipam program ("motor re-acceleration" input) and enables the user to:

- reinitialize the excessive starting time protection
- set the locked rotor protection LT time delay to a low value


## Block diagram



## Characteristics

| Settings |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Is set point |  |  |  |  |
| Setting range | 50 \% to $500 \%$ of lb |  |  |  |
| Accuracy ${ }^{(1)}$ | $\pm 5 \%$ |  |  |  |
| Resolution | 1 \% |  |  |  |
| Drop out/pick up ratio | 93.5 \% $\pm 5$ \% |  |  |  |
| Time delay T |  |  |  |  |
| Setting range | ST | 500 ms to 300 s |  |  |
|  | LT | 50 ms to 300 s |  |  |
|  | LTS | 50 ms to 300 s |  |  |
| Accuracy ${ }^{(1)}$ |  | $\pm 2 \%$ or $\pm 25 \mathrm{~ms}$ at 2 Is |  |  |
| Resolution |  | 10 ms |  |  |
| Inputs |  |  |  |  |
| Designation | Syntax | Equations | Logipam |  |
| Protection reset | P48/51LR_1_101 | ■ | ■ |  |
| Motor re-acceleration | P48/51LR_1_102 | - | $\square$ |  |
| Protection inhibition | P48/51LR_1_113 | - | ■ |  |
| Outputs |  |  |  |  |
| Designation | Syntax | Equations | Logipam | Matrix |
| Protection output | P48/51LR_1_3 | ■ | ■ | - |
| Locked rotor | P48/51LR_1_13 | - | - | - |
| Excessive starting time | P48/51LR_1_14 | $\square$ | $\square$ | $\square$ |
| Locked rotor at start-up | P48/51LR_1_15 | $\square$ | ■ | - |
| Protection inhibited | P48/51LR_1_16 | $\square$ | $\square$ |  |
| Starting in progress | P48/51LR_1_22 | $\square$ | $\square$ |  |
| (1) Under reference con | IEC 60255-6). |  |  |  |

Protection of cables against thermal damage caused by overloads.


## Description

This protection function is used to protect cables against overloads, based on measurement of the current drawn.
The current measured by the thermal protection is an RMS 3-phase current which takes into account harmonics up to number 13.
The highest current of the three phases I1, I2 and I3, subsequently called phase current Iph, is used to calculate the heat rise:
$I p h=\max (I 1, I 2, I 3)$.
The calculated heat rise, proportional to the square of the current drawn, depends on the current drawn and the previous temperature status. Under steady-state conditions, it is equal to:
$E=\left(\frac{\mathbf{I p h}}{\mathbf{I b}}\right)^{2} \times \mathbf{1 0 0}$ in \%
The protection function issues the trip order when the phase current is greater than the permissible current for the cable. The value of the base current lb must absolutely be less than the permissible current la. By default, we use $\mathrm{lb} \approx \mathrm{la} / 1.4$.
The protection tripping time is set by the time constant T .
Cold curve: $\frac{\mathbf{t}}{\mathbf{T}}=\ln \left(\frac{\left(\frac{\mathbf{I}}{\mathbf{I b}}\right)^{2}}{\left(\frac{\mathbf{I}}{\mathbf{I b}}\right)^{2}-\left(\frac{\mathbf{l a}}{\mathbf{l b}}\right)^{2}}\right)$ where In: natural logarithm.
Hot curve: $\quad \frac{\mathbf{t}}{\mathbf{T}}=\ln \left(\frac{\left(\frac{\mathbf{I}}{\mathbf{l b}}\right)^{2}-\mathbf{1}}{\left(\frac{\mathbf{I}}{\mathbf{l b}}\right)^{2}-\left(\frac{\mathbf{l a}}{\mathbf{l b}}\right)^{2}}\right)$ where In: natural logarithm.
The present heat rise is saved in the event of an auxiliary power failure.

## Block diagram



## User information

The following information is available for the user:
■ heat rise

- time before tripping (with constant current).

Characteristics

| Settings |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Permissible current la |  |  |  |  |
| Setting range | $<1$ to 1.73 lb |  |  |  |
| Accuracy ${ }^{(1)}$ | $\pm 2$ \% |  |  |  |
| Resolution | 1 A |  |  |  |
| Time constant T |  |  |  |  |
| Setting range | 1 min . to 600 min . |  |  |  |
| Resolution | 1 min . |  |  |  |
| Characteristic times ${ }^{(1)}$ |  |  |  |  |
| Operation time accuracy | $\pm 2 \%$ or $\pm 1 \mathrm{~s}$ |  |  |  |
| Inputs |  |  |  |  |
| Designation | Syntax | Equations | Logipam |  |
| Protection reset | P49RMS_1_101 | ■ | ■ |  |
| Protection inhibition | P49RMS_1_113 | - | ■ |  |
| Outputs |  |  |  |  |
| Designation | Syntax | Equations | Logipam | Matrix |
| Delayed output | P49RMS_1_3 | ■ | ■ | $\square$ |
| Alarm | P49RMS_1_10 | $\square$ | $\square$ | - |
| Inhibit closing | P49RMS_1_11 | $\square$ | $\square$ | $\square$ |
| Protection inhibited | P49RMS_1_16 | $\square$ | $\square$ |  |
| Hot state | P49RMS_1_18 | $\square$ | $\square$ |  |
| Inhibit thermal overload | P49RMS_1_32 | $\square$ | $\square$ |  |

(1) Under reference conditions (IEC 60255-6).


## Example

Consider a copper cable, $185 \mathrm{~mm}^{2}$, with a permissible current la $=485 \mathrm{~A}$ and a 1 - second thermal withstand lth_1s = 22.4 kA .
The thermal time constant of a cable depends in its installation method. Typical timeconstant values are between 10 and 60 minutes. For buried cables, the time constant is between 20 and 60 minutes, for non-buried cables, it is between 10 and 40 minutes.
For the cable in question, the selected values are $\mathrm{T}=30$ minutes and $\mathrm{lb}=350 \mathrm{~A}$.
Check on compatibility between the 49RMS curve and the adiabatic thermal withstand.
Conditions are correct at 10 lb .
In the range of currents close to the permissible current, the 1 -second thermal withstand is used to estimate maximum thermal withstand for the cable, assuming there are no heat exchanges. The maximum tripping time is calculated as:
$\mathbf{I}^{\mathbf{2}} \mathbf{x}$ tmax $=$ constant $=\left(\mathbf{I t h} \_\mathbf{1 s}\right)^{\mathbf{2}} \times 1$.
For the cable in question and at 10 lb :
tmax $=(\text { Ith_1 s/IOlb })^{2}=(22400 / 3500)^{2}=41 \mathrm{~s}$
For $\mathrm{I}=10 \mathrm{lb}=3500 \mathrm{~A}$ and $\mathrm{la} / \mathrm{lb}=1.38$, the value of k in the cold tripping curve table is $\mathrm{k} \approx 0.0184$.
The tripping time at 10 lb is therefore:
$\mathbf{t}=\mathbf{k} \times \mathbf{T} \mathbf{6 0} \mathbf{= 0 . 0 1 8 4 \times 3 0 \times 6 0 = 3 5 . 6 s < t m a x}$.
For a 10 lb fault occuring after a rated operation phase, with $100 \%$ heat rise, the value of $k$ is: $k \approx 0.0097$.
The tripping time is:
$\mathbf{t}=\mathbf{k x} \mathbf{T} \times 60=0.0097 \times 30 \times 60=17.5 \mathrm{~s}$

## Check on discrimination

Discrimination between 49RMS for the cable and the downstream protection curves, including 49RMS protection functions, must be checked to avoid any risk of nuisance tripping.

## Curves for initial heat rise $=\mathbf{0} \%$

| Iph/lb <br> la/lb |  | 0.60 | 0.65 | 0.70 | 0.75 | 0.80 | 0.85 | 0.90 | 0.95 | 1.00 | 1.05 | 1.10 | 1.15 | 1.20 | 1.25 | 1.30 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0.50 | 1.7513 | 1.1856 | 0.8958 | 0.7138 | 0.5878 | 0.4953 | 0.4247 | 0.3691 | 0.3244 | 0.2877 | 0.2572 | 0.2314 | 0.2095 | 0.1907 | 0.1744 | 0.1601 |
| 0.55 |  | 1.8343 | 1.2587 | 0.9606 | 0.7717 | 0.6399 | 0.5425 | 0.4675 | 0.4082 | 0.3603 | 0.3207 | 0.2877 | 0.2597 | 0.2358 | 0.2152 | 0.1972 |
| 0.60 |  |  | 1.9110 | 1.3269 | 1.0217 | 0.8267 | 0.6897 | 0.5878 | 0.5090 | 0.4463 | 0.3953 | 0.3531 | 0.3178 | 0.2877 | 0.2619 | 0.2396 |
| 0.65 |  |  |  | 1.9823 | 1.3907 | 1.0793 | 0.8789 | 0.7373 | 0.6314 | 0.5491 | 0.4832 | 0.4295 | 0.3849 | 0.3473 | 0.3153 | 0.2877 |
| 0.70 |  |  |  |  | 2.0488 | 1.4508 | 1.1338 | 0.9287 | 0.7829 | 0.6733 | 0.5878 | 0.5191 | 0.4629 | 0.4159 | 0.3763 | 0.3424 |
| 0.75 |  |  |  |  |  | 2.1112 | 1.5075 | 1.1856 | 0.9762 | 0.8267 | 0.7138 | 0.6253 | 0.5540 | 0.4953 | 0.4463 | 0.4047 |
| 0.80 |  |  |  |  |  |  | 2.1699 | 1.5612 | 1.2349 | 1.0217 | 0.8687 | 0.7527 | 0.6615 | 0.5878 | 0.5270 | 0.4759 |
| 0.85 |  |  |  |  |  |  |  | 2.2254 | 1.6122 | 1.2819 | 1.0652 | 0.9091 | 0.7904 | 0.6966 | 0.6206 | 0.5578 |
| 0.90 |  |  |  |  |  |  |  |  | 2.2780 | 1.6607 | 1.3269 | 1.1069 | 0.9480 | 0.8267 | 0.7306 | 0.6526 |
| 0.95 |  |  |  |  |  |  |  |  |  | 2.3279 | 1.7070 | 1.3699 | 1.1470 | 0.9855 | 0.8618 | 0.7636 |
| 1.00 |  |  |  |  |  |  |  |  |  |  | 2.3755 | 1.7513 | 1.4112 | 1.1856 | 1.0217 | 0.8958 |
| 1.05 |  |  |  |  |  |  |  |  |  |  |  | 2.4209 | 1.7937 | 1.4508 | 1.2228 | 1.0566 |
| 1.10 |  |  |  |  |  |  |  |  |  |  |  |  | 2.4643 | 1.8343 | 1.4890 | 1.2587 |
| 1.15 |  |  |  |  |  |  |  |  |  |  |  |  |  | 2.5060 | 1.8734 | 1.5258 |
| 1.20 |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 2.5459 | 1.9110 |
| 1.25 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 2.5844 |


| Iph/lb la/lb |  | 1.40 | 1.45 | 1.50 | 1.55 | 1.60 | 1.65 | 1.70 | 1.75 | 1.80 | 1.85 | 1.90 | 1.95 | 2.00 | 2.20 | 2.40 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0.50 | 0.1475 | 0.1365 | 0.1266 | 0.1178 | 0.1099 | 0.1028 | 0.0963 | 0.0905 | 0.0852 | 0.0803 | 0.0759 | 0.0718 | 0.0680 | 0.0645 | 0.0530 | 0.0444 |
| 0.55 | 0.1815 | 0.1676 | 0.1553 | 0.1444 | 0.1346 | 0.1258 | 0.1178 | 0.1106 | 0.1040 | 0.0980 | 0.0925 | 0.0875 | 0.0829 | 0.0786 | 0.0645 | 0.0539 |
| 0.60 | 0.2201 | 0.2029 | 0.1878 | 0.1744 | 0.1623 | 0.1516 | 0.1418 | 0.1330 | 0.1251 | 0.1178 | 0.1111 | 0.1051 | 0.0995 | 0.0943 | 0.0773 | 0.0645 |
| 0.65 | 0.2637 | 0.2428 | 0.2243 | 0.2080 | 0.1934 | 0.1804 | 0.1686 | 0.1581 | 0.1485 | 0.1397 | 0.1318 | 0.1245 | 0.1178 | 0.1116 | 0.0913 | 0.0762 |
| 0.70 | 0.3132 | 0.2877 | 0.2653 | 0.2456 | 0.2281 | 0.2125 | 0.1984 | 0.1858 | 0.1744 | 0.1640 | 0.1545 | 0.1459 | 0.1380 | 0.1307 | 0.1067 | 0.0889 |
| 0.75 | 0.3691 | 0.3383 | 0.3113 | 0.2877 | 0.2667 | 0.2481 | 0.2314 | 0.2165 | 0.2029 | 0.1907 | 0.1796 | 0.1694 | 0.1601 | 0.1516 | 0.1236 | 0.1028 |
| 0.80 | 0.4326 | 0.3953 | 0.3630 | 0.3347 | 0.3098 | 0.2877 | 0.2680 | 0.2503 | 0.2344 | 0.2201 | 0.2070 | 0.1952 | 0.1843 | 0.1744 | 0.1418 | 0.1178 |
| 0.85 | 0.5049 | 0.4599 | 0.4210 | 0.3873 | 0.3577 | 0.3316 | 0.3084 | 0.2877 | 0.2691 | 0.2523 | 0.2371 | 0.2233 | 0.2107 | 0.1992 | 0.1617 | 0.1340 |
| 0.90 | 0.5878 | 0.5332 | 0.4866 | 0.4463 | 0.4112 | 0.3804 | 0.3531 | 0.3289 | 0.3072 | 0.2877 | 0.2701 | 0.2541 | 0.2396 | 0.2263 | 0.1832 | 0.1516 |
| 0.95 | 0.6836 | 0.6170 | 0.5608 | 0.5127 | 0.4710 | 0.4347 | 0.4027 | 0.3744 | 0.3491 | 0.3265 | 0.3061 | 0.2877 | 0.2710 | 0.2557 | 0.2064 | 0.1704 |
| 1.00 | 0.7956 | 0.7138 | 0.6456 | 0.5878 | 0.5383 | 0.4953 | 0.4578 | 0.4247 | 0.3953 | 0.3691 | 0.3456 | 0.3244 | 0.3052 | 0.2877 | 0.2314 | 0.1907 |
| 1.05 | 0.9287 | 0.8267 | 0.7431 | 0.6733 | 0.6142 | 0.5633 | 0.5191 | 0.4804 | 0.4463 | 0.4159 | 0.3888 | 0.3644 | 0.3424 | 0.3225 | 0.2585 | 0.2125 |
| 1.10 | 1.0904 | 0.9606 | 0.8569 | 0.7717 | 0.7005 | 0.6399 | 0.5878 | 0.5425 | 0.5027 | 0.4675 | 0.4363 | 0.4082 | 0.3830 | 0.3603 | 0.2877 | 0.2358 |
| 1.15 | 1.2934 | 1.1231 | 0.9916 | 0.8862 | 0.7996 | 0.7269 | 0.6651 | 0.6118 | 0.5654 | 0.5246 | 0.4884 | 0.4563 | 0.4274 | 0.4014 | 0.3192 | 0.2609 |
| 1.20 | 1.5612 | 1.3269 | 1.1549 | 1.0217 | 0.9147 | 0.8267 | 0.7527 | 0.6897 | 0.6353 | 0.5878 | 0.5460 | 0.5090 | 0.4759 | 0.4463 | 0.3531 | 0.2877 |
| 1.25 | 1.9473 | 1.5955 | 1.3593 | 1.1856 | 1.0509 | 0.9425 | 0.8531 | 0.7780 | 0.7138 | 0.6583 | 0.6098 | 0.5671 | 0.5292 | 0.4953 | 0.3898 | 0.3165 |
| 1.30 | 2.6214 | 1.9823 | 1.6286 | 1.3907 | 1.2155 | 1.0793 | 0.9696 | 0.8789 | 0.8026 | 0.7373 | 0.6808 | 0.6314 | 0.5878 | 0.5491 | 0.4295 | 0.3473 |
| 1.35 |  | 2.6571 | 2.0161 | 1.6607 | 1.4212 | 1.2445 | 1.1069 | 0.9959 | 0.9041 | 0.8267 | 0.7604 | 0.7029 | 0.6526 | 0.6081 | 0.4725 | 0.3804 |
| 1.40 |  |  | 2.6915 | 2.0488 | 1.6918 | 1.4508 | 1.2727 | 1.1338 | 1.0217 | 0.9287 | 0.8502 | 0.7829 | 0.7245 | 0.6733 | 0.5191 | 0.4159 |
| 1.45 |  |  |  | 2.7249 | 2.0805 | 1.7220 | 1.4796 | 1.3001 | 1.1601 | 1.0467 | 0.9527 | 0.8733 | 0.8050 | 0.7458 | 0.5699 | 0.4542 |
| 1.50 |  |  |  |  | 2.7571 | 2.1112 | 1.7513 | 1.5075 | 1.3269 | 1.1856 | 1.0712 | 0.9762 | 0.8958 | 0.8267 | 0.6253 | 0.4953 |
| 1.55 |  |  |  |  |  | 2.7883 | 2.1410 | 1.7797 | 1.5347 | 1.3529 | 1.2106 | 1.0952 | 0.9992 | 0.9179 | 0.6859 | 0.5397 |
| 1.60 |  |  |  |  |  |  | 2.8186 | 2.1699 | 1.8074 | 1.5612 | 1.3783 | 1.2349 | 1.1185 | 1.0217 | 0.7527 | 0.5878 |
| 1.65 |  |  |  |  |  |  |  | 2.8480 | 2.1980 | 1.8343 | 1.5870 | 1.4031 | 1.2587 | 1.1414 | 0.8267 | 0.6399 |
| 1.70 |  |  |  |  |  |  |  |  | 2.8766 | 2.2254 | 1.8605 | 1.6122 | 1.4272 | 1.2819 | 0.9091 | 0.6966 |

## Curves for initial heat rise = 0 \%

| Iph/Ib la/lb |  | 2.80 | 3.00 | 3.20 | 3.40 | 3.60 | 3.80 | 4.00 | 4.20 | 4.40 | 4.60 | 4.80 | 5.00 | 5.50 | 6.00 | 6.50 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0,50 | 0.0377 | 0.0324 | 0.0282 | 0.0247 | 0.0219 | 0.0195 | 0.0175 | 0.0157 | 0.0143 | 0.0130 | 0.0119 | 0.0109 | 0.0101 | 0.0083 | 0.0070 | 0.0059 |
| 0.55 | 0.0458 | 0.0393 | 0.0342 | 0.0300 | 0.0265 | 0.0236 | 0.0212 | 0.0191 | 0.0173 | 0.0157 | 0.0144 | 0.0132 | 0.0122 | 0.0101 | 0.0084 | 0.0072 |
| 0.60 | 0.0547 | 0.0470 | 0.0408 | 0.0358 | 0.0316 | 0.0282 | 0.0252 | 0.0228 | 0.0206 | 0.0188 | 0.0172 | 0.0157 | 0.0145 | 0.0120 | 0.0101 | 0.0086 |
| 0.65 | 0.0645 | 0.0554 | 0.0481 | 0.0421 | 0.0372 | 0.0331 | 0.0297 | 0.0268 | 0.0242 | 0.0221 | 0.0202 | 0.0185 | 0.0170 | 0.0141 | 0.0118 | 0.0101 |
| 0.70 | 0.0752 | 0.0645 | 0.0560 | 0.0490 | 0.0433 | 0.0385 | 0.0345 | 0.0311 | 0.0282 | 0.0256 | 0.0234 | 0.0215 | 0.0198 | 0.0163 | 0.0137 | 0.0117 |
| 0.75 | 0.0869 | 0.0745 | 0.0645 | 0.0565 | 0.0499 | 0.0444 | 0.0397 | 0.0358 | 0.0324 | 0.0295 | 0.0269 | 0.0247 | 0.0228 | 0.0188 | 0.0157 | 0.0134 |
| 0.80 | 0.0995 | 0.0852 | 0.0738 | 0.0645 | 0.0570 | 0.0506 | 0.0453 | 0.0408 | 0.0370 | 0.0336 | 0.0307 | 0.0282 | 0.0259 | 0.0214 | 0.0179 | 0.0153 |
| 0.85 | 0.1130 | 0.0967 | 0.0837 | 0.0732 | 0.0645 | 0.0574 | 0.0513 | 0.0462 | 0.0418 | 0.0380 | 0.0347 | 0.0319 | 0.0293 | 0.0242 | 0.0203 | 0.0172 |
| 0.90 | 0.1276 | 0.1091 | 0.0943 | 0.0824 | 0.0726 | 0.0645 | 0.0577 | 0.0520 | 0.0470 | 0.0427 | 0.0390 | 0.0358 | 0.0329 | 0.0271 | 0.0228 | 0.0194 |
| 0.95 | 0.1433 | 0.1223 | 0.1057 | 0.0923 | 0.0813 | 0.0722 | 0.0645 | 0.0581 | 0.0525 | 0.0477 | 0.0436 | 0.0400 | 0.0368 | 0.0303 | 0.0254 | 0.0216 |
| 1.00 | 0.1601 | 0.1365 | 0.1178 | 0.1028 | 0.0905 | 0.0803 | 0.0718 | 0.0645 | 0.0584 | 0.0530 | 0.0484 | 0.0444 | 0.0408 | 0.0336 | 0.0282 | 0.0240 |
| 1.05 | 0.1780 | 0.1516 | 0.1307 | 0.1139 | 0.1002 | 0.0889 | 0.0794 | 0.0714 | 0.0645 | 0.0586 | 0.0535 | 0.0490 | 0.0451 | 0.0371 | 0.0311 | 0.0264 |
| 1.10 | 0.1972 | 0.1676 | 0.1444 | 0.1258 | 0.1106 | 0.0980 | 0.0875 | 0.0786 | 0.0711 | 0.0645 | 0.0589 | 0.0539 | 0.0496 | 0.0408 | 0.0342 | 0.0291 |
| 1.15 | 0.2177 | 0.1848 | 0.1589 | 0.1383 | 0.1215 | 0.1076 | 0.0961 | 0.0863 | 0.0779 | 0.0708 | 0.0645 | 0.0591 | 0.0544 | 0.0447 | 0.0374 | 0.0318 |
| 1.20 | 0.2396 | 0.2029 | 0.1744 | 0.1516 | 0.1330 | 0.1178 | 0.1051 | 0.0943 | 0.0852 | 0.0773 | 0.0705 | 0.0645 | 0.0593 | 0.0488 | 0.0408 | 0.0347 |
| 1.25 | 0.2629 | 0.2223 | 0.1907 | 0.1656 | 0.1452 | 0.1285 | 0.1145 | 0.1028 | 0.0927 | 0.0842 | 0.0767 | 0.0702 | 0.0645 | 0.0530 | 0.0444 | 0.0377 |
| 1.30 | 0.2877 | 0.2428 | 0.2080 | 0.1804 | 0.1581 | 0.1397 | 0.1245 | 0.1116 | 0.1007 | 0.0913 | 0.0832 | 0.0762 | 0.0700 | 0.0575 | 0.0481 | 0.0408 |
| 1.35 | 0.3142 | 0.2646 | 0.2263 | 0.1960 | 0.1716 | 0.1516 | 0.1349 | 0.1209 | 0.1091 | 0.0989 | 0.0901 | 0.0824 | 0.0757 | 0.0621 | 0.0520 | 0.0441 |
| 1.40 | 0.3424 | 0.2877 | 0.2456 | 0.2125 | 0.1858 | 0.1640 | 0.1459 | 0.1307 | 0.1178 | 0.1067 | 0.0972 | 0.0889 | 0.0816 | 0.0670 | 0.0560 | 0.0475 |
| 1.45 | 0.3725 | 0.3122 | 0.2661 | 0.2298 | 0.2007 | 0.1770 | 0.1574 | 0.1409 | 0.1269 | 0.1150 | 0.1047 | 0.0957 | 0.0878 | 0.0720 | 0.0602 | 0.0510 |
| 1.50 | 0.4047 | 0.3383 | 0.2877 | 0.2481 | 0.2165 | 0.1907 | 0.1694 | 0.1516 | 0.1365 | 0.1236 | 0.1124 | 0.1028 | 0.0943 | 0.0773 | 0.0645 | 0.0547 |
| 1.55 | 0.4391 | 0.3659 | 0.3105 | 0.2674 | 0.2330 | 0.2050 | 0.1820 | 0.1627 | 0.1464 | 0.1325 | 0.1205 | 0.1101 | 0.1010 | 0.0828 | 0.0691 | 0.0585 |
| 1.60 | 0.4759 | 0.3953 | 0.3347 | 0.2877 | 0.2503 | 0.2201 | 0.1952 | 0.1744 | 0.1568 | 0.1418 | 0.1290 | 0.1178 | 0.1080 | 0.0884 | 0.0738 | 0.0625 |
| 1.65 | 0.5154 | 0.4266 | 0.3603 | 0.3091 | 0.2686 | 0.2358 | 0.2089 | 0.1865 | 0.1676 | 0.1516 | 0.1377 | 0.1258 | 0.1153 | 0.0943 | 0.0786 | 0.0666 |
| 1.70 | 0.5578 | 0.4599 | 0.3873 | 0.3316 | 0.2877 | 0.2523 | 0.2233 | 0.1992 | 0.1789 | 0.1617 | 0.1469 | 0.1340 | 0.1229 | 0.1004 | 0.0837 | 0.0709 |


| lph/lb <br> la/lb |  | 7.50 | 8.00 | 8.50 | 9.00 | 9.50 | 10.00 | 12.50 | 15.00 | 17.50 | 20.00 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0.50 | 0.0051 | 0.004 | 0.003 | . 0035 | 0.003 | 0.002 | 0.0025 | 0.0016 | 0.001 | 0.0008 | 0.0006 |
| 0.55 | 0.0062 | 0.005 | 0.004 | 0.0042 | 0.003 | 0.003 | 0.0030 | 0.0019 | 0.0013 | 0.0010 | 0.0008 |
| 0.60 | 0.007 | 0.006 | 0.005 | . 005 | 0.00 | 0.004 | 0.003 | 0.002 | 0.0016 | 0.0012 | 0.0009 |
| 0.65 | 0.0087 | 0.0 | . 006 | 0.0059 | 0.0 | . 00 | 0.00 | 0.002 | 0.0019 | 0.00 | 0.0011 |
| 0.70 | 0.0101 | 0.0 | 0.00 | 0.0068 | 0.0 | 0.005 | 0.0 | 0.003 | 0.002 | 0.00 | 0.0012 |
| 0.75 | 0.0115 | 0.010 | 0.0088 | . 0078 | 0.007 | 0.0063 | 0.0056 | 0.003 | 0.0025 | 0.001 | 0.0014 |
| 0.80 | 0.0131 | 0.011 | 0.0101 | 0.0089 | 0.0079 | 0.0071 | 0.0064 | 0.0041 | 0.0028 | 0.0021 | 0.0016 |
| 0.85 | 0.0149 | 0.0129 | 0.0114 | 0.0101 | 0.0090 | 0.0080 | 0.0073 | 0.0046 | 0.0032 | 0.002 | 0.0018 |
| 0.90 | 0.0167 | 0.0145 | 0.0127 | 0.0113 | 0.0101 | 0.0090 | 0.0081 | 0.0052 | 0.0036 | 0.0026 | 0.0020 |
| 0.95 | 0.0186 | 0.016 | 0.014 | 0.0126 | 0.01 | 0.0101 | 0.0091 | 0.0058 | 0.0040 | 0.0030 | 0.0023 |
| 1.00 | 0.0206 | 0.017 | 0.015 | . 013 | 0.012 | 0.0111 | 0.0101 | 0.00 | 0.0045 | 0.0033 | 0.0025 |
| 1.05 | 0.0228 | 0.0198 | 0.017 | . 015 | 0.0137 | 0.0123 | 0.0111 | 0.007 | 0.0049 | 0.0036 | 0.0028 |
| 1.10 | 0.0250 | 0.0217 | 0.019 | 0.0169 | 0.015 | 0.0135 | 0.0122 | 0.007 | 0.0054 | 0.0040 | 0.0030 |
| 1.15 | 0.0274 | 0.0238 | 0.020 | 0.0185 | 0.016 | 0.0148 | 0.0133 | 0.008 | 0.0059 | 0.0043 | 0.0033 |
| 1.20 | 0.0298 | 0.025 | 0.022 | 0.0201 | 0.01 | 0.0161 | 0.0145 | 0.009 | 0.006 | 0.0047 | 0.0036 |
| 1.25 | 0.0324 | 0.028 | 0.024 | 0.0219 | 0.01 | 0.0175 | 0.015 | 0.010 | 0.007 | 0.005 | 0.0039 |
| 1.30 | 0.0351 | 0.0305 | 0.026 | . 0237 | 0.021 | 0.0189 | 0.017 | 0.010 | 0.0075 | 0.005 | 0.0042 |
| 1.35 | 0.0379 | 0.0329 | 0.028 | . 0255 | 0.022 | 0.020 | 0.018 | 0.01 | 0.0081 | 0.006 | 0.0046 |
| 1.40 | 0.0408 | 0.0355 | 0.031 | 275 | 0.024 | 0.0220 | 0.0198 | 0.012 | 0.0087 | 0.006 | 0.0049 |
| 1.45 | 0.0439 | 0.0381 | 0.0334 | 0.0295 | 0.0263 | 0.0236 | 0.0212 | 0.0135 | 0.0094 | 0.0069 | 0.0053 |
| 1.50 | 0.0470 | 0.0408 | 0.0358 | 0.0316 | 0.0282 | 0.0252 | 0.0228 | 0.0145 | 0.0101 | 0.0074 | 0.0056 |
| 1.55 | 0.0503 | 0.0437 | 0.0383 | 0.0338 | 0.0301 | 0.0270 | 0.0243 | 0.0155 | 0.0107 | 0.0079 | 0.0060 |
| 1.60 | 0.0537 | 0.0466 | 0.0408 | 0.0361 | 0.0321 | 0.0288 | 0.0259 | 0.0165 | 0.0114 | 0.0084 | 0.0064 |
| 1.65 | 0.0572 | 0.0496 | 0.0435 | 0.0384 | 0.0342 | 0.0306 | 0.0276 | 0.0176 | 0.0122 | 0.0089 | 0.0068 |
| 1.70 | 0.0608 | 0.0527 | 0.0462 | 0.0408 | 0.0363 | 0.0325 | 0.0293 | 0.0187 | 0.0129 | 0.0095 | 0.0073 |

## Curves for initial heat rise = $\mathbf{1 0 0} \%$

| Iph/lb la/lb |  | 1.20 | 1.25 | 1.30 | 1.35 | 1.40 | 1.45 | 1.50 | 1.55 | 1.60 | 1.65 | 1.70 | 1.75 | 1.80 | 1.85 | 1.90 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1.10 | 1.0531 | 0.6487 | 0.4673 | 0.3629 | 0.2948 | 0.2469 | 0.2113 | 0.1839 | 0.1622 | 0.1446 | 0.1300 | 0.1178 | 0.1074 | 0.0984 | 0.0907 | 0.0839 |
| 1.15 |  | 1.3203 | 0.8518 | 0.6300 | 0.4977 | 0.4094 | 0.3460 | 0.2984 | 0.2613 | 0.2316 | 0.2073 | 0.1871 | 0.1700 | 0.1555 | 0.1429 | 0.1319 |
| 1.20 |  |  | 1.5243 | 1.0152 | 0.7656 | 0.6131 | 0.5093 | 0.4339 | 0.3765 | 0.3314 | 0.2950 | 0.2650 | 0.2400 | 0.2187 | 0.2004 | 0.1846 |
| 1.25 |  |  |  | 1.6886 | 1.1517 | 0.8817 | 0.7138 | 0.5978 | 0.5126 | 0.4472 | 0.3954 | 0.3533 | 0.3185 | 0.2892 | 0.2642 | 0.2427 |
| 1.30 |  |  |  |  | 1.8258 | 1.2685 | 0.9831 | 0.8030 | 0.6772 | 0.5840 | 0.5118 | 0.4543 | 0.4073 | 0.3682 | 0.3352 | 0.3070 |
| 1.35 |  |  |  |  |  | 1.9433 | 1.3705 | 1.0729 | 0.8830 | 0.7492 | 0.6491 | 0.5713 | 0.5088 | 0.4576 | 0.4148 | 0.3785 |
| 1.40 |  |  |  |  |  |  | 2.0460 | 1.4610 | 1.1536 | 0.9555 | 0.8149 | 0.7092 | 0.6263 | 0.5596 | 0.5047 | 0.4586 |
| 1.45 |  |  |  |  |  |  |  | 2.1371 | 1.5422 | 1.2267 | 1.0218 | 0.8755 | 0.7647 | 0.6776 | 0.6072 | 0.5489 |
| 1.50 |  |  |  |  |  |  |  |  | 2.2188 | 1.6159 | 1.2935 | 1.0829 | 0.9316 | 0.8165 | 0.7257 | 0.6519 |
| 1.55 |  |  |  |  |  |  |  |  |  | 2.2930 | 1.6832 | 1.3550 | 1.1394 | 0.9838 | 0.8650 | 0.7708 |
| 1.60 |  |  |  |  |  |  |  |  |  |  | 2.3609 | 1.7452 | 1.4121 | 1.1921 | 1.0327 | 0.9106 |
| 1.65 |  |  |  |  |  |  |  |  |  |  |  | 2.4233 | 1.8027 | 1.4652 | 1.2415 | 1.0787 |
| 1.70 |  |  |  |  |  |  |  |  |  |  |  |  | 2.4813 | 1.8563 | 1.5150 | 1.2879 |


| Iph/lb <br> la/lb | $\mathbf{1 . 9 5}$ | $\mathbf{2 . 0 0}$ | $\mathbf{2 . 2 0}$ | $\mathbf{2 . 4 0}$ | $\mathbf{2 . 6 0}$ | $\mathbf{2 . 8 0}$ | $\mathbf{3 . 0 0}$ | $\mathbf{3 . 2 0}$ | $\mathbf{3 . 4 0}$ | $\mathbf{3 . 6 0}$ | $\mathbf{3 . 8 0}$ | $\mathbf{4 . 0 0}$ | $\mathbf{4 . 2 0}$ | $\mathbf{4 . 4 0}$ | $\mathbf{4 . 6 0}$ | $\mathbf{4 . 8 0}$ |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| $\mathbf{1 . 1 0}$ | 0.0779 | 0.0726 | 0.0562 | 0.0451 | 0.0371 | 0.0312 | 0.0266 | 0.0230 | 0.0201 | 0.0177 | 0.0157 | 0.0141 | 0.0127 | 0.0115 | 0.0105 | 0.0096 |
| $\mathbf{1 . 1 5}$ | 0.1223 | 0.1137 | 0.0877 | 0.0702 | 0.0576 | 0.0483 | 0.0411 | 0.0355 | 0.0310 | 0.0273 | 0.0243 | 0.0217 | 0.0196 | 0.0177 | 0.0161 | 0.0147 |
| $\mathbf{1 . 2 0}$ | 0.1708 | 0.1586 | 0.1217 | 0.0970 | 0.0795 | 0.0665 | 0.0566 | 0.0488 | 0.0426 | 0.0375 | 0.0333 | 0.0298 | 0.0268 | 0.0243 | 0.0221 | 0.0202 |
| $\mathbf{1 . 2 5}$ | 0.2240 | 0.2076 | 0.1584 | 0.1258 | 0.1028 | 0.0858 | 0.0729 | 0.0628 | 0.0547 | 0.0482 | 0.0428 | 0.0382 | 0.0344 | 0.0311 | 0.0283 | 0.0259 |
| $\mathbf{1 . 3 0}$ | 0.2826 | 0.2614 | 0.1981 | 0.1566 | 0.1276 | 0.1063 | 0.0902 | 0.0776 | 0.0676 | 0.0594 | 0.0527 | 0.0471 | 0.0424 | 0.0383 | 0.0348 | 0.0318 |
| $\mathbf{1 . 3 5}$ | 0.3474 | 0.3204 | 0.2410 | 0.1897 | 0.1541 | 0.1281 | 0.1085 | 0.0932 | 0.0811 | 0.0713 | 0.0632 | 0.0564 | 0.0507 | 0.0458 | 0.0417 | 0.0380 |
| $\mathbf{1 . 4 0}$ | 0.4194 | 0.3857 | 0.2877 | 0.2253 | 0.1823 | 0.1512 | 0.1278 | 0.1097 | 0.0953 | 0.0837 | 0.0741 | 0.0661 | 0.0594 | 0.0537 | 0.0488 | 0.0445 |
| $\mathbf{1 . 4 5}$ | 0.4999 | 0.4581 | 0.3384 | 0.2635 | 0.2125 | 0.1758 | 0.1483 | 0.1271 | 0.1103 | 0.0967 | 0.0856 | 0.0763 | 0.0686 | 0.0619 | 0.0562 | 0.0513 |
| $\mathbf{1 . 5 0}$ | 0.5907 | 0.5390 | 0.3938 | 0.3046 | 0.2446 | 0.2018 | 0.1699 | 0.1454 | 0.1260 | 0.1104 | 0.0976 | 0.0870 | 0.0781 | 0.0705 | 0.0640 | 0.0584 |
| $\mathbf{1 . 5 5}$ | 0.6940 | 0.6302 | 0.4545 | 0.3491 | 0.2790 | 0.2295 | 0.1928 | 0.1646 | 0.1425 | 0.1247 | 0.1102 | 0.0982 | 0.0881 | 0.0795 | 0.0721 | 0.0657 |
| $\mathbf{1 . 6 0}$ | 0.8134 | 0.7340 | 0.5213 | 0.3971 | 0.3159 | 0.2589 | 0.2169 | 0.1849 | 0.1599 | 0.1398 | 0.1234 | 0.1098 | 0.0984 | 0.0888 | 0.0805 | 0.0734 |
| $\mathbf{1 . 6 5}$ | 0.9536 | 0.8537 | 0.5952 | 0.4492 | 0.3553 | 0.2901 | 0.2425 | 0.2063 | 0.1781 | 0.1555 | 0.1372 | 0.1220 | 0.1093 | 0.0985 | 0.0893 | 0.0814 |
| $\mathbf{1 . 7 0}$ | 1.1221 | 0.9943 | 0.6776 | 0.5059 | 0.3977 | 0.3234 | 0.2695 | 0.2288 | 0.1972 | 0.1720 | 0.1516 | 0.1347 | 0.1206 | 0.1086 | 0.0984 | 0.0897 |


| Iph/lb <br> la/lb | $\mathbf{5 . 0 0}$ | $\mathbf{5 . 5 0}$ | $\mathbf{6 . 0 0}$ | $\mathbf{6 . 5 0}$ | $\mathbf{7 . 0 0}$ | $\mathbf{7 . 5 0}$ | $\mathbf{8 . 0 0}$ | $\mathbf{8 . 5 0}$ | $\mathbf{9 . 0 0}$ | $\mathbf{9 . 5 0}$ | $\mathbf{1 0 . 0 0}$ | $\mathbf{1 2 . 5 0}$ | $\mathbf{1 5 . 0 0}$ | $\mathbf{1 7 . 5 0}$ | $\mathbf{2 0 . 0 0}$ |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| $\mathbf{1 . 1 0}$ | 0.0088 | 0.0072 | 0.0060 | 0.0051 | 0.0044 | 0.0038 | 0.0033 | 0.0030 | 0.0026 | 0.0024 | 0.0021 | 0.0014 | 0.0009 | 0.0007 | 0.0005 |
| $\mathbf{1 . 1 5}$ | 0.0135 | 0.0111 | 0.0093 | 0.0078 | 0.0067 | 0.0059 | 0.0051 | 0.0045 | 0.0040 | 0.0036 | 0.0033 | 0.0021 | 0.0014 | 0.0011 | 0.0008 |
| $\mathbf{1 . 2 0}$ | 0.0185 | 0.0152 | 0.0127 | 0.0107 | 0.0092 | 0.0080 | 0.0070 | 0.0062 | 0.0055 | 0.0049 | 0.0045 | 0.0028 | 0.0020 | 0.0014 | 0.0011 |
| $\mathbf{1 . 2 5}$ | 0.0237 | 0.0194 | 0.0162 | 0.0137 | 0.0118 | 0.0102 | 0.0090 | 0.0079 | 0.0071 | 0.0063 | 0.0057 | 0.0036 | 0.0025 | 0.0018 | 0.0014 |
| $\mathbf{1 . 3 0}$ | 0.0292 | 0.0239 | 0.0199 | 0.0169 | 0.0145 | 0.0126 | 0.0110 | 0.0097 | 0.0087 | 0.0078 | 0.0070 | 0.0045 | 0.0031 | 0.0023 | 0.0017 |
| $\mathbf{1 . 3 5}$ | 0.0349 | 0.0285 | 0.0238 | 0.0201 | 0.0173 | 0.0150 | 0.0131 | 0.0116 | 0.0103 | 0.0093 | 0.0083 | 0.0053 | 0.0037 | 0.0027 | 0.0021 |
| $\mathbf{1 . 4 0}$ | 0.0408 | 0.0334 | 0.0278 | 0.0235 | 0.0202 | 0.0175 | 0.0154 | 0.0136 | 0.0121 | 0.0108 | 0.0097 | 0.0062 | 0.0043 | 0.0031 | 0.0024 |
| $\mathbf{1 . 4 5}$ | 0.0470 | 0.0384 | 0.0320 | 0.0271 | 0.0232 | 0.0202 | 0.0177 | 0.0156 | 0.0139 | 0.0124 | 0.0112 | 0.0071 | 0.0049 | 0.0036 | 0.0028 |
| $\mathbf{1 . 5 0}$ | 0.0535 | 0.0437 | 0.0364 | 0.0308 | 0.0264 | 0.0229 | 0.0200 | 0.0177 | 0.0157 | 0.0141 | 0.0127 | 0.0081 | 0.0056 | 0.0041 | 0.0031 |
| $\mathbf{1 . 5 5}$ | 0.0602 | 0.0491 | 0.0409 | 0.0346 | 0.0297 | 0.0257 | 0.0225 | 0.0199 | 0.0177 | 0.0158 | 0.0143 | 0.0091 | 0.0063 | 0.0046 | 0.0035 |
| $\mathbf{1 . 6 0}$ | 0.0672 | 0.0548 | 0.0456 | 0.0386 | 0.0330 | 0.0286 | 0.0251 | 0.0221 | 0.0197 | 0.0176 | 0.0159 | 0.0101 | 0.0070 | 0.0051 | 0.0039 |
| $\mathbf{1 . 6 5}$ | 0.0745 | 0.0607 | 0.0505 | 0.0427 | 0.0365 | 0.0317 | 0.0277 | 0.0245 | 0.0218 | 0.0195 | 0.0176 | 0.0112 | 0.0077 | 0.0057 | 0.0043 |
| $\mathbf{1 . 7 0}$ | 0.0820 | 0.0668 | 0.0555 | 0.0469 | 0.0402 | 0.0348 | 0.0305 | 0.0269 | 0.0239 | 0.0214 | 0.0193 | 0.0122 | 0.0085 | 0.0062 | 0.0047 |

Protection of equipment against thermal damage due to overloads.


Tripping curves.

## Description

This function is used to protect capacitor banks with or without anti-harmonic inductors against overloads, based on the measurement of the current drawn.

The current measured by the thermal protection is an RMS 3-phase current which takes into account harmonics up to number 13.
The highest current of the three phases I1, I2 and I3, subsequently called phase current Iph, is used to calculate the heat rise:
Iph $=\max (11,12,13)$
Taking capacitor step ratio into account
When the number of steps ( $>1$ ) and capacitor step ratio are set in the particular characteristics, the thermal overload protection function takes into account the participation of each step in the calculation of heat rise.

The rated current of step $x(\operatorname{lbg} x)$ is equal to the fraction of current that the step represents in relation to the rated current of the capacitor bank (lb).
$\operatorname{lbgx}=\frac{\operatorname{Kgx}}{\sum_{x=1}^{n} \mathrm{Kgx}} \mathrm{lb}$
where lb is the rated current of the capacitor bank
x is the step number
n is the total number of steps, between 2 and 4
Kgx is the capacitor step ratio value of step x
The rated current of the sequence of steps (lbseq) is calculated. It is the sum of the rated currents (lbgx) of the steps closed during the sequence.

Ibseq $=\sum^{n} p(x) \operatorname{lbg} x$
$x=1$
where $x$ is the step number
n is the total number of steps, between 2 and 4
$p(x)$ is the position of the step $x$ :
$\square p(x)=1$ when the step switch $x$ is closed
$\square p(x)=0$ when the step switch $x$ is open.
The heat rise is proportional to the square of the drawn current in relation to the rated current of the sequence. Under steady state conditions, it is equal to:
$E=\left(\frac{\text { Iph }}{\text { Ibseq }}\right)^{2} \times 100 \quad$ as a \%

If the closed positions of the steps are not acquired or if the number of steps set in the particular characteristics is 1 , the rated current of the sequences is equal to the rated current of the capacitor bank. In such cases, the heat rise is proportional to the drawn current in relation to the rated current of the capacitor bank. Under steady state conditions, it is equal to:
$E=\left(\frac{\mathbf{l p h}}{\mathbf{l} \mathbf{b}}\right)^{2} \times 100 \quad$ as $\mathrm{a} \%$

## Operation curve

The protection function gives a tripping order when the current drawn is greater than the overload current, with respect to the rated current of the sequence.
The tripping time is set by assigning a hot tripping time to a setting current. This setting is used to calculate a time factor:
$\mathbf{C}=\frac{1}{\ln \left(\frac{\left(\frac{\mathbf{I s}}{\mathbf{I b}}\right)^{2}-1}{\left(\frac{\mathbf{I s}}{\mathrm{Ib}}\right)^{2}-\left(\frac{\text { Itrip }}{\mathbf{I b}}\right)^{2}}\right)}$ where In: natural logarithm.
The tripping time with an initial heat rise of $0 \%$ is then given by:
$\mathbf{t}=\mathbf{C} \times \ln \left(\frac{\left(\frac{\text { Iph }}{\text { Ibseq }}\right)^{2}}{\left(\frac{\text { Iph }}{\text { Ibseq }}\right)^{2}-\left(\frac{\text { Itrip }}{\text { Ibseq }}\right)^{2}}\right) \times$ Ts $\quad$ where In: natural logarithm.
$=\mathbf{k} \times$ Ts
The tripping time with an intial heat rise of $100 \%$ is then given by:
$\mathbf{t}=\mathbf{C} \times \operatorname{In}\left(\frac{\left(\frac{\text { Iph }}{\text { Ibseq }}\right)^{2}-1}{\left(\frac{\text { Iph }}{\text { Ibseq }}\right)^{2}-\left(\frac{\text { Itrip }}{\text { Ibseq }}\right)^{2}}\right) \times$ Ts $\quad$ where In: natural logarithm.
$=\mathbf{k x T s}$
The tripping curve tables give the values of $k$ for an inital heat rise from $0 \%$ to $100 \%$. The current heat rise is saved in the event of an auxiliary power failure.

Block diagram


## Protection functions

Thermal overload for capacitors ANSI code 49RMS

## User information

The following information is available for the user:

- heat rise
- time before tripping (with constant current).


## Characteristics

| Settings |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Alarm current lalarm |  |  |  |  |
| Setting range | 1.05 to 1.70 lb |  |  |  |
| Accuracy ${ }^{(1)}$ | $\pm 2$ \% |  |  |  |
| Resolution | 1 A |  |  |  |
| Tripping current Itrip |  |  |  |  |
| Setting range | 1.05 to 1.70 lb |  |  |  |
| Accuracy ${ }^{(1)}$ | $\pm 2$ \% |  |  |  |
| Resolution | 1 A |  |  |  |
| Setting current Is |  |  |  |  |
| Setting range | 1.02 Itrip to 2 lb |  |  |  |
| Accuracy ${ }^{(1)}$ | $\pm 2$ \% |  |  |  |
| Resolution | 1 A |  |  |  |
| Setting time Ts |  |  |  |  |
| Setting range | 1 to 2000 minutes (range varies depending on the tripping and setting currents) |  |  |  |
| Resolution | 1 min |  |  |  |
| Characteristic times |  |  |  |  |
| Operation time accuracy | $\pm 2 \%$ or $\pm 2 \mathrm{~s}$ |  |  |  |
| Inputs |  |  |  |  |
| Designation | Syntax | Equations | Logipam |  |
| Protection reset | P49RMS_1_101 | ■ | - |  |
| Protection inhibition | P49RMS_1_113 | $\square$ | ■ |  |
| Outputs |  |  |  |  |
| Designation | Syntax | Equations | Logipam | Matrix |
| Delayed output | P49RMS _1_3 | ■ | - | ■ |
| Alarm | P49RMS _1_10 | $\square$ | - | - |
| Inhibit closing | P49RMS_1_11 | $\square$ | - | - |
| Protection inhibited | P49RMS _1_16 | $\square$ | - |  |
| Hot state | P49RMS_1_18 | $\square$ | - |  |

(1) Under reference conditions (IEC 60255-6).


Parameter setting of capacitor bank step ratio.

## Example

Given a 350 kvar capacitor bank with 3 steps, and no anti-harmonic inductors, for a voltage of 2 kV . The capacitor step ratio is 1.2.2.

The rated current of the capacitor bank is:
$\mathrm{lb}=\mathrm{Q} /(\sqrt{3}$ Un $)=350000(\sqrt{3} \times 2000)=101 \mathrm{~A}$

According to the manufacturer data, this capacitor bank can operate continuously with an overload current of $120 \% \mathrm{lb}$ and for 20 minutes with an overload of $140 \% \mathrm{lb}$.

The protection settings are:
Itrip $=120 \% \mathrm{lb}=121 \mathrm{~A}$
Is $=140 \% \mathrm{lb}=141 \mathrm{~A}$
$\mathrm{Ts}=20 \mathrm{~min}$.

## Steps 1 and 2 closed

Steps 1 and 2 are closed in the sequence in progress. The sequence current is:
$\operatorname{lbseq}=\frac{1+2+0}{1+2+2} \times \mathrm{Ib}=61 \mathrm{~A}$
For a current of $125 \%$ lbseq = 76 A , and an initial heat rise of $100 \%$, the value of k in the tripping curve tables is: $k=2.486$.

The tripping time is:
$\mathbf{t}=\mathbf{k x} \mathbf{T s}=2.486 \times 20 \approx 50 \mathbf{m i n}$

All the steps closed
When all the steps are closed, the sequence current is the rated current of the capacitor bank:
$\mathrm{Ibseq}=\frac{1+2+2}{1+2+2} \times \mathrm{Ib}=101 \mathrm{~A}$
For a current of $140 \% \mathrm{lbseq}=141 \mathrm{~A}$, and an initial heat rise of $0 \%$, the value of k in the tripping curve tables is: $k=2.164$.

The tripping time is:
$\mathbf{t}=\mathrm{k} \times \mathrm{Ts}=2.164 \times 20 \approx 43 \mathrm{~min}$

The table below summarizes the rated sequence current, the tripping current and examples of tripping times for overload currents of $125 \% \mathrm{lb}$ and $140 \% \mathrm{lb}$, for initial heat rises of $0 \%$ and $100 \%$.

| Closed step numbers |  |  | Ibseq (A) | Itrip <br> (A) | 125 \% lbseq |  |  | 140 \% Ibseq |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Iph <br> (A) |  | Tripping time (mn) |  | Iph <br> (A) | Tripping time (mn) |  |
| 1 | 2 | 3 |  |  | 0 \% | 100\% |  | 0 \% | $100 \%$ |
| - | - | - | $\frac{1+0+0}{1+2+2} \times \mathrm{lb}=20$ | 24 | 25 | 83 | 50 | 28 | 43 | 20 |
| $\square$ | $\square$ | - | $\frac{1+2+0}{1+2+2} \times \mathrm{lb}=61$ | 73 | 76 | 83 | 50 | 85 | 43 | 20 |
| - | $\square$ | - | $\frac{0+2+2}{1+2+2} \times 1 b=81$ | 97 | 101 | 83 | 50 | 113 | 43 | 20 |
| ■ | $\square$ | - | $\frac{1+2+2}{1+2+2} \times \mathrm{lb}=101$ | 121 | 126 | 83 | 50 | 141 | 43 | 20 |

## Curves for initial heat rise = $0 \%$

| Is = 1.2 lb <br> Iph/lbseq <br> Itrip/lbseq | $\mathbf{1 . 1 0}$ | $\mathbf{1 . 1 5}$ | $\mathbf{1 . 2 0}$ | $\mathbf{1 . 2 5}$ | $\mathbf{1 . 3 0}$ | $\mathbf{1 . 3 5}$ | $\mathbf{1 . 4 0}$ | $\mathbf{1 . 4 5}$ | $\mathbf{1 . 5 0}$ | $\mathbf{1 . 5 5}$ | $\mathbf{1 . 6 0}$ | $\mathbf{1 . 6 5}$ | $\mathbf{1 . 7 0}$ | $\mathbf{1 . 7 5}$ | $\mathbf{1 . 8 0}$ |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


| Is = 1.2 $\mathbf{~ l b ~}$ <br> Iph/lbseq <br> Itrip/lbseq <br> $\mathbf{1 . 8 5}$ | $\mathbf{1 . 9 0}$ | $\mathbf{1 . 9 5}$ | $\mathbf{2 . 0 0}$ | $\mathbf{2 . 2 0}$ | $\mathbf{2 . 4 0}$ | $\mathbf{2 . 6 0}$ | $\mathbf{2 . 8 0}$ | $\mathbf{3 . 0 0}$ | $\mathbf{3 . 2 0}$ | $\mathbf{3 . 4 0}$ | $\mathbf{3 . 6 0}$ | $\mathbf{3 . 8 0}$ | $\mathbf{4 . 0 0}$ |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| $\mathbf{1 . 0 5}$ | 1.4660 | 1.3741 | 1.2911 | 1.2158 | 0.9747 | 0.8011 | 0.6713 | 0.5714 | 0.4927 | 0.4295 | 0.3779 | 0.3352 | 0.2995 | 0.2692 |
| $\mathbf{1 . 1 0}$ | 0.6725 | 0.6293 | 0.5905 | 0.5554 | 0.4435 | 0.3635 | 0.3040 | 0.2584 | 0.2226 | 0.1939 | 0.1704 | 0.1511 | 0.1349 | 0.1212 |
| $\mathbf{1 . 1 5}$ | 0.3699 | 0.3456 | 0.3237 | 0.3040 | 0.2417 | 0.1976 | 0.1649 | 0.1399 | 0.1204 | 0.1047 | 0.0920 | 0.0815 | 0.0728 | 0.0653 |


| Iph/lbseq Itrip/lbseq | 1.10 | 1.15 | 1.20 | 1.25 | 1.30 | 1.35 | 1.40 | 1.45 | 1.50 | 1.55 | 1.60 | 1.65 | 1.70 | 1.75 | 1.80 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1.05 | 15.0540 | 11.1530 | 9.0217 | 7.6039 | 6.5703 | 5.7750 | 5.1405 | 4.6210 | 4.1871 | 3.8189 | 3.5027 | 3.2281 | 2.9875 | 2.7752 | 2.5864 |
| 1.10 |  | 6.7905 | 5.0545 | 4.1030 | 3.4684 | 3.0047 | 2.6470 | 2.3611 | 2.1265 | 1.9301 | 1.7633 | 1.6197 | 1.4948 | 1.3852 | 1.2883 |
| 1.15 |  |  | 3.9779 | 2.9738 | 2.4220 | 2.0530 | 1.7829 | 1.5740 | 1.4067 | 1.2692 | 1.1539 | 1.0557 | 0.9711 | 0.8974 | 0.8327 |
| 1.20 |  |  |  | 2.5077 | 1.8824 | 1.5378 | 1.3070 | 1.1375 | 1.0063 | 0.9010 | 0.8143 | 0.7415 | 0.6794 | 0.6257 | 0.5790 |
| 1.25 |  |  |  |  | 1.5305 | 1.1532 | 0.9449 | 0.8050 | 0.7021 | 0.6223 | 0.5582 | 0.5052 | 0.4607 | 0.4227 | 0.3898 |


| Is = 1.3 lb |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Iph/lbseq <br> Itrip/lbseq | $\mathbf{1 . 8 5}$ | $\mathbf{1 . 9 0}$ | $\mathbf{1 . 9 5}$ | $\mathbf{2 . 0 0}$ | $\mathbf{2 . 2 0}$ | $\mathbf{2 . 4 0}$ | $\mathbf{2 . 6 0}$ | $\mathbf{2 . 8 0}$ | $\mathbf{3 . 0 0}$ | $\mathbf{3 . 2 0}$ | $\mathbf{3 . 4 0}$ | $\mathbf{3 . 6 0}$ | $\mathbf{3 . 8 0}$ | $\mathbf{4 . 0 0}$ |
| $\mathbf{1 . 0 5}$ | 2.4177 | 2.2661 | 2.1292 | 2.0051 | 1.6074 | 1.3211 | 1.1071 | 0.9424 | 0.8126 | 0.7084 | 0.6233 | 0.5529 | 0.4939 | 0.4440 |
| $\mathbf{1 . 1 0}$ | 1.2021 | 1.1249 | 1.0555 | 0.9927 | 0.7927 | 0.6498 | 0.5435 | 0.4619 | 0.3979 | 0.3465 | 0.3047 | 0.2701 | 0.2412 | 0.2167 |
| $\mathbf{1 . 1 5}$ | 0.7753 | 0.7242 | 0.6785 | 0.6372 | 0.5066 | 0.4141 | 0.3456 | 0.2933 | 0.2523 | 0.2195 | 0.1929 | 0.1709 | 0.1525 | 0.1370 |
| $\mathbf{1 . 2 0}$ | 0.5378 | 0.5013 | 0.4688 | 0.4396 | 0.3478 | 0.2834 | 0.2360 | 0.1999 | 0.1717 | 0.1493 | 0.1310 | 0.1160 | 0.1035 | 0.0929 |
| $\mathbf{1 . 2 5}$ | 0.3611 | 0.3358 | 0.3134 | 0.2933 | 0.2309 | 0.1874 | 0.1557 | 0.1316 | 0.1129 | 0.0981 | 0.0860 | 0.0761 | 0.0678 | 0.0609 |


| lph/lbseq Itrip/lbseq | 1.10 | 1.15 | 1.20 | 1.25 | 1.30 | 1.35 | 1.40 | 1.45 | 1.50 | 1.55 | 1.60 | 1.65 | 1.70 | 1.75 | 1.80 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1.05 | 21.4400 | 15.8850 | 12.8490 | 10.8300 | 9.3578 | 8.2251 | 7.3214 | 6.5815 | 5.9634 | 5.4391 | 4.9887 | 4.5976 | 4.2550 | 3.9525 | 3.6837 |
| 1.10 |  | 9.9827 | 7.4306 | 6.0317 | 5.0988 | 4.4171 | 3.8914 | 3.4710 | 3.1261 | 2.8375 | 2.5922 | 2.3811 | 2.1975 | 2.0364 | 1.8939 |
| 1.15 |  |  | 6.1214 | 4.5762 | 3.7270 | 3.1593 | 2.7435 | 2.4222 | 2.1647 | 1.9531 | 1.7757 | 1.6246 | 1.4944 | 1.3810 | 1.2813 |
| 1.20 |  |  |  | 4.1525 | 3.1170 | 2.5464 | 2.1642 | 1.8836 | 1.6664 | 1.4920 | 1.3483 | 1.2278 | 1.1249 | 1.0361 | 0.9587 |
| 1.25 |  |  |  |  | 2.9310 | 2.2085 | 1.8095 | 1.5416 | 1.3446 | 1.1918 | 1.0689 | 0.9676 | 0.8823 | 0.8095 | 0.7466 |
| 1.30 |  |  |  |  |  | 2.0665 | 1.5627 | 1.2839 | 1.0964 | 0.9582 | 0.8508 | 0.7643 | 0.6929 | 0.6327 | 0.5813 |
| 1.35 |  |  |  |  |  |  | 1.3673 | 1.0375 | 0.8546 | 0.7314 | 0.6404 | 0.5696 | 0.5125 | 0.4653 | 0.4254 |

ls $=1.4 \mathrm{lb}$

| Iph/lbseq <br> Itrip/lbseq | $\mathbf{1 . 8 5}$ | $\mathbf{1 . 9 0}$ | $\mathbf{1 . 9 5}$ | $\mathbf{2 . 0 0}$ | $\mathbf{2 . 2 0}$ | $\mathbf{2 . 4 0}$ | $\mathbf{2 . 6 0}$ | $\mathbf{2 . 8 0}$ | $\mathbf{3 . 0 0}$ | $\mathbf{3 . 2 0}$ | $\mathbf{3 . 4 0}$ | $\mathbf{3 . 6 0}$ | $\mathbf{3 . 8 0}$ | $\mathbf{4 . 0 0}$ |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| $\mathbf{1 . 0 5}$ | 3.4434 | 3.2275 | 3.0325 | 2.8557 | 2.2894 | 1.8816 | 1.5768 | 1.3422 | 1.1573 | 1.0089 | 0.8877 | 0.7874 | 0.7034 | 0.6323 |
| $\mathbf{1 . 1 0}$ | 1.7672 | 1.6537 | 1.5516 | 1.4593 | 1.1654 | 0.9552 | 0.7989 | 0.6791 | 0.5849 | 0.5094 | 0.4479 | 0.3970 | 0.3545 | 0.3186 |
| $\mathbf{1 . 1 5}$ | 1.1931 | 1.1145 | 1.0440 | 0.9805 | 0.7796 | 0.6372 | 0.5318 | 0.4513 | 0.3882 | 0.3378 | 0.2968 | 0.2629 | 0.2346 | 0.2107 |
| $\mathbf{1 . 2 0}$ | 0.8906 | 0.8302 | 0.7763 | 0.7279 | 0.5760 | 0.4692 | 0.3907 | 0.3310 | 0.2844 | 0.2472 | 0.2170 | 0.1921 | 0.1714 | 0.1538 |
| $\mathbf{1 . 2 5}$ | 0.6916 | 0.6432 | 0.6002 | 0.5618 | 0.4421 | 0.3589 | 0.2981 | 0.2521 | 0.2163 | 0.1878 | 0.1647 | 0.1457 | 0.1299 | 0.1165 |
| $\mathbf{1 . 3 0}$ | 0.5367 | 0.4977 | 0.4634 | 0.4328 | 0.3386 | 0.2738 | 0.2268 | 0.1914 | 0.1640 | 0.1422 | 0.1246 | 0.1102 | 0.0981 | 0.0880 |
| $\mathbf{1 . 3 5}$ | 0.3913 | 0.3617 | 0.3358 | 0.3129 | 0.2431 | 0.1957 | 0.1617 | 0.1361 | 0.1164 | 0.1009 | 0.0883 | 0.0780 | 0.0694 | 0.0622 |

## Curves for initial heat rise $=0 \%$

Is = $\mathbf{2} \mathbf{l b}$

| Iph/lbseq Itrip/lbseq | 1.10 | 1.15 | 1.20 | 1.25 | 1.30 | 1.35 | 1.40 | 1.45 | 1.50 | 1.55 | 1.60 | 1.65 | 1.70 | 1.75 | 1.80 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1.05 | 69.6380 | 51.5950 | 41.7340 | 35.1750 | 30.3940 | 26.7150 | 23.7800 | 21.3760 | 19.3690 | 17.6660 | 16.2030 | 14.9330 | 13.8200 | 12.8380 | 11.9650 |
| 1.10 |  | 33.9580 | 25.2760 | 20.5180 | 17.3440 | 15.0260 | 13.2370 | 11.8070 | 10.6340 | 9.6521 | 8.8176 | 8.0995 | 7.4750 | 6.9270 | 6.4425 |
| 1.15 |  |  | 22.0350 | 16.4730 | 13.4160 | 11.3720 | 9.8756 | 8.7189 | 7.7922 | 7.0303 | 6.3916 | 5.8479 | 5.3792 | 4.9710 | 4.6123 |
| 1.20 |  |  |  | 16.0520 | 12.0490 | 9.8435 | 8.3659 | 7.2814 | 6.4415 | 5.7674 | 5.2122 | 4.7460 | 4.3485 | 4.0053 | 3.7060 |
| 1.25 |  |  |  |  | 12.4460 | 9.3782 | 7.6840 | 6.5465 | 5.7100 | 5.0610 | 4.5392 | 4.1087 | 3.7467 | 3.4375 | 3.1703 |
| 1.30 |  |  |  |  |  | 10.0300 | 7.5843 | 6.2313 | 5.3211 | 4.6505 | 4.1294 | 3.7096 | 3.3629 | 3.0708 | 2.8210 |
| 1.35 |  |  |  |  |  |  | 8.2921 | 6.2917 | 5.1827 | 4.4353 | 3.8838 | 3.4544 | 3.1081 | 2.8215 | 2.5799 |
| 1.40 |  |  |  |  |  |  |  | 6.9790 | 5.3124 | 4.3868 | 3.7619 | 3.3000 | 2.9399 | 2.6491 | 2.4081 |
| 1.50 |  |  |  |  |  |  |  |  |  | 5.1152 | 3.9169 | 3.2491 | 2.7969 | 2.4617 | 2.1997 |
| 1.60 |  |  |  |  |  |  |  |  |  |  |  | 3.8403 | 2.9564 | 2.4625 | 2.1271 |
| 1.70 |  |  |  |  |  |  |  |  |  |  |  |  |  | 2.8932 | 2.2383 |


| Iph/lbseq <br> Itrip/lbseq | 1.85 | 1.90 | 1.95 | 2.00 | 2.20 | 2.40 | 2.60 | 2.80 | 3.00 | 3.20 | 3.40 | 3.60 | 3.80 | 4.00 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1.05 | 11.1840 | 10.4830 | 9.8495 | 9.2753 | 7.4358 | 6.1115 | 5.1214 | 4.3594 | 3.7590 | 3.2768 | 2.8832 | 2.5574 | 2.2846 | 2.0537 |
| 1.10 | 6.0114 | 5.6254 | 5.2781 | 4.9642 | 3.9642 | 3.2494 | 2.7177 | 2.3099 | 1.9896 | 1.7328 | 1.5235 | 1.3506 | 1.2059 | 1.0836 |
| 1.15 | 4.2947 | 4.0117 | 3.7581 | 3.5295 | 2.8064 | 2.2936 | 1.9142 | 1.6245 | 1.3975 | 1.2159 | 1.0683 | 0.9464 | 0.8446 | 0.7586 |
| 1.20 | 3.4426 | 3.2091 | 3.0008 | 2.8138 | 2.2265 | 1.8138 | 1.5104 | 1.2795 | 1.0993 | 0.9555 | 0.8388 | 0.7426 | 0.6624 | 0.5946 |
| 1.25 | 2.9368 | 2.7311 | 2.5486 | 2.3855 | 1.8775 | 1.5240 | 1.2659 | 1.0704 | 0.9184 | 0.7974 | 0.6994 | 0.6187 | 0.5515 | 0.4949 |
| 1.30 | 2.6048 | 2.4157 | 2.2489 | 2.1007 | 1.6433 | 1.3288 | 1.1007 | 0.9289 | 0.7958 | 0.6901 | 0.6047 | 0.5346 | 0.4762 | 0.4271 |
| 1.35 | 2.3729 | 2.1935 | 2.0365 | 1.8978 | 1.4745 | 1.1871 | 0.9804 | 0.8257 | 0.7061 | 0.6116 | 0.5354 | 0.4730 | 0.4210 | 0.3774 |
| 1.40 | 2.2046 | 2.0301 | 1.8787 | 1.7459 | 1.3461 | 1.0785 | 0.8878 | 0.7459 | 0.6369 | 0.5509 | 0.4817 | 0.4252 | 0.3782 | 0.3388 |
| 1.50 | 1.9875 | 1.8112 | 1.6620 | 1.5337 | 1.1600 | 0.9190 | 0.7509 | 0.6276 | 0.5337 | 0.4603 | 0.4016 | 0.3538 | 0.3143 | 0.2812 |
| 1.60 | 1.8779 | 1.6825 | 1.5240 | 1.3920 | 1.0256 | 0.8008 | 0.6484 | 0.5386 | 0.4560 | 0.3920 | 0.3411 | 0.2998 | 0.2659 | 0.2376 |
| 1.70 | 1.8713 | 1.6215 | 1.4355 | 1.2893 | 0.9143 | 0.7007 | 0.5610 | 0.4625 | 0.3895 | 0.3335 | 0.2894 | 0.2538 | 0.2246 | 0.2004 |

## Curves for initial heat rise = 100 \%

| Is $=\mathbf{1 . 2} \mathbf{~ l b}$ <br> Iph/lbseq <br> Itrip/lbseq | $\mathbf{1 . 1 0}$ | $\mathbf{1 . 1 5}$ | $\mathbf{1 . 2 0}$ | $\mathbf{1 . 2 5}$ | $\mathbf{1 . 3 0}$ | $\mathbf{1 . 3 5}$ | $\mathbf{1 . 4 0}$ | $\mathbf{1 . 4 5}$ | $\mathbf{1 . 5 0}$ | $\mathbf{1 . 5 5}$ | $\mathbf{1 . 6 0}$ | $\mathbf{1 . 6 5}$ | $\mathbf{1 . 7 0}$ | $\mathbf{1 . 7 5}$ | $\mathbf{1 . 8 0}$ |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| $\mathbf{1 . 0 5}$ | 2.5249 | 1.4422 | 1.0000 | 0.7585 | 0.6064 | 0.5019 | 0.4258 | 0.3679 | 0.3226 | 0.2862 | 0.2563 | 0.2313 | 0.2102 | 0.1922 | 0.1766 |
| $\mathbf{1 . 1 0}$ |  | 1.624 | 1.000 | 0.720 | 0.559 | 0.454 | 0.381 | 0.3257 | 0.2835 | 0.2501 | 0.2229 | 0.2004 | 0.1816 | 0.1655 | 0.1518 |
| $\mathbf{1 . 1 5}$ |  |  | 1.000 | 0.645 | 0.477 | 0.377 | 0.310 | 0.2621 | 0.2260 | 0.1979 | 0.1754 | 0.1570 | 0.1417 | 0.1288 | 0.1177 |


| Iph/Ibseq Itrip/lbseq | 1.85 | 1.90 | 1.95 | 2.00 | 2.20 | 2.40 | 2.60 | 2.80 | 3.00 | 3.20 | 3.40 | 3.60 | 3.80 | 4.00 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1.05 | 0.1630 | 0.1511 | 0.1405 | 0.1311 | 0.1020 | 0.0821 | 0.0677 | 0.0569 | 0.0486 | 0.0421 | 0.0368 | 0.0325 | 0.0289 | 0.0259 |
| 1.10 | 0.1398 | 0.1293 | 0.1201 | 0.1119 | 0.0867 | 0.0696 | 0.0573 | 0.0481 | 0.0410 | 0.0354 | 0.0310 | 0.0273 | 0.0243 | 0.0217 |
| 1.15 | 0.1082 | 0.0999 | 0.0926 | 0.0861 | 0.0664 | 0.0531 | 0.0436 | 0.0366 | 0.0312 | 0.0269 | 0.0235 | 0.0207 | 0.0184 | 0.0165 |


| lph/lbseq Itrip/lbseq |  | 1.15 | 1.20 | 1.25 | 1.30 | 1.35 | 1.40 | 1.45 | 1.50 | 1.55 | 1.60 | 1.65 | 1.70 | 1.75 | 1.80 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1.05 | 4.1639 | 2.3784 | 1.6492 | 1.2509 | 1.0000 | 0.8276 | 0.7021 | 0.6068 | 0.5320 | 0.4719 | 0.4226 | 0.3815 | 0.3467 | 0.3170 | 0.2913 |
| 1.10 |  | 2.9020 | 1.7875 | 1.2878 | 1.0000 | 0.8123 | 0.6802 | 0.5823 | 0.5068 | 0.4470 | 0.3984 | 0.3583 | 0.3246 | 0.2959 | 0.2713 |
| 1.15 |  |  | 2.0959 | 1.3521 | 1.0000 | 0.7901 | 0.6498 | 0.5493 | 0.4737 | 0.4148 | 0.3676 | 0.3291 | 0.2970 | 0.2699 | 0.2468 |
| 1.20 |  |  |  | 1.5014 | 1.0000 | 0.7541 | 0.6039 | 0.5017 | 0.4274 | 0.3708 | 0.3264 | 0.2905 | 0.2610 | 0.2364 | 0.2154 |
| 1.25 |  |  |  |  | 1.0000 | 0.6820 | 0.5222 | 0.4227 | 0.3541 | 0.3036 | 0.2648 | 0.2341 | 0.2092 | 0.1886 | 0.1713 |


| Is = 1.3 lb <br> Iph/lbseq <br> Itrip/lbseq | $\mathbf{1 . 8 5}$ | $\mathbf{1 . 9 0}$ | $\mathbf{1 . 9 5}$ | $\mathbf{2 . 0 0}$ | $\mathbf{2 . 2 0}$ | $\mathbf{2 . 4 0}$ | $\mathbf{2 . 6 0}$ | $\mathbf{2 . 8 0}$ | $\mathbf{3 . 0 0}$ | $\mathbf{3 . 2 0}$ | $\mathbf{3 . 4 0}$ | $\mathbf{3 . 6 0}$ | $\mathbf{3 . 8 0}$ | $\mathbf{4 . 0 0}$ |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| $\mathbf{1 . 0 5}$ | 0.2688 | 0.2491 | 0.2317 | 0.2162 | 0.1682 | 0.1354 | 0.1117 | 0.0939 | 0.0802 | 0.0694 | 0.0607 | 0.0535 | 0.0476 | 0.0426 |
| $\mathbf{1 . 1 0}$ | 0.2499 | 0.2311 | 0.2146 | 0.2000 | 0.1550 | 0.1243 | 0.1023 | 0.0859 | 0.0733 | 0.0633 | 0.0554 | 0.0488 | 0.0434 | 0.0389 |
| $\mathbf{1 . 1 5}$ | 0.2268 | 0.2094 | 0.1941 | 0.1805 | 0.1393 | 0.1114 | 0.0915 | 0.0767 | 0.0653 | 0.0564 | 0.0492 | 0.0434 | 0.0386 | 0.0345 |
| $\mathbf{1 . 2 0}$ | 0.1974 | 0.1819 | 0.1682 | 0.1562 | 0.1199 | 0.0955 | 0.0783 | 0.0655 | 0.0557 | 0.0481 | 0.0419 | 0.0369 | 0.0328 | 0.0293 |
| $\mathbf{1 . 2 5}$ | 0.1565 | 0.1438 | 0.1327 | 0.1230 | 0.0938 | 0.0745 | 0.0609 | 0.0508 | 0.0432 | 0.0372 | 0.0324 | 0.0285 | 0.0253 | 0.0226 |

Is = 1.4 lb

| Iph/lbseq <br> Iph <br> Itrip/lbseq <br> 1.10 | $\mathbf{1 . 1 5}$ | $\mathbf{1 . 2 0}$ | $\mathbf{1 . 2 5}$ | $\mathbf{1 . 3 0}$ | $\mathbf{1 . 3 5}$ | $\mathbf{1 . 4 0}$ | $\mathbf{1 . 4 5}$ | $\mathbf{1 . 5 0}$ | $\mathbf{1 . 5 5}$ | $\mathbf{1 . 6 0}$ | $\mathbf{1 . 6 5}$ | $\mathbf{1 . 7 0}$ | $\mathbf{1 . 7 5}$ | $\mathbf{1 . 8 0}$ |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| $\mathbf{1 . 0 5}$ | 5.9304 | 3.3874 | 2.3488 | 1.7816 | 1.4243 | 1.1788 | 1.0000 | 0.8642 | 0.7577 | 0.6721 | 0.6019 | 0.5434 | 0.4938 | 0.4515 | 0.4148 |
| $\mathbf{1 . 1 0}$ |  | 4.2662 | 2.6278 | 1.8931 | 1.4701 | 1.1942 | 1.0000 | 0.8560 | 0.7451 | 0.6571 | 0.5857 | 0.5267 | 0.4771 | 0.4350 | 0.3988 |
| $\mathbf{1 . 1 5}$ |  | 3.2252 | 2.0806 | 1.5388 | 1.2158 | 1.0000 | 0.8453 | 0.7289 | 0.6383 | 0.5657 | 0.5064 | 0.4570 | 0.4154 | 0.3797 |  |
| $\mathbf{1 . 2 0}$ |  |  | 2.4862 | 1.6559 | 1.2488 | 1.0000 | 0.8307 | 0.7077 | 0.6141 | 0.5405 | 0.4811 | 0.4323 | 0.3914 | 0.3567 |  |
| $\mathbf{1 . 2 5}$ |  |  | 1.9151 | 1.3061 | 1.0000 | 0.8095 | 0.6780 | 0.5814 | 0.5072 | 0.4484 | 0.4007 | 0.3612 | 0.3280 |  |  |
| $\mathbf{1 . 3 0}$ |  |  |  | 1.4393 | 1.0000 | 0.7750 | 0.6330 | 0.5339 | 0.4603 | 0.4035 | 0.3581 | 0.3211 | 0.2903 |  |  |
| $\mathbf{1 . 3 5}$ |  |  |  | 1.0000 | 0.7053 | 0.5521 | 0.4544 | 0.3855 | 0.3340 | 0.2940 | 0.2618 | 0.2355 |  |  |  |

Is $=1.4 \mathrm{lb}$

| lph/lbseq Itrip/lbseq | 1.85 | 1.90 | 1.95 | 2.00 | 2.20 | 2.40 | 2.60 | 2.80 | 3.00 | 3.20 | 3.40 | 3.60 | 3.80 | 4.00 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1.05 | 0.3829 | 0.3548 | 0.3300 | 0.3079 | 0.2396 | 0.1928 | 0.1590 | 0.1337 | 0.1142 | 0.0988 | 0.0864 | 0.0762 | 0.0678 | 0.0607 |
| 1.10 | 0.3673 | 0.3398 | 0.3155 | 0.2940 | 0.2278 | 0.1828 | 0.1505 | 0.1263 | 0.1078 | 0.0931 | 0.0814 | 0.0718 | 0.0638 | 0.0571 |
| 1.15 | 0.3490 | 0.3222 | 0.2986 | 0.2778 | 0.2143 | 0.1714 | 0.1408 | 0.1180 | 0.1005 | 0.0868 | 0.0758 | 0.0668 | 0.0593 | 0.0531 |
| 1.20 | 0.3269 | 0.3011 | 0.2786 | 0.2587 | 0.1985 | 0.1582 | 0.1296 | 0.1085 | 0.0923 | 0.0796 | 0.0694 | 0.0611 | 0.0543 | 0.0486 |
| 1.25 | 0.2997 | 0.2753 | 0.2541 | 0.2355 | 0.1796 | 0.1426 | 0.1165 | 0.0973 | 0.0827 | 0.0712 | 0.0621 | 0.0546 | 0.0485 | 0.0433 |
| 1.30 | 0.2643 | 0.2420 | 0.2228 | 0.2060 | 0.1561 | 0.1235 | 0.1006 | 0.0838 | 0.0711 | 0.0612 | 0.0533 | 0.0468 | 0.0415 | 0.0371 |
| 1.35 | 0.2135 | 0.1948 | 0.1788 | 0.1649 | 0.1240 | 0.0976 | 0.0793 | 0.0659 | 0.0558 | 0.0480 | 0.0417 | 0.0367 | 0.0325 | 0.0290 |

## Curves for initial heat rise $=100 \%$

Is $=\mathbf{2} \mathbf{l b}$

| Iph/lbseq Itrip/lbseq | 1.10 | 1.15 | 1.20 | 1.25 | 1.30 | 1.35 | 1.40 | 1.45 | 1.50 | 1.55 | 1.60 | 1.65 | 1.70 | 1.75 | 1.80 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1.05 | 19.2620 | 11.0020 | 7.6288 | 5.7866 | 4.6259 | 3.8286 | 3.2480 | 2.8069 | 2.4611 | 2.1831 | 1.9550 | 1.7648 | 1.6039 | 1.4663 | 1.3473 |
| 1.10 |  | 14.5120 | 8.9388 | 6.4398 | 5.0007 | 4.0622 | 3.4016 | 2.9118 | 2.5344 | 2.2351 | 1.9923 | 1.7915 | 1.6230 | 1.4797 | 1.3565 |
| 1.15 |  |  | 11.6100 | 7.4893 | 5.5392 | 4.3766 | 3.5996 | 3.0427 | 2.6238 | 2.2975 | 2.0364 | 1.8228 | 1.6451 | 1.4951 | 1.3669 |
| 1.20 |  |  |  | 9.6105 | 6.4010 | 4.8272 | 3.8656 | 3.2112 | 2.7355 | 2.3737 | 2.0892 | 1.8597 | 1.6709 | 1.5129 | 1.3788 |
| 1.25 |  |  |  |  | 8.1323 | 5.5465 | 4.2465 | 3.4375 | 2.8792 | 2.4688 | 2.1537 | 1.9041 | 1.7014 | 1.5337 | 1.3927 |
| 1.30 |  |  |  |  |  | 6.9855 | 4.8534 | 3.7614 | 3.0722 | 2.5911 | 2.2342 | 1.9582 | 1.7380 | 1.5583 | 1.4088 |
| 1.35 |  |  |  |  |  |  | 6.0646 | 4.2771 | 3.3484 | 2.7556 | 2.3380 | 2.0258 | 1.7828 | 1.5879 | 1.4280 |
| 1.40 |  |  |  |  |  |  |  | 5.3051 | 3.7883 | 2.9911 | 2.4776 | 2.1131 | 1.8388 | 1.6241 | 1.4511 |
| 1.50 |  |  |  |  |  |  |  |  |  | 4.1166 | 2.9979 | 2.3998 | 2.0090 | 1.7283 | 1.5149 |
| 1.60 |  |  |  |  |  |  |  |  |  |  |  | 3.2166 | 2.3778 | 1.9239 | 1.6242 |
| 1.70 |  |  |  |  |  |  |  |  |  |  |  |  |  | 2.4956 | 1.8670 |


| Iph/lbseq Itrip/lbseq | 1.85 | 1.90 | 1.95 | 2.00 | 2.20 | 2.40 | 2.60 | 2.80 | 3.00 | 3.20 | 3.40 | 3.60 | 3.80 | 4.00 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1.05 | 1.2436 | 1.1525 | 1.0718 | 1.0000 | 0.7783 | 0.6262 | 0.5165 | 0.4343 | 0.3709 | 0.3209 | 0.2806 | 0.2476 | 0.2202 | 0.1972 |
| 1.10 | 1.2495 | 1.1559 | 1.0733 | 1.0000 | 0.7750 | 0.6217 | 0.5118 | 0.4297 | 0.3666 | 0.3168 | 0.2768 | 0.2441 | 0.2170 | 0.1943 |
| 1.15 | 1.2562 | 1.1597 | 1.0750 | 1.0000 | 0.7713 | 0.6169 | 0.5066 | 0.4247 | 0.3618 | 0.3124 | 0.2727 | 0.2404 | 0.2136 | 0.1911 |
| 1.20 | 1.2638 | 1.1640 | 1.0768 | 1.0000 | 0.7673 | 0.6115 | 0.5010 | 0.4192 | 0.3567 | 0.3076 | 0.2683 | 0.2363 | 0.2099 | 0.1877 |
| 1.25 | 1.2725 | 1.1690 | 1.0790 | 1.0000 | 0.7628 | 0.6057 | 0.4949 | 0.4133 | 0.3511 | 0.3025 | 0.2636 | 0.2320 | 0.2059 | 0.1841 |
| 1.30 | 1.2826 | 1.1747 | 1.0814 | 1.0000 | 0.7578 | 0.5992 | 0.4882 | 0.4069 | 0.3451 | 0.2969 | 0.2585 | 0.2274 | 0.2017 | 0.1802 |
| 1.35 | 1.2945 | 1.1813 | 1.0842 | 1.0000 | 0.7522 | 0.5920 | 0.4808 | 0.3998 | 0.3386 | 0.2910 | 0.2531 | 0.2224 | 0.1971 | 0.1760 |
| 1.40 | 1.3085 | 1.1891 | 1.0874 | 1.0000 | 0.7459 | 0.5841 | 0.4728 | 0.3921 | 0.3315 | 0.2844 | 0.2471 | 0.2170 | 0.1922 | 0.1715 |
| 1.50 | 1.3463 | 1.2094 | 1.0958 | 1.0000 | 0.7306 | 0.5652 | 0.4539 | 0.3744 | 0.3152 | 0.2697 | 0.2337 | 0.2048 | 0.1811 | 0.1614 |
| 1.60 | 1.4070 | 1.2406 | 1.1082 | 1.0000 | 0.7102 | 0.5410 | 0.4303 | 0.3527 | 0.2955 | 0.2520 | 0.2178 | 0.1904 | 0.1681 | 0.1496 |
| 1.70 | 1.5237 | 1.2953 | 1.1286 | 1.0000 | 0.6816 | 0.5089 | 0.4000 | 0.3253 | 0.2711 | 0.2302 | 0.1983 | 0.1730 | 0.1524 | 0.1355 |



Dry-type transformer thermal model
The thermal limit for dry-type transformers is determined by the thermal limit for insulating components in order to avoid damaging them. The table below defines the maximum permissible temperature and the winding temperature gradient according to the insulation class:

| Insulation class $\left({ }^{\circ} \mathrm{C}\right)$ | Gradient $\Delta \boldsymbol{\theta} \mathbf{n}$ | Maximum permissible winding <br> temperature $\theta_{\text {max }}$ <br> $130^{\circ} \mathrm{C}\left(266^{\circ} \mathrm{F}\right)$ |
| :--- | :--- | :--- |
| $105(\mathrm{~A})$ | $75^{\circ} \mathrm{C}\left(67^{\circ} \mathrm{F}\right)$ | $145^{\circ} \mathrm{C}\left(293^{\circ} \mathrm{F}\right)$ |
| $120(\mathrm{E})$ | $90^{\circ} \mathrm{C}\left(194^{\circ} \mathrm{F}\right)$ | $155^{\circ} \mathrm{C}\left(311^{\circ} \mathrm{F}\right)$ |
| $130(\mathrm{~B})$ | $100^{\circ} \mathrm{C}\left(212^{\circ} \mathrm{F}\right)$ | $180^{\circ} \mathrm{C}\left(356^{\circ} \mathrm{F}\right)$ |
| $155(\mathrm{~F})$ | $125^{\circ} \mathrm{C}\left(257^{\circ} \mathrm{F}\right)$ | $180^{\circ}\left(500^{\circ} \mathrm{F}\right)$ |
| $180(\mathrm{H})$ | $150^{\circ} \mathrm{C}\left(302^{\circ} \mathrm{F}\right)$ | $205^{\circ} \mathrm{C}\left(400^{\circ} \mathrm{F}\right.$ |
| 200 | $170^{\circ} \mathrm{C}\left(338^{\circ} \mathrm{F}\right)$ | $225^{\circ} \mathrm{C}\left(437{ }^{\circ} \mathrm{F}\right)$ |
| 220 | $190^{\circ} \mathrm{C}\left(374^{\circ} \mathrm{F}\right)$ | $245^{\circ} \mathrm{C}\left(473^{\circ} \mathrm{F}\right)$ |

The winding maximum permissible thermal capacity used equals:
$\theta_{\text {max }}{ }^{-\theta}{ }_{\mathbf{a}}$
Where:
$\theta_{\mathbf{a}}$ : ambient temperature (rated value equals $20^{\circ} \mathrm{C}$ or $68^{\circ} \mathrm{F}$ )
$\Delta \theta \mathrm{n}$ : temperature gradient at rated current lb
${ }^{\theta}$ max : insulating component maximum permissible temperature according to the insulation class

The temperature build-up $\delta \theta$ in the dry-type transformer winding is calculated as follows:
$\mathbf{l e q} \geq 5 \% \mathrm{lb}: \delta \theta_{\mathbf{n}}=\delta \theta_{\mathbf{n - 1}}+\left[\Delta \theta n \cdot\left(\frac{\mathbf{l e q}}{\mathbf{l b}}\right)^{\mathbf{q}}-\delta \theta_{n-1}\right] \cdot \frac{\mathbf{d t}}{\tau}$
$l e q<5 \% \mathrm{lb}: \delta \theta_{\mathrm{n}}=\delta \theta_{\mathrm{n}-1} \cdot\left(1-\frac{\mathrm{dt}}{\tau}\right)$
Where:
$\tau$ : dry-type transformer time constant
$\mathbf{q}$ : equals 1.6 for transformers with natural cooling (AN) equals 2 for transformers with forced cooling (AF)

The protection trips when the temperature build-up $\delta \theta$ in the winding reaches
$\theta_{\max ^{-}}{ }_{\mathbf{a}}$.

## Evaluating the time constant

The thermal protection function protects the MV winding as well as the LV winding. Therefore the time constant $\tau$ corresponds to the lowest value of the MV winding and LV winding time constants.

The time constant is evaluated, for each winding, according to standard IEC 6007612 as follows:

$$
\tau=\frac{\mathbf{C} \cdot\left(\Delta \theta_{\mathbf{n}}-\theta_{\mathbf{e}}\right)}{\mathbf{P r}}
$$

Where:
Pr : total winding loss in Watts
C : winding thermal capacity in Watts min, given by the winding material:
■ Aluminum: 15 times weight of Al conductor $(\mathrm{kg})+24.5$ times weight of epoxy and other insulating component (kg)
■ Copper: 6.42 times weight of Cu conductor ( kg ) +24.5 times weight of epoxy and other insulating component (kg)
$\theta_{\mathbf{e}}$ : contribution of the core to the thermal capacity used:

- $5^{\circ} \mathrm{C}\left(41^{\circ} \mathrm{F}\right)$ for MV winding
- $25^{\circ} \mathrm{C}\left(77^{\circ} \mathrm{F}\right)$ for LV winding


## Example of a class B dry-type transformer:

Regardless of the winding material, the LV winding has the lowest time constant.
The following graph gives the values of the time constant $\tau$ for different $20 \mathrm{kV} / 410$
V dry-type transformer power ratings:

$20 \mathrm{kV} / 410 \mathrm{~V}$ dry-type transformer time constant.

## Saving the thermal capacity used

On loss of the auxiliary power supply, the winding thermal capacity used is saved.

## Operating information

The following information is available to the operator:
$\square$ the winding relative thermal capacity used E as a \%: $\mathbf{E}_{\mathbf{k}}=100 \cdot \frac{\theta_{\mathbf{k}}-\theta \mathbf{a}}{\Delta \theta_{\mathbf{n}}}$

- the time before tripping in minutes (at constant current)


## Accounting for ambient temperature

The characteristics of dry-type transformers are defined for an ambient temperature of $20^{\circ} \mathrm{C}\left(68^{\circ} \mathrm{F}\right)$. When the Sepam is equipped with the temperature sensor module option, the ambient temperature is measured by sensor no. 8 and added to the winding temperature.

## Characteristics

| Settings |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Measurement origin |  |  |  |  |
| Setting range | I1, I2, I3 / I'1, I'2, I'3 |  |  |  |
| Choice of transformer or thermal model |  |  |  |  |
| Setting range | Dry-type transformer |  |  |  |
|  | Natural ventilation (AN) |  |  |  |
|  | Forced ventilation (AF) |  |  |  |
|  | Generic model ${ }^{(1)}$ |  |  |  |
| Insulation class |  |  |  |  |
| Setting range | 105 (A) |  |  |  |
|  | 120 (E) |  |  |  |
|  | 130 (B) |  |  |  |
|  | 155 (F) |  |  |  |
|  | 180 (H) |  |  |  |
|  | 200 |  |  |  |
|  | 220 |  |  |  |
| Alarm set point ( $\theta$ alarm) |  |  |  |  |
| Setting range | class 105: $95^{\circ} \mathrm{C}$ to $130{ }^{\circ} \mathrm{C}\left(203{ }^{\circ} \mathrm{F}\right.$ to $\left.266{ }^{\circ} \mathrm{F}\right)$ |  |  |  |
|  | class 120: $110^{\circ} \mathrm{C}$ to $145^{\circ} \mathrm{C}\left(230^{\circ} \mathrm{F}\right.$ to $\left.293{ }^{\circ} \mathrm{F}\right)$ |  |  |  |
|  | class 130: $120^{\circ} \mathrm{C}$ to $155^{\circ} \mathrm{C}\left(248^{\circ} \mathrm{F}\right.$ to $\left.311^{\circ} \mathrm{F}\right)$ |  |  |  |
|  | class 155: $145^{\circ} \mathrm{C}$ to $180^{\circ} \mathrm{C}\left(293{ }^{\circ} \mathrm{F}\right.$ to $\left.356{ }^{\circ} \mathrm{F}\right)$ |  |  |  |
|  | class 180: $170{ }^{\circ} \mathrm{C}$ to $205^{\circ} \mathrm{C}\left(338^{\circ} \mathrm{F}\right.$ to $\left.401^{\circ} \mathrm{F}\right)$ |  |  |  |
|  | class 200: $190^{\circ} \mathrm{C}$ to $225{ }^{\circ} \mathrm{C}\left(374{ }^{\circ} \mathrm{F}\right.$ to $\left.437{ }^{\circ} \mathrm{F}\right)$ |  |  |  |
|  | class 220: $210^{\circ} \mathrm{C}$ to $245{ }^{\circ} \mathrm{C}\left(410^{\circ} \mathrm{F}\right.$ to $\left.473{ }^{\circ} \mathrm{F}\right)$ |  |  |  |
| Resolution | $1^{\circ} \mathrm{C}\left(1^{\circ} \mathrm{F}\right)$ |  |  |  |
| Tripping set point ( $\theta$ trip) |  |  |  |  |
| Setting range | class 105: $95^{\circ} \mathrm{C}$ to $130{ }^{\circ} \mathrm{C}\left(203^{\circ} \mathrm{F}\right.$ to $\left.266^{\circ} \mathrm{F}\right)$ |  |  |  |
|  | class 120: $110^{\circ} \mathrm{C}$ to $145^{\circ} \mathrm{C}\left(230^{\circ} \mathrm{F}\right.$ to $\left.293{ }^{\circ} \mathrm{F}\right)$ |  |  |  |
|  | class 130: $120^{\circ} \mathrm{C}$ to $155^{\circ} \mathrm{C}\left(248^{\circ} \mathrm{F}\right.$ to $\left.311^{\circ} \mathrm{F}\right)$ |  |  |  |
|  | class 155: $145{ }^{\circ} \mathrm{C}$ to $180^{\circ} \mathrm{C}\left(293{ }^{\circ} \mathrm{F}\right.$ to $\left.356{ }^{\circ} \mathrm{F}\right)$ |  |  |  |
|  | class 180: $170{ }^{\circ} \mathrm{C}$ to $205^{\circ} \mathrm{C}\left(338{ }^{\circ} \mathrm{F}\right.$ to $\left.401^{\circ} \mathrm{F}\right)$ |  |  |  |
|  | class 200: $190^{\circ} \mathrm{C}$ to $225{ }^{\circ} \mathrm{C}\left(374{ }^{\circ} \mathrm{F}\right.$ to $\left.437^{\circ} \mathrm{F}\right)$ |  |  |  |
|  | class 220: $210^{\circ} \mathrm{C}$ to $245^{\circ} \mathrm{C}\left(410^{\circ} \mathrm{F}\right.$ to $\left.473^{\circ} \mathrm{F}\right)$ |  |  |  |
| Resolution | $1^{\circ} \mathrm{C}\left(1^{\circ} \mathrm{F}\right)$ |  |  |  |
| Transformer time constant ( $\tau$ ) |  |  |  |  |
| Setting range | 1 min to 600 min |  |  |  |
| Resolution | 1 min |  |  |  |
| Accounting for ambient temperature |  |  |  |  |
| Setting range | yes/no |  |  |  |
| Characteristic times |  |  |  |  |
| Operating time accuracy | $\pm 2 \%$ or $\pm 1 \mathrm{~s}$ |  |  |  |
| Inputs |  |  |  |  |
| Designation | Syntax | Equations | Logipam |  |
| Reset protection | P49RMS_1_101 | - | ■ |  |
| Inhibit protection | P49RMS_1_113 | $\square$ | - |  |
| Outputs |  |  |  |  |
| Designation | Syntax | Equations | Logipam | Matrix |
| Time-delayed output | P49RMS_1_3 | - | - | - |
| Alarm | P49RMS_1_10 | - | - | - |
| Inhibit closing | P49RMS _1_11 | $\square$ | $\square$ | - |
| Protection inhibited | P49RMS_1_16 | - | - |  |
| Hot state | P49RMS_1_18 | $\square$ | $\square$ |  |
| Thermal overload inhibited | P49RMS_1_32 | - | - |  |
| Zero speed | P49RMS_1_38 | - | - |  |

(1) See settings associated with generic thermal overload.


Immersed transformer thermal model
The immersed transformer thermal model takes account of thermal exchanges between the winding and the oil. To this end IEC standard 60076-2 proposes a model for each of the transformer components:
■ a thermal model with 2 time constants for the winding

- a thermal model with 1 time constant for the oil.

The winding thermal model transfer function is as follows:


Where $\Delta \theta$ enr : winding temperature gradient at current lb
y : winding thermal capacity used exponent
$\begin{array}{ll}\kappa_{21} & : \text { thermal exchange coefficient between the winding and the oil } \\ \kappa_{22} & : \text { multiplying factor applied to the time constants } \\ \tau_{\mathrm{enr}} & : \text { winding time constant } \\ \tau_{\text {huile }} & : \text { oil time constant }\end{array}$

IEC standard 60076-7 proposes, depending on the nature of the immersed transformer, the following valuesz

| Transformer | $\kappa_{21}$ |  | $\Delta \theta \mathbf{e n r}$ | $\mathbf{y}$ | $\tau_{\text {enr }}$ | $\tau_{\text {huile }}$ |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| ONAN (distribution) | 1 | 2 | $23^{\circ} \mathrm{C}$ | 1,6 | 4 min | 180 min |
| ONAN (power) | 2 | 2 | $26^{\circ} \mathrm{C}$ | 1,3 | 10 min | 210 min |
| ONAF | 2 | 2 | $26^{\circ} \mathrm{C}$ | 1,3 | 7 min | 150 min |
| OF | 1.3 | 1 | $22^{\circ} \mathrm{C}$ | 1,3 | 7 min | 90 min |
| OD | 1 | 1 | $29^{\circ} \mathrm{C}$ | 2 | 7 min | 90 min |
| N |  |  |  |  |  |  |

Note: For distribution ONAN and OD transformers, the winding thermal model only reacts with the winding time constant.

When the winding and oil time constants are given by the immersed transformer manufacturer, the user can enter them in place of the default values proposed by the standard.
For transformers in which the oil flow can be restricted, exchanges between the winding and the oil are worse, so the winding thermal capacity used values are exceeded. In this case coefficient $\kappa_{21}$ takes the following values:

| Transformer | Restricted flow |  |
| :--- | :--- | :--- |
|  | OFF | ON |
| ONAN (power) | 2 | 3 |
| ONAF | 2 | 3 |
| OF | 1,3 | 1,45 |

## Accounting for ambient temperature

The characteristics of immersed transformers are defined for an ambient temperature of $20^{\circ} \mathrm{C}\left(68^{\circ} \mathrm{F}\right)$. When the Sepam is equipped with the temperature sensor module option, the ambient temperature is measured by sensor no. 8 and added to the oil temperature rise.

The oil thermal model transfer function is as follows:


Where $\Delta \theta$ ho : oil temperature gradient at current lb
$\mathbf{R}$ : ratio between the on-load losses and the no-load losses
$\mathbf{x} \quad$ : oil thermal capacity used exponent
$\kappa_{11}$ : multiplying factor applied to the oil time constant

IEC standard 60076-7 proposes, depending on the nature of the immersed transformer, the following values:

| Transformer | $\kappa_{11}$ | $\Delta \theta \mathbf{h o}$ | $\mathbf{x}$ | $\mathbf{R}$ |
| :--- | :--- | :--- | :--- | :--- |
| ONAN (distribution) | 1 | $55^{\circ} \mathrm{C}$ | 0,8 | 5 |
| ONAN (power) | 0,5 | $52^{\circ} \mathrm{C}$ | 0,8 | 6 |
| ONAF | 0,5 | $52^{\circ} \mathrm{C}$ | 0,8 | 6 |
| OF | 1 | $56^{\circ} \mathrm{C}$ | 1 | 6 |
| OD | 1 | $49^{\circ} \mathrm{C}$ | 1 | 6 |

## Taking account of the oil temperature

When the Sepam is equipped with the temperature sensor module option, sensor no. 8 can be assigned to the oil temperature measurement. In this case the oil
temperature measurement is substituted for the oil thermal model. The measured oil temperature $\theta_{\text {oil }}$ is added to the winding temperature rise.

## Saving the thermal capacity used

On loss of the auxiliary power supply, both the winding and oil thermal capacity used are saved.

## Operating information

The following information is available to the operator:

- the time before tripping in minutes (at constant current)
- the relative thermal capacity used $\mathbf{E}_{\mathbf{k}}$ of the transformer expressed as a \%:
$\square$ when the oil temperature is estimated by a calculation:

$$
\mathbf{E}_{\mathbf{k}}=100 \cdot \frac{\theta_{\mathbf{k}}-\theta_{\text {ambiant }}}{\Delta \theta \text { enr }+\Delta \theta \text { ho }}
$$

- when the oil temperature is measured:
$\mathbf{E}_{\mathbf{k}}=100 \cdot \frac{\theta_{\mathbf{k}}-\theta_{\text {huile }}}{\Delta \theta \mathbf{e n r}}$


## Characteristics

| Settings |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Measurement origin |  |  |  |  |
| Setting range $\quad 11, \mathrm{I} 2, \mathrm{I} / \mathrm{l} \mathrm{I}^{\prime} 1, \mathrm{I} 2$, I'3 |  |  |  |  |
| Choice of transformer or thermal model |  |  |  |  |
| Setting range | Immersed transformer |  |  |  |
|  | ONAN (distribution) |  |  |  |
|  | ONAN (power) |  |  |  |
|  | ONAF |  |  |  |
|  | OD |  |  |  |
|  | OF |  |  |  |
|  | Generic model(1) |  |  |  |
| Alarm set point ( $\theta$ alarm) |  |  |  |  |
| Setting range | Immersed transfo: | $98{ }^{\circ} \mathrm{C}$ to $160^{\circ} \mathrm{C}\left(208{ }^{\circ} \mathrm{F}\right.$ to $\left.320{ }^{\circ} \mathrm{F}\right)$ |  |  |
|  | Dry-type transfo: $\quad 95^{\circ} \mathrm{C}$ to $245^{\circ} \mathrm{C}\left(203{ }^{\circ} \mathrm{F}\right.$ to $\left.473{ }^{\circ} \mathrm{F}\right)$ |  |  |  |
| Resolution | $1^{\circ} \mathrm{C}\left(1^{\circ} \mathrm{F}\right)$ |  |  |  |
| Tripping set point ( $\theta$ trip) |  |  |  |  |
| Setting range | Immersed transfo: $98{ }^{\circ} \mathrm{C}$ to $160^{\circ} \mathrm{C}\left(208{ }^{\circ} \mathrm{F}\right.$ to $\left.320{ }^{\circ} \mathrm{F}\right)$ |  |  |  |
|  | Dry-type transfo: $\quad 95^{\circ} \mathrm{C}$ to $245^{\circ} \mathrm{C}\left(203^{\circ} \mathrm{F}\right.$ to $\left.473{ }^{\circ} \mathrm{F}\right)$ |  |  |  |
| Resolution | $1^{\circ} \mathrm{C}\left(1^{\circ} \mathrm{F}\right)$ |  |  |  |
| Winding time constant ( $\tau_{\text {enr }}$ ) |  |  |  |  |
| Setting range | 1 mn to 600 mn |  |  |  |
| Resolution | 1 min |  |  |  |
| Oil time constant ( $\tau_{\text {huile }}$ ) |  |  |  |  |
| Setting range | 5 mn to 600 mn |  |  |  |
| Resolution | 1 min |  |  |  |
| Accounting for ambient temperature |  |  |  |  |
| Setting range | yes / no |  |  |  |
| Accounting for oil temperature |  |  |  |  |
| Setting range | yes/no |  |  |  |
| Restricted oil flow |  |  |  |  |
| Setting range | on / off |  |  |  |
| Characteristic times |  |  |  |  |
| Operating time accuracy | $\pm 2 \%$ or $\pm 1 \mathrm{~s}$ |  |  |  |
| Inputs |  |  |  |  |
| Designation | Syntax | Equations | Logipam |  |
| Reset protection | P49RMS_1_101 | ■ | $\square$ |  |
| Inhibit protection | P49RMS_1_113 | - | - |  |
| Outputs |  |  |  |  |
| Designation | Syntax | Equations | Logipam | Matrix |
| Time-delayed output | P49RMS_1_3 | ■ | $\square$ | $\square$ |
| Alarm | P49RMS _1_10 | $\square$ | - | $\square$ |
| Inhibit closing | P49RMS_1_11 | $\square$ | $\square$ | $\square$ |
| Protection inhibited | P49RMS_1_16 | - | - |  |
| Hot state | P49RMS_1_18 | $\square$ | - |  |
| Thermal overload inhibited | P49RMS_1_32 | - | - |  |
| Zero speed | P49RMS_1_38 | - | - |  |
| (1) See settings associated with generic thermal overload. |  |  |  |  |
| Glossary of transformer type abbreviations: <br> ■ AN: air-cooled transformer with natural ventilation <br> - AF: air-cooled transformer with forced ventilation <br> ■ ONAN: transformer immersed in mineral oil, cooled by natural air convection <br> - ONAF: transformer immersed in oil with forced circulation <br> ■ OD: transformer immersed in oil with forced circulation, directed into the windings <br> ■ OF: transformer immersed in oil with forced circulation |  |  |  |  |

## Protection functions

Thermal overload for motors ANSI code 49RMS

## Operation

This function is used to protect the stator and the rotor of an asynchronous motor.

## Block diagram

The stator thermal overload protection is provided by a thermal model with 2 time constants ( $\tau$ long and $\tau$ short).
The rotor excessive starting time thermal protection is provided by an adiabatic thermal model.


## Blocking of tripping and closing inhibition

The protection tripping and inhibit closing outputs can be inhibited by:
■ an "Inhibit thermal overload" latched logic input
■ an "Authorize emergency restart" latched logic input

- an "Inhibit thermal overload" remote control order (TC).


## Start inhibit

When the protection trips, circuit breaker closing is inhibited until the rotor thermal capacity used allows another motor start.
This inhibit is grouped together with the "Starts per hour" protection function, and signaled by the message "INHIBIT START".
The inhibit time before starting is authorized can be accessed from:
■ the "Machine diagnosis" tab in the SFT2841 software

- the Sepam front panel.


## "Hot state" set point

The thermal overload function provides a "hot state" data item used by the starts per hour function (ANSI code 66). It is used to distinguish between cold starts and hot starts. The number of consecutive starts per hour is stated by the motor manufacturer.
Depending on the manufacturer, the previous load current defining hot state varies between 0.6 lb and lb . Hence the "hot state" set point can be adjusted to suit the motor characteristics.

## Saving the thermal capacity used

On loss of the auxiliary power supply, the thermal capacity used of the rotor W , the stator $E$ and the metal frame $M$ are saved and reused in their current state until the relay is re-energized.

## Operating information

The following information can be accessed from the "Machine diagnosis" tab in the SFT2841 software and the Sepam front panel:

- the stator thermal capacity used
- the time before the stator protection trips (at constant current)
- the time before restarting is authorized.


## Protection functions

Thermal overload for motors ANSI code 49RMS

| Settings |  |
| :---: | :---: |
| Measurement origin |  |
| Setting range 11, 12,13 |  |
| Choice of thermal model |  |
| Setting range 2 Constant |  |
| Generic ${ }^{(1)}$ |  |
| Thermal model switching threshold | Is_therm |
| Setting range 1 to 10 pu of lb |  |
| Resolution 0.1 pu of lb |  |
| Stator thermal settings |  |
| Motor thermal capacity used time constant | $\tau_{\text {long }}$ |
| Setting range 1 mn to 600 mn |  |
| Resolution 1 mn |  |
| Stator thermal capacity used time constant | $\tau_{\text {short }}$ |
| Setting range 1 mn to 60 mn |  |
| Resolution 0,1 mn |  |
| Cooling time constant | $\tau_{\text {cool }}$ |
| Setting range 5 mn to 600 mn |  |
| Resolution 1 mn |  |
| Tripping current set point | Itrip |
| Setting range $50 \%$ to $173 \%$ of lb |  |
| Resolution $1 \%$ of lb |  |
| Alarm current set point | lalarm |
| Setting range $50 \%$ to $173 \%$ of lb |  |
| Resolution $1 \%$ of lb |  |
| Thermal exchange coefficient between the stator and the motor | $\alpha$ |
| Setting range 0 to 1 |  |
| Resolution 0.01 |  |
| Hot state set point |  |
| Setting range 0.5 to 1 pu of lb |  |
| Resolution 0.01 pu of lb |  |
| Accounting for ambient temperature |  |
| Setting range Yes / No |  |
| Maximum equipment temperature (insulation class) | Tmax |
| Setting range $70^{\circ} \mathrm{C}$ to $250^{\circ} \mathrm{C}$ or <br>  $158^{\circ} \mathrm{F}$ to $482^{\circ} \mathrm{F}$ |  |
| Resolution $\quad 1^{\circ} \mathrm{C}$ or $1^{\circ} \mathrm{F}$ |  |
| Rotor thermal settings |  |
| Locked rotor amperes | IL |
| Setting range 1 to 10 pu of lb |  |
| Resolution 0.01 pu of lb |  |
| Locked rotor torque | LRT |
| Setting range 0.2 to 2 pu of lb |  |
| Resolution 0.01 pu of lb |  |
| Locked cold rotor limit time | Tc |
| Setting range 1 s to 300 s |  |
| Resolution 0.1 s |  |
| Locked hot rotor limit time | Th |
| Setting range 1 s to 300 s |  |
| Resolution 0.1 s |  |
| Characteristic times |  |
| $\begin{aligned} & \text { Operating time } \\ & \text { accuracy }\end{aligned} \quad \pm 2 \%$ or $\pm 1 \mathrm{~s}$ |  |


| Inputs |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- |
| Designation | Syntax | Equations | Logipam |  |
| Reset protection | P49RMS_1_101 | ■ | ■ |  |
| Inhibit protection | P49RMS_1_113 | ■ | ■ |  |
| Outputs |  |  |  |  |
| Designation | Syntax | Equations | Logipam | Matrix |
| Time-delayed output | P49RMS_1_3 | ■ | ■ | ■ |
| Alarm | P49RMS_1_10 | ■ | ■ | ■ |
| Inhibit closing | P49RMS_1_11 | ■ | ■ | ■ |
| Protection inhibited | P49RMS_1_16 | ■ | ■ |  |
| Hot state | P49RMS_1_18 | ■ | ■ |  |
| Thermal overload inhibited | P49RMS_1_32 | ■ | ■ |  |
| Zero speed | P49RMS_1_38 | ■ | ■ |  |

1 Selection of the motor / generic thermal overload protection function
2 Switching threshold between the stator and rotor thermal models (Is_therm)
3 Rotor thermal model parameters
4 Stator thermal model parameters
5 Calculated stator thermal model parameters

## Help with parameter setting

The function parameters are set using the motor manufacturer data and the SFT2841 software (49RMS tab in the protection functions).


SFT2841 software: 49RMS protection parameter-setting screen for a motor application.

## Parameter-setting procedure

1. Select the thermal overload protection function by choosing the
"2 Time constants" value from the "Thermal Model" drop-down list.
Note: The "Generic" value selects the generic thermal overload protection function (see page 153 to set the parameters for this protection function).
2. Enter the rotor and stator parameters using the motor manufacturer data.

- Rotor parameters:
- Locked cold rotor limit time (Tc)
- Locked hot rotor limit time (Th)
$\square$ Locked rotor torque (LRT)
$\square$ Starting current (IL)
■ Stator parameters:
- Heating time constant: $\tau$ long
$\square$ Cooling time constant: $\tau$ cool

3. Determine in graphic form the switching threshold between the stator and rotor thermal models (Is_therm).
Depending on the manufacturer curves, there are 2 possible scenarios:
■ If there is any discontinuity between the manufacturer curves (see example on next page), choose Is_therm at the stator breaking point.
■ If there is no discontinuity:

- Plot the locked cold rotor thermal model curve, between IL and Ib, using the equation below in order to determine Is_therm:
$\mathrm{W}(\mathrm{I})=\mathrm{Tc} x(\mathrm{IL} / \mathrm{I})^{2}$
- Determine the value of Is_therm for which the rotor thermal model (adiabatic) no longer corresponds to the manufacturer's locked cold rotor curve.


Determination of Is_therm in the case of discontinuous manufacturer curves.

Itrip: permissible continuous current and tripping set point in pu of lb
IL: starting current in pu of Ib
Tc: Locked cold rotor limit time
Th: Locked hot rotor limit time
4. Determine the following stator parameters:

■ Tripping current set point Itrip

- Stator thermal capacity used time constant $\tau$ short

■ Thermal exchange coefficient $\alpha$
If these parameters are not available, proceed as follows to calculate them using the SFT2841 software:
4.1. Press the "Use Genetic Algorithm" button which can be accessed from the 49RMS tab in the protection functions.
4.2. Enter 4 typical points found on the manufacturer's cold stator curve.
4.3. Press the "Use Genetic Algorithm" button: the SFT2841 software calculates all 3 parameters.

Example of parameter setting no. 1: $3100 \mathrm{~kW} / 6.3 \mathrm{kV}$ motor
We have the following manufacturer data:

| Parameter | Name | Value | Rotor / stator |
| :--- | :--- | :--- | :--- |
| insulation class |  | F | - |
| rated current | IL | 5.6 lb | - |
| starting current | Tn | $19,884 \mathrm{Nm}$ | rotor |
| rated torque | LRT | 0.7 Tn | rotor |
| starting torque | $\tau$ long | 90 minutes | rotor |
| motor time constant | $\tau$ cool | 300 minutes | stator |
| cooling constant | $\mathrm{Tc} / \mathrm{Th}$ | $29 \mathrm{~s} / 16.5 \mathrm{~s}$ | rotor |
| locked cold / hot rotor limit time |  | 2.3 s | - |
| starting time |  | $3(2)$ | - |
| number of consecutive <br> cold (hot) starts |  |  |  |

## Setting the function parameters

1. Selection of "2 Time constants" from the "Thermal Model" drop-down list to select the motor thermal overload protection function.
2. Set the rotor and stator model parameters using the manufacturer data:

| Rotor parameter | Name | Value |
| :--- | :--- | :--- |
| Locked cold rotor limit time | Tc | 29 s |
| Locked hot rotor limit time | Th | 16.5 s |
| Locked rotor torque | LRT | 0.7 pu rated torque |
| Starting current | IL | 5.6 lb |
| Stator parameter | Name | Value |
| Alarm current set point | lalarm | $<$ ltrip |
| Heating time constant | $\tau$ long | 90 minutes |
| Cooling time constant | $\tau$ cool | 300 minutes |

3. Determination of Is_therm switching threshold between the 2 models: In this example there is a clear distinction between the rotor and stator manufacturer curves.
Therefore the Is_therm switching threshold at the rotor curve breaking point is selected.
Hence Is_therm = 2.8 lb


## 4. Determination of the stator parameters:

For example on the cold stator curve (previous graphic) the following 4 points are selected, spread between Ib and Is_therm:

| $\mathbf{I} / \mathbf{l} \mathbf{b}$ | Ttrip |
| :--- | :--- |
| 1.4 | 6000 s |
| 1.8 | 1500 s |
| 2.4 | 400 s |
| 2.8 | 250 s |

The SFT2841 software calculates the missing stator parameters on the basis of these 4 points:

| Calculated stator parameter | Name | Value |
| :--- | :--- | :--- |
| Tripping current set point | Itrip | 1.2 lb |
| Stator heating time constant | $\tau$ short | 5.5 mn |
| Thermal exchange coefficient between stator and motor $\alpha$ | 0.7 |  |

The function parameter setting is complete:

On the graphic below the manufacturer curves are bold lines, whereas the curves generated from the configured model are fine lines.
The function protects the motor beyond its stated characteristics.


Comparison of the manufacturer curves and the configured model.

Example of parameter setting no. 2: 600 kW / 6 kV motor
We have the following manufacturer data:

| Parameter | Name | Value | Rotor / stator |
| :--- | :--- | :--- | :--- |
| insulation class |  | F | - |
| rated current | IL | 69.9 A | - |
| starting current | Tn | 392.2 kgm | rotor |
| rated torque | LRT | 0.9 Tn | rotor |
| starting torque | $\tau$ long | 60 minutes | stator |
| motor time constant | $\tau$ cool | 180 minutes | stator |
| cooling constant | Tc / Th | $33.5 \mathrm{~s} / 25 \mathrm{~s}$ | rotor |
| $\left.\begin{array}{llll}\text { locked cold / hot rotor limit time } & & 1.2 \mathrm{~s} & - \\ \hline \begin{array}{l}\text { starting time }\end{array} & 2(1) & - \\ \hline \begin{array}{l}\text { number of consecutive } \\ \text { cold (hot) starts }\end{array} & & & \end{array}\right]$ |  |  |  |

Setting the function parameters

1. Selection of the " 2 Time constants" value from the "Thermal Model" drop-down list to select the motor thermal overload protection function.
2. Set the rotor and stator parameters using the manufacturer data:

| Rotor parameter | Name | Value |
| :--- | :--- | :--- |
| Locked cold rotor limit time | Tc | 33.5 s |
| Locked hot rotor limit time | Th | 25 s |
| Locked rotor torque | LRT | 0.9 pu rated torque |
| Starting current | IL | 6 lb |
| Stator parameter | Name | Value |
| Alarm current set point | lalarm | $<$ Itrip |
| Heating time constant | $\tau$ long | 60 minutes |
| Cooling time constant | $\tau$ cool | 180 minutes |



In this example the rotor and stator manufacturer curves (in bold lines) merge into one another.
We therefore plot the rotor model curves (in fine lines) defined by:

- cold curve
$W(I)=33,5 \cdot(6 / I)^{2}$
- hot curve
$W(I)=25 \cdot(6 / I)^{2}$

We can see that the rotor model curve coincides with the manufacturer curve over the whole current range $\mathrm{I} / \mathrm{lb}$.
We therefore select the Is_therm switching threshold $=1.01 \mathrm{lb}$.
The rotor model thus protects the motor over its whole operating range.
4. Determination of the stator parameters:

The SFT2841 software calculates the following stator parameters:

| Calculated stator parameter | Name | Value |
| :--- | :--- | :--- |
| Tripping current set point | Itrip | 1.01 lb |
| Stator heating time constant | $\tau$ short | 60 Minutes |
| Thermal exchange coefficient between stator and motor | $\alpha$ | 1 |

In this example, the stator thermal overload protection is only used to define the thermal state of the motor, in order to be able to:
■ change the locked cold rotor limit time value to its corresponding hot value
■ define the hot / cold thermal state of the motor.
The function parameter setting is complete.


Stator thermal model.
$\mathrm{rl}_{\mathrm{eq}}{ }^{2}$ : heat generated by the copper losses at equivalent current leq
C1 : stator thermal capacity
R1 : thermal resistance between the stator and the motor metal frame
C2 : motor thermal capacity
R2 : motor thermal resistance
$\theta$ a : ambient temperature
$\theta c u \quad$ : stator winding temperature
Өfe : motor metal frame temperature
$\tau$ short $=$ R1C1: stator winding time constant
$\tau$ long $=$ R2C2 : motor metal frame time constant

## Stator thermal model

The stator thermal model takes account of thermal exchanges between the stator winding and the motor metal frames using 2 time constants.

Having used $\alpha$ to designate the ratio $\mathrm{R} 2 /(\mathrm{R} 1+\mathrm{R} 2)$, the stator winding relative thermal capacity used $E$ transfer function is expressed as follows:
$\mathbf{E}(\mathbf{p})=\left[\frac{(1-\alpha)}{\left(1+\mathbf{p} \tau_{\text {short }}\right)}+\frac{\alpha}{\left(1+\mathbf{p} \tau_{\text {long }}\right)}\right]$
where $0<\alpha<1$.
The thermal model time response with two time constants is proportional to the square of the current.


The stator thermal overload protection trips when $\mathrm{E}\left(\mathrm{l}_{\text {eq }}, \mathrm{t}\right)=\mathrm{K}^{2}, \mathrm{~K}$ being the permissible continuous current in pu of lb.
For $\alpha=0$, there is no thermal exchange between the stator and the metal frame since the motor thermal resistance R2 is zero. Thus the stator heats up with the lowest time constant $\tau$ short.
Conversely for $\alpha=1$, the thermal exchange between the stator and the metal frame is perfect, therefore the stator and the metal frame only make one, resulting in the stator heating up with a time constant close to that of the metal frame $\tau$ long.
For $0<\alpha<1$, thermal management with 2 time constants makes it possible:

- to protect the stator winding correctly against strong overloads, since the resulting time constant is close to the stator time constant
- for the motor to run at low overload as close as possible to the limits defined by the manufacturer data, since the resulting time constant is close to that of the metal frame.

Illustration of the influence of the $\alpha$ coefficient on a motor whose time constants are as follows:
■ stator winding: $\tau$ short $=4 \mathrm{mn}$
■ metal frame: $\tau$ long $=60 \mathrm{mn}$.

Ttrip in sec


## Stator thermal model (continued)

## Equivalent current $\mathrm{l}_{\mathrm{eq}}$

The presence of a negative sequence component accelerates the motor temperature build-up. The current negative sequence component is taken into account in the protection function by the equation
$I_{e q}=\sqrt{\left(\frac{I d}{I b}\right)^{2}+K i \cdot\left(\frac{I i}{I b}\right)^{2}}$
where Id is the current positive sequence component
li is the current negative sequence component
lb is the motor rated current
Ki is the negative sequence component coefficient.
For an asynchronous motor, Ki is calculated using the following parameters:

- LRT: locked rotor torque in pu of the rated torque
- IL: starting current in pu of the rated current lb
- N: rated speed in rpm.

The number of pairs of poles $n p$ is defined by the expression:
$\mathrm{np}=\operatorname{int}\left(\frac{60 \cdot \mathrm{fn}}{\mathrm{N}}\right)$

The rated slip $g_{n}$ is defined by the expression:
$g_{n}=1-\frac{N \cdot n p}{60 \cdot f n}$
where fn is the network frequency in Hz .

The coefficient Ki is defined by the expression:
$K i=2 \frac{L R T}{g_{n} \cdot I_{L}^{2}}-1$

## Accounting for ambient temperature

Asynchronous motors are designed to run at a maximum ambient temperature of $40^{\circ} \mathrm{C}\left(104^{\circ} \mathrm{F}\right)$. Where Sepam is equipped with the temperature sensor module option (with sensor no. 8 assigned to measuring the ambient temperature), the stator thermal capacity used is multiplied by the correction factor fcorr, from the time when the ambient temperature is higher than $40^{\circ} \mathrm{C}$.
$\mathrm{fcorr}=\frac{\mathrm{T}_{\text {max }-40}^{T_{\text {max }^{-}} \mathrm{T}_{\text {ambiant }}}}{\text { and }}$
where Tmax is the maximum temperature in the thermal class for the motor insulating components defined in accordance with standard 60085.

| Class | $\mathbf{7 0}$ | Y | A | E | B | F | H | $\mathbf{2 0 0}$ | $\mathbf{2 2 0}$ | $\mathbf{2 5 0}$ |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Tmax in $^{\circ} \mathbf{C}$ | 70 | 90 | 105 | 120 | 130 | 155 | 180 | 200 | 220 | 250 |
| Tmax in $^{\circ} \mathbf{F}$ | 158 | 194 | 221 | 248 | 266 | 311 | 356 | 392 | 428 | 482 |

## Stator thermal model (continued)

Metal frame thermal capacity used
Having used $\beta$ to designate the ratio $\frac{{ }^{\tau} \text { long }}{\tau_{\text {long }}{ }^{-\tau} \text { short }}$
the motor metal frame relative thermal capacity used $M$ transfer function is expressed as follows:
$\mathbf{M}(\mathbf{p})=\left[\frac{(1-\beta)}{\left(1+\mathbf{p} \tau_{\text {short }}\right)}+\frac{\beta}{\left(1+\mathbf{p} \tau_{\text {long }}\right)}\right]$
where $\beta>1$.

Example: Starting with a zero initial thermal capacity used and applying a current the same as the rated current lb , the stator and metal frame relative thermal capacity used reach $100 \%$.

Initially, the metal frame thermal capacity used has a zero slope, until the heat transfer is established between the stator and the metal frame.


Stator and metal frame thermal capacity used for a load current lb.
The metal frame relative thermal capacity used is used to:

- adapt the rotor protection rotor limit time
- define the hot state of the motor.


## Cooling time constant

When the current leq is less than $5 \%$ of lb , the motor is deemed to have stopped. In this case it is the cooling time constant $\tau$ cool of the metal frame that is taken into account to estimate stator cooling.


## Steinmetz diagram.

Rs: stator resistance
Xs: stator reactance
Rr: rotor resistance
Xr: rotor reactance
Rm: magnetic loss
Xm: magnetizing reactance g : slip

## Rotor thermal model

For the rotor, guide IEEE C37.96-2000 on protection of asynchronous motors defines an adiabatic thermal model, dependent on the slip, which is based on the equivalent Steinmetz diagram.

During the asynchronous motor starting phase, rotoric currents travel across the rotor conductors to a depth that depends on the slip.
Therefore the rotor inductance Xr and the rotor resistance $\operatorname{Rr}$ vary as a function of the slip $g$ as follows:
$\mathrm{Rr}=\mathrm{Krg}+\mathrm{Ro}$
$X r=K x g+X o$
Kr: coefficient taking account of the increase in the rotor resistance
Kx : coefficient taking account of the decrease in the rotor reactance


Coefficients $K r$ and $K x$ as a function of the slip.

Assuming that the positive sequence rotor resistance $\mathrm{Rr}+$ varies almost linearly between Ro and R1:

$$
\mathbf{R}_{\mathbf{r}+}=\left(\mathbf{R}_{\mathbf{1}}-\mathbf{R}_{\mathbf{0}}\right) \cdot \mathbf{g}+\mathbf{R}_{\mathbf{0}}
$$

The proportion of negative sequence current can be high during the motor starting phase. As a result the negative sequence rotor resistance Rr - is high in order to evaluate the rotor thermal capacity used.
It is obtained by replacing the slip $g$ with the negative slip sequence $(2-\mathrm{g})$. Thus:
$\mathbf{R}_{\mathbf{r}-}=\left(\mathbf{R}_{\mathbf{1}}-\mathbf{R}_{\mathbf{0}}\right) \cdot(\mathbf{2}-\mathbf{g})+\mathbf{R}_{\mathbf{0}}$

The thermal model used in the Sepam relay measures the active part of the positive sequence impedance during the motor starting phase to evaluate the slip g.

Depending on the motor status, the positive and negative sequence rotor resistances are as follows:

| Motor status | $\mathbf{R}_{\mathbf{r}+}$ | $\mathbf{R}_{\mathbf{r}}$ |
| :--- | :--- | :--- |
| Stop $\mathbf{g}=\mathbf{1})$ | $\mathrm{R}_{1}$ | $\mathrm{R}_{1}$ |
| Rated speed $\mathbf{( g} \approx \mathbf{0})$ | $\mathrm{R}_{0}$ | $2 \mathrm{R}_{1}-\mathrm{R}_{0}$ |

## Rotor thermal model (continued)

The mechanical power developed by the motor equals the electrical power drawn in the resistance $\operatorname{Rr}(1-\mathrm{g}) / \mathrm{g}$.
The torque $Q$ equals:
$Q=\frac{P}{w}=\frac{P}{1-g}=\frac{\frac{R_{r}(g) \cdot(1-g)}{g} \cdot I_{L}^{2}}{1-g}=I_{L}^{2} \cdot \frac{R_{r}(g)}{g}$
Thus:
$R_{\mathbf{r}}(\mathbf{g})=\frac{\mathbf{Q}}{\mathrm{I}_{L}^{2}} \cdot \mathbf{g}$
When the motor has stopped, $g=1$. We can therefore deduce that:
$R_{1}=\frac{L R T}{I_{L}^{2}} \quad$ (in pu of Zn )
Where LRT: locked rotor torque in pu of the rated torque
l: locked rotor current in pu of lb
When the motor is at rated speed, the torque $Q$ equals the rated torque $Q n$ and the current equals the rated current In , thus $\mathrm{R}_{0}=\mathrm{g}_{\mathrm{n}}$ (in pu of Zn ).
Where:
$\mathbf{Z n}=\frac{\mathbf{U n}}{\sqrt{3} \mathrm{Ib}}$
$g_{n}$ : rated slip

When the motor is at its rated speed of rotation, the ratio between the positive and negative sequence resistances is:
$2 \frac{R_{1}}{R_{0}}-1=2 \frac{L R T}{g_{n} \cdot I_{L}^{2}}-1$

During the starting phase the rotor thermal capacity used W is defined by the following expression:
$W_{n}=W_{n-1}+\left[\frac{R_{r}}{R_{1}}\left(\frac{I d}{I_{L}}\right)^{2}+\frac{R_{r}}{R_{1}}\left(\frac{I}{} I_{L}\right)^{2}\right] \cdot \frac{d t}{T(M)}$
Where $T(M)$ : locked rotor limit time depends on the thermal state of the motor $M$ :
$T(M)=T c-(T c-T h) \times M$, where $0 \leq M \leq 1$.
Tc: locked cold rotor limit time at the starting current $I_{L}$
Th: locked hot rotor limit time at the starting current $\mathrm{I}_{\mathrm{L}}$.
Example for a motor whose starting time is 5 s and the locked cold rotor limit time is 20 s.
■ When the rotor is locked, the slip $\mathrm{g}=1$, as a result $\mathrm{Rr}+=\mathrm{R} 1$. Thus the thermal capacity used is $5 / 20=25 \%$.

- When the slip g changes from 1 to 0 in 5 s , the rotor thermal capacity used is $17 \%$.


Comparison of the rotor thermal capacity used during normal starting with locked rotor.

Protection of equipment against thermal damage caused by overloads.

## Description

This function is used to protect equipment (motors, transformers, generators) against overloads, based on measurement of the current drawn.

## Operation curve

The protection issues a trip order when the heat rise E, calculated according to the measurement of an equivalent current leq, is greater than the set point Es.
The greatest permissible continuous current is
$\mathbf{I}=\mathbf{I b} \sqrt{E s}$
The protection tripping time is set by the time constant T .

- the calculated heat rise depends on the current drawn and the previous heat rise ■ the cold curve defines the protection tripping time based on zero heat rise
■ the hot curve defines the protection tripping time based on $100 \%$ rated heat rise.


$$
\begin{aligned}
& \frac{t}{T}=\ln \frac{\left(\frac{\mathrm{leq}}{\mathrm{lb}}\right)^{2}}{\left(\frac{\mathrm{leq}}{\mathrm{Ib}}\right)^{2}-E s} \\
& \frac{t}{\mathrm{t}}=\ln \frac{\left(\frac{\mathrm{leq}}{\mathrm{Ib}}\right)^{2}-1}{\left(\frac{\mathrm{leq}}{\mathrm{Ib}}\right)^{2}-E s}
\end{aligned}
$$

## Alarm set point, tripping set point

Two set points are available for heat rise:
■ Es1: alarm

- Es2: tripping.


## "Hot state" set point

When the function is used to protect a motor, this fixed set point is designed for detection of the hot state used by the number of starts function. The value of the fixed set point is $50 \%$.

Heat rise and cooling time constants


Heat rise time constant.


Cooling time constant.

For self-ventilated rotating machines, cooling is more effective when the machine is running than when it is stopped. Running and stopping of the equipment are calculated based on the value of the current:
■ running if I $>0.1 \mathrm{lb}$
$■$ stopped if l $<0.1 \mathrm{lb}$.

## Two time constants may be set:

■ T1: heat rise time constant: concerns equipment that is running
■ T2: cooling time constant: concerns equipment that is stopped.

## Taking into account harmonics

The current measured by the thermal protection is an RMS 3-phase current which takes into account harmonics up to number 13.

## Taking into account ambient temperature

Most machines are designed to operate at a maximum ambient temperature of $40^{\circ} \mathrm{C}$ $\left(104^{\circ} \mathrm{F}\right)$. The thermal overload function takes into account the ambient temperature (Sepam equipped with the temperature sensor option ${ }^{(1)}$ ) to increase the calculated heat rise value when the temperature measured exceeds $40^{\circ} \mathrm{C}\left(104^{\circ} \mathrm{F}\right)$.
Increase factor: $\mathbf{f a}=\frac{\mathbf{T m a x}-\mathbf{4 0} 0^{\circ} \mathrm{C}}{\mathrm{Tmax}-\text { Tambiant }}$
where T max is the equipment maximum temperature (according to insulation class) T ambient is the measured temperature.
Table of insulation classes

| Class | $\mathbf{Y}$ | $\mathbf{A}$ | $\mathbf{E}$ | $\mathbf{B}$ | $\mathbf{F}$ | $\mathbf{H}$ | 200 | 220 | 250 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Tmax | $90^{\circ} \mathrm{C}$ | $105^{\circ} \mathrm{C}$ | $120^{\circ} \mathrm{C}$ | $130^{\circ} \mathrm{C}$ | $155^{\circ} \mathrm{C}$ | $180^{\circ} \mathrm{C}$ | $200^{\circ} \mathrm{C}$ | $220^{\circ} \mathrm{C}$ | $250{ }^{\circ} \mathrm{C}$ |
| Tmax | $194^{\circ} \mathrm{F}$ | $221^{\circ} \mathrm{F}$ | $248^{\circ} \mathrm{F}$ | $266^{\circ} \mathrm{F}$ | $311^{\circ} \mathrm{F}$ | $356^{\circ} \mathrm{F}$ | $392^{\circ} \mathrm{F}$ | $428^{\circ} \mathrm{F}$ | $482^{\circ} \mathrm{F}$ |
| Reference IEC $60085(1984)$ |  |  |  |  |  |  |  |  |  |

Reference IEC 60085 (1984).

## Adaptation of the protection to motor thermal withstand

Motor thermal protection is often set based on the hot and cold curves supplied by the machine manufacturer.
To fully comply with these experimental curves, additional parameters must be set:
■ initial heat rise, Es0, is used to reduce the cold tripping time.
modified cold curve: $\frac{\mathbf{t}}{\mathbf{T}}=\ln \frac{\left(\frac{\mathbf{l e q}}{\mathbf{l} \mathbf{b}}\right)^{2}-\mathbf{E s} \mathbf{0}}{\left(\frac{\mathbf{l e q}}{\mathbf{l}}\right)^{2}-\mathbf{E s}}$ where In: natural logarithm

- a second group of parameters (time constants and set points) is used to take into account thermal withstand with locked rotors. This second set of parameters is taken into account when the current is greater than an adjustable set point Is.


## Taking into account the negative sequence component

 In the case of motors with coiled rotors, the presence of a negative sequence component increases the heat rise in the motor. The negative sequence component of the current is taken into account in the protection function by the equation.$\mathbf{l e q}=\sqrt{\mathbf{l p h}^{2}+\mathbf{K} \times \mathbf{l i}^{2}}$ where | Iph is the largest phase current |
| :--- |
|  |
| li is the negative sequence component of the current |
| K is a adjustable coefficient |

K may have the following values: 0-2.25-4.5-9
For an asynchronous motor, K is determined as follows:
$\mathbf{K}=\mathbf{2} \times \frac{\mathbf{C d}}{\mathbf{C n}} \times \frac{\mathbf{1}}{\mathbf{g} \times\left(\frac{\mathrm{Id}}{\mathrm{Ib}}\right)^{2}}-1$ where $\begin{aligned} & \text { Cn, Cd: rated torque and starting torque } \\ & \begin{array}{l}\text { lb, Id: base current and starting current } \\ \mathrm{g}: \text { rated slip }\end{array}\end{aligned}$

## Learning of the cooling time constant T2

The time constant T2 may be learnt according to the temperatures measured in the equipment by temperature sensors connected to the MET148-2 module number 1.
T2 is estimated:

- after a heating/cooling sequence:
- heating period detected by ES > 70 \%
$\square$ followed by a shutdown detected by leq < $10 \%$ of lb
■ when the machine temperature is measured by RTDs connected to MET148-2
module number 1 :
$\square$ RTD 1, 2 or 3 assigned to motor/generator stator temperature measurement
- RTD 1, 3 or 5 assigned to transformer temperature measurement

After each new heating/cooling sequence is detected, a new T2 value is estimated. Following estimation, T2 can be used in two manners:

- automatically, in which case each new calculated value updates the T2 constant used
■ or manually by entering the value for the T2 parameter.
Measurement accuracy may be improved by using RTD 8 to measure the ambient temperature.
Because the function has two operating modes, a time constant is estimated for each mode.
For generator-transformer unit or motor-transformer unit applications, it is advised to connect the rotating machine RTDs to MET148-2 module number 1 to take advantage of T2 learning on the rotating machine rather than on the transformer.


## Start inhibit

The thermal overload protection can inhibit the closing of the motor control device until the heat rise drops back down below a value that allows restarting.
This value takes into account the heat rise produced by the motor when starting.
The inhibition function is grouped together with the starts per hour protection function and the indication START INHIBIT informs the user.

## Saving the heat rise information

The current heat rise is saved in the event of an auxiliary power failure.

## Inhibition of tripping

Tripping of the thermal overload protection may be inhibited by the logic input "Inhibit thermal overload" when required by the process.

## Use of two operating modes

The thermal overload protection function may be used to protect equipment with two operating modes, for example:

- transformers with two ventilation modes, with or without forced ventilation
(ONAN / ONAF)
■ two-speed motors.
The protection function comprises two groups of settings, and each group is suitable for equipment protection in one of the two operating modes.
Switching from one group of thermal settings to the other is done without losing the heat rise information. It is controlled:
■ either via a logic input, assigned to the "switching of thermal settings" function
■ or when the phase current reaches an adjustable Is set point (to be used for switching of thermal settings of a motor with locked rotor).
The base current of the equipment, used to calculate heat rise, also depends on the operating mode:
■ for logic input switching in mode 2, the base current lb-mode 2, a specific thermal overload protection setting, is used to calculate the heat rise in the equipment
■ in all other cases, the base current lb, defined as a general Sepam parameter, is used to calculate the heat rise in the equipment.


## User information

The following information is available for the user:

- heat rise
- learnt cooling time constant T2
- time before restart enabled (in case of inhibition of starting)
- time before tripping (with constant current).

See the section on measurement and machine operation assistance functions.

## Block diagram



## Characteristics

| Settings |  |
| :---: | :---: |
| Measurement origin |  |
| Setting range | I1, I2, I3 / I'1, I'2, I'3 |
| Taking into account the negative sequence component K |  |
| Setting range | 0-2.25-4.59-9 |
| Taking into account ambient temperature |  |
| Setting range | Yes / no |
| Using the learnt cooling time constant T2 |  |
| Setting range | Yes/no |
| Maximum equipment temperature Tmax (according to insulation class) |  |
| Setting range | $60^{\circ} \mathrm{C}$ to $200{ }^{\circ} \mathrm{C}$ or $140{ }^{\circ} \mathrm{F}$ to $392{ }^{\circ} \mathrm{F}$ |
| Resolution | $1^{\circ} \mathrm{C}$ or $1^{\circ} \mathrm{F}$ |


| Inputs |  | Syntax | Equations | Logipam |  |
| :--- | :--- | :--- | :--- | :--- | :--- |
| Designation | P49RMS_1_101 | ■ | ■ |  |  |
| Protection reset | P49RMS_1_113 | ■ | ■ |  |  |
| Protection inhibition |  |  |  |  |  |
| Outputs | Syntax | Equations | Logipam | Matrix |  |
| Designation | P49RMS_1_3 | ■ | ■ | ■ |  |
| Delayed output | P49RMS_1_10 | ■ | ■ | ■ |  |
| Alarm | P49RMS_1_11 | ■ | ■ | ■ |  |
| Inhibit closing | P49RMS_1_16 | ■ | ■ |  |  |
| Protection inhibited | P49RMS_1_18 | ■ | ■ |  |  |
| Hot state | P49RMS_1_32 | ■ | ■ |  |  |
| Inhibit thermal overload |  |  |  |  |  |

## Thermal mode 1 <br> Alarm set point Es1

| Setting range | 0 \% to 300 \% |
| :---: | :---: |
| Accuracy ${ }^{(1)}$ | $\pm 2$ \% |
| Resolution | 1 \% |
| Tripping set point Es2 |  |
| Setting range | 0 \% to $300 \%$ |
| Accuracy ${ }^{(1)}$ | $\pm 2$ \% |
| Resolution | 1 \% |
| Initial heat rise set point Es0 |  |
| Setting range | 0 \% to $100 \%$ |
| Accuracy ${ }^{(1)}$ | $\pm 2$ \% |
| Resolution | 1 \% |
| Heat rise time constant T1 |  |
| Setting range | 1 min . to 600 min . |
| Resolution | 1 min . |

Cooling time constant T2

| Setting range | 5 min . to 600 min . |
| :---: | :---: |
| Resolution | 1 min . |
| Thermal mode 2 |  |
| Using thermal mode 2 |  |
| Setting range | Yes/no |
| Alarm set point Es1 |  |
| Setting range | 0 \% to $300 \%$ |
| Accuracy ${ }^{(1)}$ | $\pm 2$ \% |
| Resolution | 1 \% |
| Tripping set point Es2 |  |
| Setting range | 0 \% to $300 \%$ |
| Accuracy ${ }^{(1)}$ | $\pm 2$ \% |
| Resolution | 1\% |
| Initial heat rise set point EsO |  |
| Setting range | 0 \% to $100 \%$ |
| Accuracy ${ }^{(1)}$ | $\pm 2$ \% |
| Resolution | 1\% |
| Heat rise time constant T1 |  |
| Setting range | 1 min . to 600 min . |
| Resolution | 1 min . |
| Cooling time constant T2 |  |
| Setting range | 5 min . to 600 min . |
| Resolution | 1 min . |
| Switching set point for thermal mode 2 |  |
| Setting range | 25 \% to $800 \%$ of lb |
| Accuracy ${ }^{(1)}$ | $\pm 5 \%$ |
| Resolution | 1 \% |
| Base current lb - mode 2 |  |
| Setting range | 0.2 to 2.6 In or l'n |
| Accuracy ${ }^{(1)}$ | $\pm 5 \%$ |
| Resolution | 1 A |
| Characteristic times ${ }^{(1)}$ |  |

Operation time accuracy $\pm 2 \%$ or $\pm 1 \mathrm{~s}$
(1) Under reference conditions (IEC 60255-8).

## Example 1: motor

The following data are available:

- time constants for on operation T1 and off operation T2:
ㅁ $\mathrm{T} 1=25 \mathrm{~min}$.
- T2 = 70 min .
- maximum steady state current:

Imax/lb=1.05.
Setting of tripping set point Es2
Es2 $=\left(\right.$ Imax/lb) ${ }^{2}=110 \%$
Note. If the motor draws a current of 1.05 lb continuously, the heat rise calculated by the thermal overload protection will reach $110 \%$.

## Setting of alarm set point Es1

Es1 $=90 \%(\mathrm{l} / \mathrm{lb}=0.95)$.
Knegative: 4.5 (usual value)
The other thermal overload parameters do not need to be set. They are not taken into account by default.

## Example 2: motor

The following data are available:

- motor thermal withstand in the form of hot and cold curves (see solid line curves in Figure 1)
- cooling time constant T2
- maximum steady state current:
$\mathrm{Imax} / \mathrm{Ib}=1.05$.
Setting of tripping set point Es2
Es2 $=(\text { Imax/lb })^{2}=110 \%$
Setting of alarm set point Es1:
Es1 $=90 \%(1 / / \mathrm{lb}=0.95)$.
The manufacturer's hot/cold curves ${ }^{(1)}$ may be used to determine the heating time constant T1.
The method consists of placing the Sepam hot/cold curves below those of the motor.

Figure 1. Motor thermal withstand and thermal overload tripping curves.


For an overload of 2 lb , the value $\mathrm{t} / \mathrm{T} 1=0.0339{ }^{(2)}$.
In order for Sepam to trip at point $1(t=70 \mathrm{~s})$, T 1 is equal to $2065 \mathrm{sec} \approx 34 \mathrm{~min}$. With a setting of $\mathrm{T} 1=34 \mathrm{~min}$., the tripping time is obtained based on a cold state (point 2). In this case, it is equal to $t / T 1=0.3216 \Rightarrow t=665 \mathrm{sec}$, i.e. $\approx 11 \mathrm{~min}$., which is compatible with the motor thermal withstand when it is cold.
The negative sequence factor K is calculated using the equation defined on page 154.
The parameters of the $2^{\text {nd }}$ thermal overload relay do not need to be set.
They are not taken into account by default.

## Example 3: motor

The following data are available:

- motor thermal withstand in the form of hot and cold curves (see solid line curves
in Figure 2)
- cooling time constant T2
- maximum steady state current: $\operatorname{Imax} / \mathrm{lb}=1.1$.

The thermal overload parameters are determined in the same way as in the previous example.
Setting of tripping set point Es2
Es2 $=(\text { Imax/lb })^{2}=120 \%$

## Setting of alarm set point Es1

Es1 $=90 \%(\mathrm{l} / \mathrm{lb}=0.95)$.
The time constant T1 is calculated so that the thermal overload protection trips after 100 seconds (point 1).
With $\mathrm{t} / \mathrm{T} 1=0.069(\mathrm{l} / \mathrm{lb}=2$ and Es2 $=120 \%)$ :
$\Rightarrow T 1=100 \mathrm{sec} / 0.069=1449 \mathrm{sec} \approx 24 \mathrm{~min}$.
The tripping time starting from the cold state is equal to:
$\mathrm{t} / \mathrm{T} 1=0.3567 \Rightarrow \mathrm{t}=24 \mathrm{~min} . \times 0.3567=513 \mathrm{sec}$ (point 2').
This tripping time is too long since the limit for this overload current is 400 sec (point 2).
If the time constant T1 is lowered, the thermal overload protection will trip earlier, below point 2.
The risk that motor starting when hot will not be possible also exists in this case (see Figure 2 in which a lower Sepam hot curve would intersect the starting curve with U = 0.9 Un).
The Es0 parameter is a setting that is used to solve these differences by lowering the Sepam cold curve without moving the hot curve.
In this example, the thermal overload protection should trip after 400 sec starting from the cold state.
The following equation is used to obtain the Es0 value:

where:
$\mathbf{t}_{\text {necessary }}$ : tripping time necessary starting from a cold state.
$I_{\text {processed }}$ : equipment current.
(1) When the machine manufacturer provides both a time constant T1 and the machine hot/cold curves, the use of the curves is recommended since they are more accurate.
(2) It is possible to use the charts containing the numerical values of the Sepam hot curve or the equation of the curve which is given on page 153.

# Thermal overload for machines ANSI code 49RMS Setting examples 

In numerical values, the following is obtained:
$E s 0=4-e^{\frac{400 \mathrm{~s}}{24 \times 60 \mathrm{~s}}} \times[4-(1.2)]=0.3035 \approx(31 \%)$
By setting EsO = $31 \%$, point $2^{\prime}$ is moved downward to obtain a shorter tripping time that is compatible with the motor thermal withstand when cold (see Figure 3). Note. A setting Es0 $=100 \%$ therefore means that the hot and cold curves are the same.

Figure 2. Hot/cold curves not compatible with the motor thermal withstand.


Figure 3. Hot/cold curves compatible with the motor thermal withstand via the setting of an initial heat rise Es0.


## Use of the additional setting group

When a motor rotor is locked or is turning very slowly, its thermal behavior is different from that with the rated load.
In such conditions, the motor is damaged by overheating of the rotor or stator. For high power motors, rotor overheating is most often a limiting factor.
The thermal overload parameters chosen for operation with a low overload are no longer valid.
In order to protect the motor in this case, "excessive starting time" protection may be used.
Nevertheless, motor manufacturers provide the thermal withstand curves when the rotor is locked, for different voltages at the time of starting.

Figure 4. Locked rotor thermal withstand.

(1) thermal withstand, motor running
(2) thermal withstand, motor stopped
(3) Sepam tripping curve
(4) starting at $65 \%$ Un
(5) starting at $80 \%$ Un
(6) starting at $100 \%$ Un

In order to take these curves into account, the $2^{\text {nd }}$ thermal overload relay may be used.
The time constant in this case is, in theory, shorter, however, it should be determined in the same way as that of the $1^{\text {st }}$ relay.
The thermal overload protection switches between the first and second relay if the equivalent current leq exceeds the Is value (set point current).

## Example 4. transformer with 2 ventilation modes

The following data are available:
The rated current of a transformer with 2 ventilation modes is:
■ lb = 200 A without forced ventilation (ONAN mode), the main operating mode of the transformer
■ lb = 240 A with forced ventilation (ONAF mode), a temporary operating mode, to have $20 \%$ more power available

Setting of the base current for ventilation operating mode 1: lb=200 A
(to be set in the Sepam general parameters).
Setting of the base current for ventilation operating mode 2: Ib2 = 240 A
(to be set among the specific thermal overload protection settings).
Switching of thermal settings via logic input, to be assigned to the "switching of thermal settings" function and to be connected to the transformer ventilation control unit.
The settings related to each ventilation operating mode (Es set points, time constants, etc.) are to be determined according to the transformer characteristics provided by the manufacturer.

| I/lb Es (\%) | 1.00 | 1.05 | 1.10 | 1.15 | 1.20 | 1.25 | 1.30 | 1.35 | 1.40 | 1.45 | 1.50 | 1.55 | 1.60 | 1.65 | 1.70 | 1.75 | 1.80 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 50 | 0.6931 | 0.6042 | 0.5331 | 0.4749 | 0.4265 | 0.3857 | 0.3508 | 0.3207 | 0.2945 | 0.2716 | 0.2513 | 0.2333 | 0.2173 | 0.2029 | 0.1900 | 0.1782 | 0.1676 |
| 55 | 0.7985 | 0.6909 | 0.6061 | 0.5376 | 0.4812 | 0.4339 | 0.3937 | 0.3592 | 0.3294 | 0.3033 | 0.2803 | 0.2600 | 0.2419 | 0.2257 | 0.2111 | 0.1980 | 0.1860 |
| 60 | 0.9163 | 0.7857 | 0.6849 | 0.6046 | 0.5390 | 0.4845 | 0.4386 | 0.3993 | 0.3655 | 0.3360 | 0.3102 | 0.2873 | 0.2671 | 0.2490 | 0.2327 | 0.2181 | 0.2048 |
| 65 | 1.0498 | 0.8905 | 0.7704 | 0.6763 | 0.6004 | 0.5379 | 0.4855 | 0.4411 | 0.4029 | 0.3698 | 0.3409 | 0.3155 | 0.2929 | 0.2728 | 0.2548 | 0.2386 | 0.2239 |
| 70 | 1.2040 | 1.0076 | 0.8640 | 0.7535 | 0.6657 | 0.5942 | 0.5348 | 0.4847 | 0.4418 | 0.4049 | 0.3727 | 0.3444 | 0.3194 | 0.2972 | 0.2774 | 0.2595 | 0.2434 |
| 75 | 1.3863 | 1.1403 | 0.9671 | 0.8373 | 0.7357 | 0.6539 | 0.5866 | 0.5302 | 0.4823 | 0.4412 | 0.4055 | 0.3742 | 0.3467 | 0.3222 | 0.3005 | 0.2809 | 0.2633 |
| 80 | 1.6094 | 1.2933 | 1.0822 | 0.9287 | 0.8109 | 0.7174 | 0.6413 | 0.5780 | 0.5245 | 0.4788 | 0.4394 | 0.4049 | 0.3747 | 0.3479 | 0.3241 | 0.3028 | 0.2836 |
| 85 | 1.8971 | 1.4739 | 1.2123 | 1.0292 | 0.8923 | 0.7853 | 0.6991 | 0.6281 | 0.5686 | 0.5180 | 0.4745 | 0.4366 | 0.4035 | 0.3743 | 0.3483 | 0.3251 | 0.3043 |
| 90 | 2.3026 | 1.6946 | 1.3618 | 1.1411 | 0.9808 | 0.8580 | 0.7605 | 0.6809 | 0.6147 | 0.5587 | 0.5108 | 0.4694 | 0.4332 | 0.4013 | 0.3731 | 0.3480 | 0.3254 |
| 95 |  | 1.9782 | 1.5377 | 1.2670 | 1.0780 | 0.9365 | 0.8258 | 0.7366 | 0.6630 | 0.6012 | 0.5486 | 0.5032 | 0.4638 | 0.4292 | 0.3986 | 0.3714 | 0.3470 |
| 100 |  | 2.3755 | 1.7513 | 1.4112 | 1.1856 | 1.0217 | 0.8958 | 0.7956 | 0.7138 | 0.6455 | 0.5878 | 0.5383 | 0.4953 | 0.4578 | 0.4247 | 0.3953 | 0.3691 |
| 105 |  | 3.0445 | 2.0232 | 1.5796 | 1.3063 | 1.1147 | 0.9710 | 0.8583 | 0.7673 | 0.6920 | 0.6286 | 0.5746 | 0.5279 | 0.4872 | 0.4515 | 0.4199 | 0.3917 |
| 110 |  |  | 2.3979 | 1.7824 | 1.4435 | 1.2174 | 1.0524 | 0.9252 | 0.8238 | 0.7406 | 0.6712 | 0.6122 | 0.5616 | 0.5176 | 0.4790 | 0.4450 | 0.4148 |
| 115 |  |  | 3.0040 | 2.0369 | 1.6025 | 1.3318 | 1.1409 | 0.9970 | 0.8837 | 0.7918 | 0.7156 | 0.6514 | 0.5964 | 0.5489 | 0.5074 | 0.4708 | 0.4384 |
| 120 |  |  |  | 2.3792 | 1.7918 | 1.4610 | 1.2381 | 1.0742 | 0.9474 | 0.8457 | 0.7621 | 0.6921 | 0.6325 | 0.5812 | 0.5365 | 0.4973 | 0.4626 |
| 125 |  |  |  | 2.9037 | 2.0254 | 1.6094 | 1.3457 | 1.1580 | 1.0154 | 0.9027 | 0.8109 | 0.7346 | 0.6700 | 0.6146 | 0.5666 | 0.5245 | 0.4874 |
| 130 |  |  |  |  | 2.3308 | 1.7838 | 1.4663 | 1.2493 | 1.0885 | 0.9632 | 0.8622 | 0.7789 | 0.7089 | 0.6491 | 0.5975 | 0.5525 | 0.5129 |
| 135 |  |  |  |  | 2.7726 | 1.9951 | 1.6035 | 1.3499 | 1.1672 | 1.0275 | 0.9163 | 0.8253 | 0.7494 | 0.6849 | 0.6295 | 0.5813 | 0.5390 |
| 140 |  |  |  |  |  | 2.2634 | 1.7626 | 1.4618 | 1.2528 | 1.0962 | 0.9734 | 0.8740 | 0.7916 | 0.7220 | 0.6625 | 0.6109 | 0.5658 |
| 145 |  |  |  |  |  | 2.6311 | 1.9518 | 1.5877 | 1.3463 | 1.1701 | 1.0341 | 0.9252 | 0.8356 | 0.7606 | 0.6966 | 0.6414 | 0.5934 |
| 150 |  |  |  |  |  | 3.2189 | 2.1855 | 1.7319 | 1.4495 | 1.2498 | 1.0986 | 0.9791 | 0.8817 | 0.8007 | 0.7320 | 0.6729 | 0.6217 |
| 155 |  |  |  |  |  |  | 2.4908 | 1.9003 | 1.5645 | 1.3364 | 1.1676 | 1.0361 | 0.9301 | 0.8424 | 0.7686 | 0.7055 | 0.6508 |
| 160 |  |  |  |  |  |  | 2.9327 | 2.1030 | 1.6946 | 1.4313 | 1.2417 | 1.0965 | 0.9808 | 0.8860 | 0.8066 | 0.7391 | 0.6809 |
| 165 |  |  |  |  |  |  |  | 2.3576 | 1.8441 | 1.5361 | 1.3218 | 1.1609 | 1.0343 | 0.9316 | 0.8461 | 0.7739 | 0.7118 |
| 170 |  |  |  |  |  |  |  | 2.6999 | 2.0200 | 1.6532 | 1.4088 | 1.2296 | 1.0908 | 0.9793 | 0.8873 | 0.8099 | 0.7438 |
| 175 |  |  |  |  |  |  |  | 3.2244 | 2.2336 | 1.7858 | 1.5041 | 1.3035 | 1.1507 | 1.0294 | 0.9302 | 0.8473 | 0.7768 |
| 180 |  |  |  |  |  |  |  |  | 2.5055 | 1.9388 | 1.6094 | 1.3832 | 1.2144 | 1.0822 | 0.9751 | 0.8861 | 0.8109 |
| 185 |  |  |  |  |  |  |  |  | 2.8802 | 2.1195 | 1.7272 | 1.4698 | 1.2825 | 1.1379 | 1.0220 | 0.9265 | 0.8463 |
| 190 |  |  |  |  |  |  |  |  | 3.4864 | 2.3401 | 1.8608 | 1.5647 | 1.3555 | 1.1970 | 1.0713 | 0.9687 | 0.8829 |
| 195 |  |  |  |  |  |  |  |  |  | 2.6237 | 2.0149 | 1.6695 | 1.4343 | 1.2597 | 1.1231 | 1.0126 | 0.9209 |
| 200 |  |  |  |  |  |  |  |  |  | 3.0210 | 2.1972 | 1.7866 | 1.5198 | 1.3266 | 1.1778 | 1.0586 | 0.9605 |


|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| I/lb Es (\%) | 1.85 | 1.90 | 1.95 | 2.00 | 2.20 | 2.40 | 2.60 | 2.80 | 3.00 | 3.20 | 3.40 | 3.60 | 3.80 | 4.00 | 4.20 | 4.40 | 4.60 |
| 50 | 0.1579 | 0.1491 | 0.1410 | 0.1335 | 0.1090 | 0.0908 | 0.0768 | 0.0659 | 0.0572 | 0.0501 | 0.0442 | 0.0393 | 0.0352 | 0.0317 | 0.0288 | 0.0262 | 0.0239 |
| 55 | 0.1752 | 0.1653 | 0.1562 | 0.1479 | 0.1206 | 0.1004 | 0.0849 | 0.0727 | 0.0631 | 0.0552 | 0.0487 | 0.0434 | 0.0388 | 0.0350 | 0.0317 | 0.0288 | 0.0263 |
| 60 | 0.1927 | 0.1818 | 0.1717 | 0.1625 | 0.1324 | 0.1100 | 0.0929 | 0.0796 | 0.069 | 0.0604 | 0.0533 | 0.0474 | 0.0424 | 0.0382 | 0.0346 | 0.0315 | 0.0288 |
| 65 | 0.2106 | 0.1985 | 0.1875 | 0.1773 | 0.1442 | 0.1197 | 0.1011 | 0.0865 | 0.075 | 0.0656 | 0.0579 | 0.0515 | 0.0461 | 0.0415 | 0.0375 | 0.0342 | 0.0312 |
| 70 | 0.2288 | 0.2156 | 0.2035 | 0.1924 | 0.1562 | 0.1296 | 0.1093 | 0.0935 | 0.081 | 0.0708 | 0.0625 | 0.0555 | 0.0497 | 0.0447 | 0.0405 | 0.0368 | 0.0336 |
| 75 | 0.2474 | 0.2329 | 0.2197 | 0.2076 | 0.1684 | 0.1395 | 0.1176 | 0.1006 | 0.087 | 0.0761 | 0.0671 | 0.0596 | 0.0533 | 0.0480 | 0.0434 | 0.0395 | 0.0361 |
| 80 | 0.2662 | 0.2505 | 0.2362 | 0.2231 | 0.1807 | 0.1495 | 0.1260 | 0.1076 | 0.0931 | 0.0813 | 0.0717 | 0.0637 | 0.0570 | 0.0513 | 0.0464 | 0.0422 | 0.0385 |
| 85 | 0.2855 | 0.2685 | 0.2530 | 0.2389 | 0.1931 | 0.1597 | 0.1344 | 0.1148 | 0.0992 | 0.0867 | 0.0764 | 0.0678 | 0.0607 | 0.0546 | 0.0494 | 0.0449 | 0.0410 |
| 90 | 0.3051 | 0.2868 | 0.2701 | 0.2549 | 0.2057 | 0.1699 | 0.1429 | 0.1219 | 0.1054 | 0.092 | 0.0811 | 0.0720 | 0.0644 | 0.0579 | 0.0524 | 0.0476 | 0.0435 |
| 95 | 0.3251 | 0.3054 | 0.2875 | 0.2712 | 0.2185 | 0.1802 | 0.1514 | 0.1292 | 0.1116 | 0.0974 | 0.0858 | 0.0761 | 0.0681 | 0.0612 | 0.0554 | 0.0503 | 0.0459 |
| 100 | 0.3456 | 0.3244 | 0.3051 | 0.2877 | 0.2314 | 0.1907 | 0.1601 | 0.1365 | 0.1178 | 0.1028 | 0.0905 | 0.0803 | 0.0718 | 0.0645 | 0.0584 | 0.0530 | 0.0484 |
| 105 | 0.3664 | 0.3437 | 0.3231 | 0.3045 | 0.2445 | 0.2012 | 0.1688 | 0.1438 | 0.1241 | 0.1082 | 0.0952 | 0.0845 | 0.0755 | 0.0679 | 0.0614 | 0.0558 | 0.0509 |
| 110 | 0.3877 | 0.3634 | 0.3415 | 0.3216 | 0.2578 | 0.2119 | 0.1776 | 0.1512 | 0.1304 | 0.1136 | 0.1000 | 0.0887 | 0.0792 | 0.0712 | 0.0644 | 0.0585 | 0.0534 |
| 115 | 0.4095 | 0.3835 | 0.3602 | 0.3390 | 0.2713 | 0.2227 | 0.1865 | 0.1586 | 0.1367 | 0.1191 | 0.1048 | 0.0929 | 0.0830 | 0.0746 | 0.0674 | 0.0612 | 0.0559 |
| 120 | 0.4317 | 0.4041 | 0.3792 | 0.3567 | 0.2849 | 0.2336 | 0.1954 | 0.1661 | 0.1431 | 0.1246 | 0.1096 | 0.0972 | 0.0868 | 0.0780 | 0.0705 | 0.0640 | 0.0584 |
| 125 | 0.4545 | 0.4250 | 0.3986 | 0.3747 | 0.2988 | 0.2446 | 0.2045 | 0.1737 | 0.1495 | 0.1302 | 0.1144 | 0.1014 | 0.0905 | 0.0813 | 0.0735 | 0.0667 | 0.0609 |
| 130 | 0.4778 | 0.4465 | 0.4184 | 0.3930 | 0.3128 | 0.2558 | 0.2136 | 0.1813 | 0.156 | 0.1358 | 0.1193 | 0.1057 | 0.0943 | 0.0847 | 0.0766 | 0.0695 | 0.0634 |
| 135 | 0.5016 | 0.4683 | 0.4386 | 0.4117 | 0.3270 | 0.2671 | 0.2228 | 0.1890 | 0.1625 | 0.1414 | 0.1242 | 0.1100 | 0.0982 | 0.0881 | 0.0796 | 0.0723 | 0.0659 |
| 140 | 0.5260 | 0.4907 | 0.4591 | 0.4308 | 0.3414 | 0.2785 | 0.2321 | 0.1967 | 0.1691 | 0.147 | 0.1291 | 0.1143 | 0.1020 | 0.0916 | 0.0827 | 0.0751 | 0.0685 |
| 145 | 0.5511 | 0.5136 | 0.4802 | 0.4502 | 0.3561 | 0.2900 | 0.2414 | 0.2045 | 0.1757 | 0.1527 | 0.1340 | 0.1187 | 0.1058 | 0.0950 | 0.0858 | 0.0778 | 0.0710 |
| 150 | 0.5767 | 0.5370 | 0.5017 | 0.4700 | 0.3709 | 0.3017 | 0.2509 | 0.2124 | 0.1823 | 0.1584 | 0.1390 | 0.1230 | 0.1097 | 0.0984 | 0.0889 | 0.0806 | 0.0735 |
| 155 | 0.6031 | 0.5610 | 0.5236 | 0.4902 | 0.3860 | 0.3135 | 0.2604 | 0.2203 | 0.189 | 0.1641 | 0.1440 | 0.1274 | 0.1136 | 0.1019 | 0.0920 | 0.0834 | 0.0761 |
| 160 | 0.6302 | 0.5856 | 0.5461 | 0.5108 | 0.4013 | 0.3254 | 0.2701 | 0.2283 | 0.1957 | 0.1699 | 0.1490 | 0.1318 | 0.1174 | 0.1054 | 0.0951 | 0.0863 | 0.0786 |
| 165 | 0.6580 | 0.6108 | 0.5690 | 0.5319 | 0.4169 | 0.3375 | 0.2798 | 0.2363 | 0.2025 | 0.1757 | 0.1540 | 0.1362 | 0.1213 | 0.1088 | 0.0982 | 0.0891 | 0.0812 |
| 170 | 0.6866 | 0.6366 | 0.5925 | 0.5534 | 0.4327 | 0.3498 | 0.2897 | 0.2444 | 0.2094 | 0.1815 | 0.1591 | 0.1406 | 0.1253 | 0.1123 | 0.1013 | 0.0919 | 0.0838 |
| 175 | 0.7161 | 0.6631 | 0.6166 | 0.5754 | 0.4487 | 0.3621 | 0.2996 | 0.2526 | 0.2162 | 0.1874 | 0.1641 | 0.1451 | 0.1292 | 0.1158 | 0.1045 | 0.0947 | 0.0863 |
| 180 | 0.7464 | 0.6904 | 0.6413 | 0.5978 | 0.4651 | 0.3747 | 0.3096 | 0.2608 | 0.2231 | 0.1933 | 0.1693 | 0.1495 | 0.1331 | 0.1193 | 0.1076 | 0.0976 | 0.0889 |
| 185 | 0.7777 | 0.7184 | 0.6665 | 0.6208 | 0.4816 | 0.3874 | 0.3197 | 0.2691 | 0.2301 | 0.1993 | 0.1744 | 0.1540 | 0.1371 | 0.1229 | 0.1108 | 0.1004 | 0.0915 |
| 190 | 0.8100 | 0.7472 | 0.6925 | 0.6444 | 0.4985 | 0.4003 | 0.3300 | 0.2775 | 0.2371 | 0.2052 | 0.1796 | 0.1585 | 0.1411 | 0.1264 | 0.1140 | 0.1033 | 0.0941 |
| 195 | 0.8434 | 0.7769 | 0.7191 | 0.6685 | 0.5157 | 0.4133 | 0.3403 | 0.2860 | 0.2442 | 0.2113 | 0.1847 | 0.1631 | 0.1451 | 0.1300 | 0.1171 | 0.1062 | 0.0967 |
| 200 | 0.8780 | 0.8075 | 0.7465 | 0.6931 | 0.5331 | 0.4265 | 0.3508 | 0.2945 | 0.2513 | 0.2173 | 0.1900 | 0.1676 | 0.1491 | 0.1335 | 0.1203 | 0.1090 | 0.0993 |


| l/lb Es (\%) | 4.80 | 5.00 | 5.50 | 6.00 | 6.50 | 7.00 | 7.50 | 8.00 | 8.50 | 9.00 | 9.50 | 10.00 | 12.50 | 15.00 | 17.50 | 20.00 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 50 | 0.0219 | 0.0202 | 0.0167 | 0.0140 | 0.0119 | 0.0103 | 0.0089 | 0.0078 | 0.0069 | 0.0062 | 0.0056 | 0.0050 | 0.0032 | 0.0022 | 0.0016 | 0.0013 |
| 55 | 0.0242 | 0.0222 | 0.0183 | 0.0154 | 0.0131 | 0.0113 | 0.0098 | 0.0086 | 0.0076 | 0.0068 | 0.0061 | 0.0055 | 0.0035 | 0.0024 | 0.0018 | 0.0014 |
| 60 | 0.0264 | 0.0243 | 0.0200 | 0.0168 | 0.0143 | 0.0123 | 0.0107 | 0.0094 | 0.0083 | 0.0074 | 0.0067 | 0.0060 | 0.0038 | 0.0027 | 0.0020 | 0.0015 |
| 65 | 0.0286 | 0.0263 | 0.0217 | 0.0182 | 0.0155 | 0.0134 | 0.0116 | 0.0102 | 0.0090 | 0.0081 | 0.0072 | 0.0065 | 0.0042 | 0.0029 | 0.0021 | 0.0016 |
| 70 | 0.0309 | 0.0284 | 0.0234 | 0.0196 | 0.0167 | 0.0144 | 0.0125 | 0.0110 | 0.0097 | 0.0087 | 0.0078 | 0.0070 | 0.0045 | 0.0031 | 0.0023 | 0.0018 |
| 75 | 0.0331 | 0.0305 | 0.0251 | 0.0211 | 0.0179 | 0.0154 | 0.0134 | 0.0118 | 0.0104 | 0.0093 | 0.0083 | 0.0075 | 0.0048 | 0.0033 | 0.0025 | 0.0019 |
| 80 | 0.0353 | 0.0325 | 0.0268 | 0.0225 | 0.0191 | 0.0165 | 0.0143 | 0.0126 | 0.0111 | 0.0099 | 0.0089 | 0.0080 | 0.0051 | 0.0036 | 0.0026 | 0.0020 |
| 85 | 0.0376 | 0.0346 | 0.0285 | 0.0239 | 0.0203 | 0.0175 | 0.0152 | 0.0134 | 0.0118 | 0.0105 | 0.0095 | 0.0085 | 0.0055 | 0.0038 | 0.0028 | 0.0021 |
| 90 | 0.0398 | 0.0367 | 0.0302 | 0.0253 | 0.0215 | 0.0185 | 0.0161 | 0.0142 | 0.0125 | 0.0112 | 0.0100 | 0.0090 | 0.0058 | 0.0040 | 0.0029 | 0.0023 |
| 95 | 0.0421 | 0.0387 | 0.0319 | 0.0267 | 0.0227 | 0.0196 | 0.0170 | 0.0150 | 0.0132 | 0.0118 | 0.0106 | 0.0095 | 0.0061 | 0.0042 | 0.0031 | 0.0024 |
| 100 | 0.0444 | 0.0408 | 0.0336 | 0.0282 | 0.0240 | 0.0206 | 0.0179 | 0.0157 | 0.0139 | 0.0124 | 0.0111 | 0.0101 | 0.0064 | 0.0045 | 0.0033 | 0.0025 |
| 105 | 0.0466 | 0.0429 | 0.0353 | 0.0296 | 0.0252 | 0.0217 | 0.0188 | 0.0165 | 0.0146 | 0.0130 | 0.0117 | 0.0106 | 0.0067 | 0.0047 | 0.0034 | 0.0026 |
| 110 | 0.0489 | 0.0450 | 0.0370 | 0.0310 | 0.0264 | 0.0227 | 0.0197 | 0.0173 | 0.0153 | 0.0137 | 0.0123 | 0.0111 | 0.0071 | 0.0049 | 0.0036 | 0.0028 |
| 115 | 0.0512 | 0.0471 | 0.0388 | 0.0325 | 0.0276 | 0.0237 | 0.0207 | 0.0181 | 0.0160 | 0.0143 | 0.0128 | 0.0116 | 0.0074 | 0.0051 | 0.0038 | 0.0029 |
| 120 | 0.0535 | 0.0492 | 0.0405 | 0.0339 | 0.0288 | 0.0248 | 0.0216 | 0.0189 | 0.0167 | 0.0149 | 0.0134 | 0.0121 | 0.0077 | 0.0053 | 0.0039 | 0.0030 |
| 125 | 0.0558 | 0.0513 | 0.0422 | 0.0353 | 0.0300 | 0.0258 | 0.0225 | 0.0197 | 0.0175 | 0.0156 | 0.0139 | 0.0126 | 0.0080 | 0.0056 | 0.0041 | 0.0031 |
| 130 | 0.0581 | 0.0534 | 0.0439 | 0.0368 | 0.0313 | 0.0269 | 0.0234 | 0.0205 | 0.0182 | 0.0162 | 0.0145 | 0.0131 | 0.0084 | 0.0058 | 0.0043 | 0.0033 |
| 135 | 0.0604 | 0.0555 | 0.0457 | 0.0382 | 0.0325 | 0.0279 | 0.0243 | 0.0213 | 0.0189 | 0.0168 | 0.0151 | 0.0136 | 0.0087 | 0.0060 | 0.0044 | 0.0034 |
| 140 | 0.0627 | 0.0576 | 0.0474 | 0.0397 | 0.0337 | 0.0290 | 0.0252 | 0.0221 | 0.0196 | 0.0174 | 0.0156 | 0.0141 | 0.0090 | 0.0062 | 0.0046 | 0.0035 |
| 145 | 0.0650 | 0.0598 | 0.0491 | 0.0411 | 0.0349 | 0.0300 | 0.0261 | 0.0229 | 0.0203 | 0.0181 | 0.0162 | 0.0146 | 0.0093 | 0.0065 | 0.0047 | 0.0036 |
| 150 | 0.0673 | 0.0619 | 0.0509 | 0.0426 | 0.0361 | 0.0311 | 0.0270 | 0.0237 | 0.0210 | 0.0187 | 0.0168 | 0.0151 | 0.0096 | 0.0067 | 0.0049 | 0.0038 |
| 155 | 0.0696 | 0.0640 | 0.0526 | 0.0440 | 0.0374 | 0.0321 | 0.0279 | 0.0245 | 0.0217 | 0.0193 | 0.0173 | 0.0156 | 0.0100 | 0.0069 | 0.0051 | 0.0039 |
| 160 | 0.0720 | 0.0661 | 0.0543 | 0.0455 | 0.0386 | 0.0332 | 0.0289 | 0.0253 | 0.0224 | 0.0200 | 0.0179 | 0.0161 | 0.0103 | 0.0071 | 0.0052 | 0.0040 |
| 165 | 0.0743 | 0.0683 | 0.0561 | 0.0469 | 0.0398 | 0.0343 | 0.0298 | 0.0261 | 0.0231 | 0.0206 | 0.0185 | 0.0166 | 0.0106 | 0.0074 | 0.0054 | 0.0041 |
| 170 | 0.0766 | 0.0704 | 0.0578 | 0.0484 | 0.0411 | 0.0353 | 0.0307 | 0.0269 | 0.0238 | 0.0212 | 0.0190 | 0.0171 | 0.0109 | 0.0076 | 0.0056 | 0.0043 |
| 175 | 0.0790 | 0.0726 | 0.0596 | 0.0498 | 0.0423 | 0.0364 | 0.0316 | 0.0277 | 0.0245 | 0.0218 | 0.0196 | 0.0177 | 0.0113 | 0.0078 | 0.0057 | 0.0044 |
| 180 | 0.0813 | 0.0747 | 0.0613 | 0.0513 | 0.0435 | 0.0374 | 0.0325 | 0.0285 | 0.0252 | 0.0225 | 0.0201 | 0.0182 | 0.0116 | 0.0080 | 0.0059 | 0.0045 |
| 185 | 0.0837 | 0.0769 | 0.0631 | 0.0528 | 0.0448 | 0.0385 | 0.0334 | 0.0293 | 0.0259 | 0.0231 | 0.0207 | 0.0187 | 0.0119 | 0.0083 | 0.0061 | 0.0046 |
| 190 | 0.0861 | 0.0790 | 0.0649 | 0.0542 | 0.0460 | 0.0395 | 0.0344 | 0.0301 | 0.0266 | 0.0237 | 0.0213 | 0.0192 | 0.0122 | 0.0085 | 0.0062 | 0.0048 |
| 195 | 0.0884 | 0.0812 | 0.0666 | 0.0557 | 0.0473 | 0.0406 | 0.0353 | 0.0309 | 0.0274 | 0.0244 | 0.0218 | 0.0197 | 0.0126 | 0.0087 | 0.0064 | 0.0049 |
| 200 | 0.0908 | 0.0834 | 0.0684 | 0.0572 | 0.0485 | 0.0417 | 0.0362 | 0.0317 | 0.0281 | 0.0250 | 0.0224 | 0.0202 | 0.0129 | 0.0089 | 0.0066 | 0.0050 |


| Hot c | S |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { l/lb } \\ & \text { Es (\%) } \end{aligned}$ | 1.00 | 1.05 | 1.10 | 1.15 | 1.20 | 1.25 | 1.30 | 1.35 | 1.40 | 1.45 | 1.50 | 1.55 | 1.60 | 1.65 | 1.70 | 1.75 | 1.80 |
| 105 |  | 0.6690 | 0.2719 | 0.1685 | 0.1206 | 0.0931 | 0.0752 | 0.0627 | 0.0535 | 0.0464 | 0.0408 | 0.0363 | 0.0326 | 0.0295 | 0.0268 | 0.0245 | 0.0226 |
| 110 |  | 3.7136 | 0.6466 | 0.3712 | 0.2578 | 0.1957 | 0.1566 | 0.1296 | 0.1100 | 0.0951 | 0.0834 | 0.0740 | 0.0662 | 0.0598 | 0.0544 | 0.0497 | 0.0457 |
| 115 |  |  | 1.2528 | 0.6257 | 0.4169 | 0.3102 | 0.2451 | 0.2013 | 0.1699 | 0.1462 | 0.1278 | 0.1131 | 0.1011 | 0.0911 | 0.0827 | 0.0755 | 0.0693 |
| 120 |  |  | 3.0445 | 0.9680 | 0.6061 | 0.4394 | 0.3423 | 0.2786 | 0.2336 | 0.2002 | 0.1744 | 0.1539 | 0.1372 | 0.1234 | 0.1118 | 0.1020 | 0.0935 |
| 125 |  |  |  | 1.4925 | 0.8398 | 0.5878 | 0.4499 | 0.3623 | 0.3017 | 0.2572 | 0.2231 | 0.1963 | 0.1747 | 0.1568 | 0.1419 | 0.1292 | 0.1183 |
| 130 |  |  |  | 2.6626 | 1.1451 | 0.7621 | 0.5705 | 0.4537 | 0.3747 | 0.3176 | 0.2744 | 0.2407 | 0.2136 | 0.1914 | 0.1728 | 0.1572 | 0.1438 |
| 135 |  |  |  |  | 1.5870 | 0.9734 | 0.7077 | 0.5543 | 0.4535 | 0.3819 | 0.3285 | 0.2871 | 0.2541 | 0.2271 | 0.2048 | 0.1860 | 0.1699 |
| 140 |  |  |  |  | 2.3979 | 1.2417 | 0.8668 | 0.6662 | 0.5390 | 0.4507 | 0.3857 | 0.3358 | 0.2963 | 0.2643 | 0.2378 | 0.2156 | 0.1967 |
| 145 |  |  |  |  |  | 1.6094 | 1.0561 | 0.7921 | 0.6325 | 0.5245 | 0.4463 | 0.3869 | 0.3403 | 0.3028 | 0.2719 | 0.2461 | 0.2243 |
| 150 |  |  |  |  |  | 2.1972 | 1.2897 | 0.9362 | 0.7357 | 0.6042 | 0.5108 | 0.4408 | 0.3864 | 0.3429 | 0.3073 | 0.2776 | 0.2526 |
| 155 |  |  |  |  |  | 3.8067 | 1.5950 | 1.1047 | 0.8508 | 0.6909 | 0.5798 | 0.4978 | 0.4347 | 0.3846 | 0.3439 | 0.3102 | 0.2817 |
| 160 |  |  |  |  |  |  | 2.0369 | 1.3074 | 0.9808 | 0.7857 | 0.6539 | 0.5583 | 0.4855 | 0.4282 | 0.3819 | 0.3438 | 0.3118 |
| 165 |  |  |  |  |  |  | 2.8478 | 1.5620 | 1.1304 | 0.8905 | 0.7340 | 0.6226 | 0.5390 | 0.4738 | 0.4215 | 0.3786 | 0.3427 |
| 170 |  |  |  |  |  |  |  | 1.9042 | 1.3063 | 1.0076 | 0.8210 | 0.6914 | 0.5955 | 0.5215 | 0.4626 | 0.4146 | 0.3747 |
| 175 |  |  |  |  |  |  |  | 2.4288 | 1.5198 | 1.1403 | 0.9163 | 0.7652 | 0.6554 | 0.5717 | 0.5055 | 0.4520 | 0.4077 |
| 180 |  |  |  |  |  |  |  | 3.5988 | 1.7918 | 1.2933 | 1.0217 | 0.8449 | 0.7191 | 0.6244 | 0.5504 | 0.4908 | 0.4418 |
| 185 |  |  |  |  |  |  |  |  | 2.1665 | 1.4739 | 1.1394 | 0.9316 | 0.7872 | 0.6802 | 0.5974 | 0.5312 | 0.4772 |
| 190 |  |  |  |  |  |  |  |  | 2.7726 | 1.6946 | 1.2730 | 1.0264 | 0.8602 | 0.7392 | 0.6466 | 0.5733 | 0.5138 |
| 195 |  |  |  |  |  |  |  |  | 4.5643 | 1.9782 | 1.4271 | 1.1312 | 0.9390 | 0.8019 | 0.6985 | 0.6173 | 0.5518 |
| 200 |  |  |  |  |  |  |  |  |  | 2.3755 | 1.6094 | 1.2483 | 1.0245 | 0.8688 | 0.7531 | 0.6633 | 0.5914 |
| I/lb Es (\%) | 1.85 | 1.90 | 1.95 | 2.00 | 2.20 | 2.40 | 2.60 | 2.80 | 3.00 | 3.20 | 3.40 | 3.60 | 3.80 | 4.00 | 4.20 | 4.40 | 4.60 |
| 105 | 0.0209 | 0.0193 | 0.0180 | 0.0168 | 0.0131 | 0.0106 | 0.0087 | 0.0073 | 0.0063 | 0.0054 | 0.0047 | 0.0042 | 0.0037 | 0.0033 | 0.0030 | 0.0027 | 0.0025 |
| 110 | 0.0422 | 0.0391 | 0.0363 | 0.0339 | 0.0264 | 0.0212 | 0.0175 | 0.0147 | 0.0126 | 0.0109 | 0.0095 | 0.0084 | 0.0075 | 0.0067 | 0.0060 | 0.0055 | 0.0050 |
| 115 | 0.0639 | 0.0592 | 0.0550 | 0.0513 | 0.0398 | 0.0320 | 0.0264 | 0.0222 | 0.0189 | 0.0164 | 0.0143 | 0.0126 | 0.0112 | 0.0101 | 0.0091 | 0.0082 | 0.0075 |
| 120 | 0.0862 | 0.0797 | 0.0740 | 0.0690 | 0.0535 | 0.0429 | 0.0353 | 0.0297 | 0.0253 | 0.0219 | 0.0191 | 0.0169 | 0.0150 | 0.0134 | 0.0121 | 0.0110 | 0.0100 |
| 125 | 0.1089 | 0.1007 | 0.0934 | 0.0870 | 0.0673 | 0.0540 | 0.0444 | 0.0372 | 0.0317 | 0.0274 | 0.0240 | 0.0211 | 0.0188 | 0.0168 | 0.0151 | 0.0137 | 0.0125 |
| 130 | 0.1322 | 0.1221 | 0.1132 | 0.1054 | 0.0813 | 0.0651 | 0.0535 | 0.0449 | 0.0382 | 0.0330 | 0.0288 | 0.0254 | 0.0226 | 0.0202 | 0.0182 | 0.0165 | 0.0150 |
| 135 | 0.1560 | 0.1440 | 0.1334 | 0.1241 | 0.0956 | 0.0764 | 0.0627 | 0.0525 | 0.0447 | 0.0386 | 0.0337 | 0.0297 | 0.0264 | 0.0236 | 0.0213 | 0.0192 | 0.0175 |
| 140 | 0.1805 | 0.1664 | 0.1540 | 0.1431 | 0.1100 | 0.0878 | 0.0720 | 0.0603 | 0.0513 | 0.0443 | 0.0386 | 0.0340 | 0.0302 | 0.0270 | 0.0243 | 0.0220 | 0.0200 |
| 145 | 0.2055 | 0.1892 | 0.1750 | 0.1625 | 0.1246 | 0.0993 | 0.0813 | 0.0681 | 0.0579 | 0.0499 | 0.0435 | 0.0384 | 0.0341 | 0.0305 | 0.0274 | 0.0248 | 0.0226 |
| 150 | 0.2312 | 0.2127 | 0.1965 | 0.1823 | 0.1395 | 0.1110 | 0.0908 | 0.0759 | 0.0645 | 0.0556 | 0.0485 | 0.0427 | 0.0379 | 0.0339 | 0.0305 | 0.0276 | 0.0251 |
| 155 | 0.2575 | 0.2366 | 0.2185 | 0.2025 | 0.1546 | 0.1228 | 0.1004 | 0.0838 | 0.0712 | 0.0614 | 0.0535 | 0.0471 | 0.0418 | 0.0374 | 0.0336 | 0.0304 | 0.0277 |
| 160 | 0.2846 | 0.2612 | 0.2409 | 0.2231 | 0.1699 | 0.1347 | 0.1100 | 0.0918 | 0.0780 | 0.0671 | 0.0585 | 0.0515 | 0.0457 | 0.0408 | 0.0367 | 0.0332 | 0.0302 |
| 165 | 0.3124 | 0.2864 | 0.2639 | 0.2442 | 0.1855 | 0.1468 | 0.1197 | 0.0999 | 0.0847 | 0.0729 | 0.0635 | 0.0559 | 0.0496 | 0.0443 | 0.0398 | 0.0360 | 0.0328 |
| 170 | 0.3410 | 0.3122 | 0.2874 | 0.2657 | 0.2012 | 0.1591 | 0.1296 | 0.1080 | 0.0916 | 0.0788 | 0.0686 | 0.0603 | 0.0535 | 0.0478 | 0.0430 | 0.0389 | 0.0353 |
| 175 | 0.3705 | 0.3388 | 0.3115 | 0.2877 | 0.2173 | 0.1715 | 0.1395 | 0.1161 | 0.0984 | 0.0847 | 0.0737 | 0.0648 | 0.0574 | 0.0513 | 0.0461 | 0.0417 | 0.0379 |
| 180 | 0.4008 | 0.3660 | 0.3361 | 0.3102 | 0.2336 | 0.1840 | 0.1495 | 0.1244 | 0.1054 | 0.0906 | 0.0788 | 0.0692 | 0.0614 | 0.0548 | 0.0493 | 0.0446 | 0.0405 |
| 185 | 0.4321 | 0.3940 | 0.3614 | 0.3331 | 0.2502 | 0.1967 | 0.1597 | 0.1327 | 0.1123 | 0.0965 | 0.0839 | 0.0737 | 0.0653 | 0.0583 | 0.0524 | 0.0474 | 0.0431 |
| 190 | 0.4644 | 0.4229 | 0.3873 | 0.3567 | 0.2671 | 0.2096 | 0.1699 | 0.1411 | 0.1193 | 0.1025 | 0.0891 | 0.0782 | 0.0693 | 0.0619 | 0.0556 | 0.0503 | 0.0457 |
| 195 | 0.4978 | 0.4525 | 0.4140 | 0.3808 | 0.2842 | 0.2226 | 0.1802 | 0.1495 | 0.1264 | 0.1085 | 0.0943 | 0.0828 | 0.0733 | 0.0654 | 0.0588 | 0.0531 | 0.0483 |
| 200 | 0.5324 | 0.4831 | 0.4413 | 0.4055 | 0.3017 | 0.2358 | 0.1907 | 0.1581 | 0.1335 | 0.1145 | 0.0995 | 0.0873 | 0.0773 | 0.0690 | 0.0620 | 0.0560 | 0.0509 |


|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| I/lb <br> Es (\%) | 4.80 | 5.00 | 5.50 | 6.00 | 6.50 | 7.00 | 7.50 | 8.00 | 8.50 | 9.00 | 9.50 | 10.00 | 12.50 | 15.00 | 17.50 | 20.00 |
| 105 | 0.0023 | 0.0021 | 0.0017 | 0.0014 | 0.0012 | 0.0010 | 0.0009 | 0.0008 | 0.0007 | 0.0006 | 0.0006 | 0.0005 | 0.0003 | 0.0002 | 0.0002 | 0.0001 |
| 110 | 0.0045 | 0.0042 | 0.0034 | 0.0029 | 0.0024 | 0.0021 | 0.0018 | 0.0016 | 0.0014 | 0.0013 | 0.0011 | 0.0010 | 0.0006 | 0.0004 | 0.0003 | 0.0003 |
| 115 | 0.0068 | 0.0063 | 0.0051 | 0.0043 | 0.0036 | 0.0031 | 0.0027 | 0.0024 | 0.0021 | 0.0019 | 0.0017 | 0.0015 | 0.0010 | 0.0007 | 0.0005 | 0.0004 |
| 120 | 0.0091 | 0.0084 | 0.0069 | 0.0057 | 0.0049 | 0.0042 | 0.0036 | 0.0032 | 0.0028 | 0.0025 | 0.0022 | 0.0020 | 0.0013 | 0.0009 | 0.0007 | 0.0005 |
| 125 | 0.0114 | 0.0105 | 0.0086 | 0.0072 | 0.0061 | 0.0052 | 0.0045 | 0.0040 | 0.0035 | 0.0031 | 0.0028 | 0.0025 | 0.0016 | 0.0011 | 0.0008 | 0.0006 |
| 130 | 0.0137 | 0.0126 | 0.0103 | 0.0086 | 0.0073 | 0.0063 | 0.0054 | 0.0048 | 0.0042 | 0.0038 | 0.0034 | 0.0030 | 0.0019 | 0.0013 | 0.0010 | 0.0008 |
| 135 | 0.0160 | 0.0147 | 0.0120 | 0.0101 | 0.0085 | 0.0073 | 0.0064 | 0.0056 | 0.0049 | 0.0044 | 0.0039 | 0.0035 | 0.0023 | 0.0016 | 0.0011 | 0.0009 |
| 140 | 0.0183 | 0.0168 | 0.0138 | 0.0115 | 0.0097 | 0.0084 | 0.0073 | 0.0064 | 0.0056 | 0.0050 | 0.0045 | 0.0040 | 0.0026 | 0.0018 | 0.0013 | 0.0010 |
| 145 | 0.0206 | 0.0189 | 0.0155 | 0.0129 | 0.0110 | 0.0094 | 0.0082 | 0.0072 | 0.0063 | 0.0056 | 0.0051 | 0.0046 | 0.0029 | 0.0020 | 0.0015 | 0.0011 |
| 150 | 0.0229 | 0.0211 | 0.0172 | 0.0144 | 0.0122 | 0.0105 | 0.0091 | 0.0080 | 0.0070 | 0.0063 | 0.0056 | 0.0051 | 0.0032 | 0.0022 | 0.0016 | 0.0013 |
| 155 | 0.0253 | 0.0232 | 0.0190 | 0.0158 | 0.0134 | 0.0115 | 0.0100 | 0.0088 | 0.0077 | 0.0069 | 0.0062 | 0.0056 | 0.0035 | 0.0025 | 0.0018 | 0.0014 |
| 160 | 0.0276 | 0.0253 | 0.0207 | 0.0173 | 0.0147 | 0.0126 | 0.0109 | 0.0096 | 0.0085 | 0.0075 | 0.0067 | 0.0061 | 0.0039 | 0.0027 | 0.0020 | 0.0015 |
| 165 | 0.0299 | 0.0275 | 0.0225 | 0.0187 | 0.0159 | 0.0136 | 0.0118 | 0.0104 | 0.0092 | 0.0082 | 0.0073 | 0.0066 | 0.0042 | 0.0029 | 0.0021 | 0.0016 |
| 170 | 0.0323 | 0.0296 | 0.0242 | 0.0202 | 0.0171 | 0.0147 | 0.0128 | 0.0112 | 0.0099 | 0.0088 | 0.0079 | 0.0071 | 0.0045 | 0.0031 | 0.0023 | 0.0018 |
| 175 | 0.0346 | 0.0317 | 0.0260 | 0.0217 | 0.0183 | 0.0157 | 0.0137 | 0.0120 | 0.0106 | 0.0094 | 0.0084 | 0.0076 | 0.0048 | 0.0034 | 0.0025 | 0.0019 |
| 180 | 0.0370 | 0.0339 | 0.0277 | 0.0231 | 0.0196 | 0.0168 | 0.0146 | 0.0128 | 0.0113 | 0.0101 | 0.0090 | 0.0081 | 0.0052 | 0.0036 | 0.0026 | 0.0020 |
| 185 | 0.0393 | 0.0361 | 0.0295 | 0.0246 | 0.0208 | 0.0179 | 0.0155 | 0.0136 | 0.0120 | 0.0107 | 0.0096 | 0.0086 | 0.0055 | 0.0038 | 0.0028 | 0.0021 |
| 190 | 0.0417 | 0.0382 | 0.0313 | 0.0261 | 0.0221 | 0.0189 | 0.0164 | 0.0144 | 0.0127 | 0.0113 | 0.0101 | 0.0091 | 0.0058 | 0.0040 | 0.0030 | 0.0023 |
| 195 | 0.0441 | 0.0404 | 0.0330 | 0.0275 | 0.0233 | 0.0200 | 0.0173 | 0.0152 | 0.0134 | 0.0119 | 0.0107 | 0.0096 | 0.0061 | 0.0043 | 0.0031 | 0.0024 |
| 200 | 0.0464 | 0.0426 | 0.0348 | 0.0290 | 0.0245 | 0.0211 | 0.0183 | 0.0160 | 0.0141 | 0.0126 | 0.0113 | 0.0102 | 0.0065 | 0.0045 | 0.0033 | 0.0025 |

## Breaker failure ANSI code 50BF

## Backup protection if the circuit breaker does not trip.

## Description

If a breaker fails to open following a tripping order (detected by the non-extinction of the fault current), this backup protection sends a tripping order to the upstream or adjacent breakers.
The "breaker failure" protection function is activated by an O 1 output tripping order received from the overcurrent protection functions which trip the circuit breaker ( $50 / 51,50 \mathrm{~N} / 51 \mathrm{~N}, 46,67 \mathrm{~N}, 67,64 \mathrm{REF}, 87 \mathrm{M}, 87 \mathrm{~T}$ ). It checks for the disappearance of current during the time interval specified by the time delay T . It may also take into account the position of the circuit breaker, read on the logic inputs to determine the actual opening of the breaker. Wiring a volt-free closed circuit breaker position contact on the "breaker closed" equation editor input or Logipam can ensure that the protection is effective in the following situations:
■ When 50BF is activated by protection function $50 \mathrm{~N} / 51 \mathrm{~N}$ (set point Is0 $<0.2 \mathrm{In}$ ),
detection of the 50BF current set point can possibly not be operational.
■ When trip circuit supervision (TCS) is used, the closed circuit breaker contact is short-circuited. Logic input I101 is therefore no longer operational.
Automatic activation of this protection function requires the use of the circuit breaker control function in the control logic. A specific input may also be used to activate the protection by logic equation or by Logipam. That option is useful for adding special cases of activation (e.g. tripping by an external protection unit).
The time-delayed output of the protection function should be assigned to a logic output via the control matrix.
Starting and stopping of the time delay T counter are conditioned by the presence of a current above the set point ( $\mathrm{l}>\mathrm{Is}$ ).

## Block diagram



Setting: (1) Not accounting for the circuit breaker position
(2) Accounting for the circuit breaker position

Characteristics

| Settings |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Is set point |  |  |  |  |
| Setting range | 0.2 ln to 2 ln |  |  |  |
| Accuracy ${ }^{(1)}$ | $\pm 5$ \% |  |  |  |
| Resolution | 0.1 A |  |  |  |
| Drop out/pick up ratio | 87.5 \% $\pm 2$ \% |  |  |  |
| Time delay T |  |  |  |  |
| Setting range | 50 ms to 3 s |  |  |  |
| Accuracy ${ }^{(1)}$ | $\pm 2 \%$ or -10 ms to +15 ms |  |  |  |
| Resolution | 10 ms or 1 digit |  |  |  |
| Taking into account circuit breaker position |  |  |  |  |
| Setting range | With / without |  |  |  |
| Characteristic times |  |  |  |  |
| Overshoot time | $<35 \mathrm{~ms}$ at 2 Is |  |  |  |
| Inputs |  |  |  |  |
| Designation | Syntax | Equations | Logipam |  |
| Protection reset | P50BF_1_101 | ■ | $\square$ |  |
| Start 50BF | P50BF_1_107 | - | ■ |  |
| Protection inhibition | P50BF_1_113 | $\square$ | $\square$ |  |
| Breaker closed | P50BF_1_119 | $\square$ | - |  |
| Outputs |  |  |  |  |
| Designation | Syntax | Equations | Logipam | Matrix |
| Instantaneous output (pick-up) | P50BF_1_1 | ■ | - |  |
| Delayed output | P50BF_1_3 | $\square$ | $\square$ | - |
| Protection inhibited | P50BF_1_16 | $\square$ | $\square$ |  |

## (1) Under reference conditions (IEC 60255-6)

## Example of setting

Below is a case that may be used to determine the time-delay setting of the breaker failure function:
■ overcurrent protection setting: T = inst

- circuit breaker operating time: 60 ms
- auxiliary relay operating time to open the upstream breaker(s): 10 ms .


## Fault

器】 clearing of fault
without breaker failure


The breaker failure function time delay is the sum of the following times:

- Sepam O1 output relay pick-up time $=10 \mathrm{~ms}$
- circuit breaker opening time $=60 \mathrm{~ms}$
- Breaker failure function overshoot time $=35 \mathrm{~ms}$.

To avoid unwanted tripping of the upstream breakers, add a margin of approximately 20 ms .
The time delay is 125 ms minimum, set at 130 ms .

## Protection functions

Inadvertent energization ANSI code 50/27

Protection against inadvertent energization of generators that are shut down.


Example: Generator shutdown and normal starting.


Example: Generator shutdown and inadvertent starting.

## Description

The protection function checks the generator starting sequence to detect inadvertent energization of generators that are shut down.
A generator which is energized when shut down operates like a motor. A starting current occurs and produces significant heat rise that can damage machine windings.
The check on the generator starting sequence is carried out by an instantaneous phase overcurrent protection function, confirmed by an undervoltage protection function. The undervoltage protection function is set up with:

- an on time delay T1 to make the function insensitive to voltage sags
- a timer hold T2 during which the function detects a generator starting current caused by inadvertent energization.
By taking into account the circuit-breaker position, it is possible to check the quality of synchronization. If when the machine couples, the voltage and frequency differences are too high, when the circuit breaker closes, a current immediately appears that the function detects.
When the VT monitoring detects a measurement problem on the voltage channels, the part concerning the voltages is inhibited.

Block diagram


## Characteristics

| Settings |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Current set point |  |  |  |  |
| Setting range | 0.05 to 4 In |  |  |  |
| Accuracy ${ }^{(1)}$ | $\pm 5 \%$ or 0.02 ln |  |  |  |
| Resolution | 1 A |  |  |  |
| Drop out/pick up ratio | 95.5 \% or 0.015 ln |  |  |  |
| Voltage set point |  |  |  |  |
| Setting range | $10 \%$ to $100 \%$ of Un |  |  |  |
| Accuracy ${ }^{(1)}$ | $\pm 2$ \% or 0.005 Unp |  |  |  |
| Resolution | 1 \% |  |  |  |
| Drop out/pick up ratio | 103 \% |  |  |  |
| Advanced settings |  |  |  |  |
| Use of breaker position |  |  |  |  |
| Setting range | Used / not used |  |  |  |
| T1 time |  |  |  |  |
| Setting range | 0 to 10 s |  |  |  |
| Accuracy ${ }^{(1)}$ | $\pm 2 \%$ or from -10 ms to +25 ms |  |  |  |
| Resolution | 10 ms or 1 digit |  |  |  |
| T2 time |  |  |  |  |
| Setting range | 0 to 10 s |  |  |  |
| Accuracy ${ }^{(1)}$ | $\pm 2 \%$ or from -10 ms to +25 ms |  |  |  |
| Resolution | 10 ms or 1 digit |  |  |  |
| Characteristic times ${ }^{(1)}$ |  |  |  |  |
| Operation time | < 40 ms at 2 Is (typically 30 ms ) |  |  |  |
| Inputs |  |  |  |  |
| Designation | Syntax | Equations Logipam |  |  |
| Protection reset | P50/27_1_101 | - | ■ |  |
| Protection inhibition | P50/27_1_113 ■ ■ |  |  |  |
| Outputs |  |  |  |  |
| Designation | Syntax | Equations | Logipam | Matrix |
| Tripping output | P50/27_1_3 | - | - | $\square$ |
| Protection inhibited | P50/27_1_16 | $\square$ | - |  |
| Protection ready | P50/27_1_35 | $\square$ | - |  |

(1) Under reference conditions (IEC 60255-6).

## Example of setting

Synchronous generator data
■ $\mathrm{S}=3.15 \mathrm{MVA}$

- Un1 $=6.3 \mathrm{kV}$
- $\mathrm{Xd}=233 \%$
- X'd = 21 \%
- X"d=15\%
- the generator is connected to a network with a Psc $=10$ MVA
- the maximum admissible duration of a voltage sag is 2.5 seconds.

To set the protection function, it is necessary to calculate the rated generator impedance:

- $\mathrm{lb}=\mathrm{S} /(\sqrt{3} . \mathrm{Un} 1)=289 \mathrm{~A}$
- $\mathrm{Zn}=\mathrm{Un} 1 /(\sqrt{3} . \mathrm{lb})=12.59 \Omega$

The network impedance is:
Zpsc $=(\text { Un1 })^{2} /$ Psc $=3.97 \Omega$
The Istart starting current is approximately:
Istart $=\frac{\mathrm{Un} 1}{\sqrt{3}\left(\mathrm{Zpsc}+\frac{\mathrm{X}^{\prime \prime} \mathrm{d}}{100} \times \mathrm{Zn}\right)}=621 \mathrm{~A}$
The current set point is set between $20 \%$ and $50 \%$ of the starting current.

## Is $=\mathbf{0 , 5} \times$ Istart $\sim 311 \mathrm{~A}$

The voltage set point is often set between $80 \%$ and $85 \%$ of Un. In this example, the selected set point is Us = $85 \%$.
The T1 time is set longer than the maximum admissible duration of a voltage sag, e.g. $\mathrm{T} 1=4 \mathrm{sec}$.

T2 is set to detect the appearance of a current during starting.
For example, T2 = 250 ms .

Protection against overcurrents and overloads.

## Operation

Protection against overcurrents or overloads:

- It is three-phase and includes a time delay, which is either definite or IDMT.

■ Each of the 8 relays has 2 groups of settings. The setting group A or B can be switched by a logic input or a remote control order depending on the parameter setting.
■ For better detection of faraway faults, protection can be confirmed by unit 1 of one of the following protections:

- undervoltage
- negative sequence overvoltage.
- The custom curve, defined point by point, can be used with this protection.
- An adjustable timer hold delay, either definite or IDMT, allows coordination with electromechanical relays and detection of reboot faults.
- The protection incorporates a harmonic 2 restraint which can be used to set the protection Is set point close to the rated current of the device to be protected, for example to avoid transformer inrush currents.
This harmonic 2 restraint, which can be selected by parameter setting, is active as long as the current is less than half the minimum short-circuit current of the network downstream of the device to be protected.

| Tripping curve | Timer hold |
| :--- | :--- |
| Definite time (DT) | Definite time |
| Standard inverse time (SIT) | Definite time |
| Very inverse time (VIT or LTI) | Definite time |
| Extremely inverse time (EIT) | Definite time |
| Ultra inverse time (UIT) | Definite time |
| RI curve | Definite time |
| IEC inverse time SIT / A | Definite time or IDMT |
| IEC very inverse time VIT or LTI / B | Definite time or IDMT |
| IEC extremely inverse time EIT / C | Definite time or IDMT |
| IEEE moderately inverse (IEC / D) | Definite time or IDMT |
| IEEE very inverse (IEC / E) | Definite time or IDMT |
| IEEE extremely inverse (IEC / F) | Definite time or IDMT |
| IAC inverse | Definite time or IDMT |
| IAC very inverse | Definite time or IDMT |
| IAC extremely inverse | Definite time or IDMT |
| Customized | Definite time |

Block diagram


## Protection functions

## Phase overcurrent ANSI code 50/51

## Characteristics

| Settings |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Measurement origin |  |  |  |  |
| Setting range | Main channels (I) / Additional channels (l) |  |  |  |
| Tripping curve |  |  |  |  |
| Setting range | See previous page |  |  |  |
| Is set point |  |  |  |  |
| Setting range | Definite time | $0.05 \mathrm{In} \leqslant \mathrm{Is} \leqslant 24 \mathrm{In}$ expressed in amperes |  |  |
|  | IDMT | $0.05 \mathrm{In} \leqslant \mathrm{Is} \leqslant 2.4 \mathrm{In}$ expressed in amperes |  |  |
| Accuracy (1) | $\pm 5 \%$ or $\pm 0.01 \mathrm{ln}$ |  |  |  |
| Resolution | 1 A or 1 digit |  |  |  |
| Drop out/pick up ratio | $93.5 \% \pm 5 \%$ or > (1-0.015 In/ls) $\times 100 \%$ |  |  |  |
| Time delay T (operation time at 10 ls ) |  |  |  |  |
| Setting range | Definite time | Inst, $50 \mathrm{~ms} \leqslant \mathrm{~T} \leqslant 300 \mathrm{~s}$ |  |  |
|  | IDMT | $100 \mathrm{~ms} \leqslant \mathrm{~T} \leqslant 12.5 \mathrm{~s}$ or TMS ${ }^{(2)}$ |  |  |
| Accuracy ${ }^{(1)}$ | Definite time | $\pm 2 \%$ or from -10 ms to +25 ms |  |  |
|  | IDMT | Class 5 or from -10 ms to +25 ms |  |  |
| Resolution | 10 ms or 1 digit |  |  |  |
| Advanced settings |  |  |  |  |
| Confirmation |  |  |  |  |
| Setting range | By undervoltage (unit 1) <br> By negative sequence overvoltage (unit 1) <br> None, no confirmation |  |  |  |
| Timer hold T1 |  |  |  |  |
| Setting range | Definite time | 0; 0.05 to 300 s |  |  |
|  | IDMT ${ }^{(3)}$ | 0.5 to 20 s |  |  |
| Resolution | 10 ms or 1 digit |  |  |  |
| Harmonic 2 restraint |  |  |  |  |
| Setting range | 5 to $50 \%$ |  |  |  |
| Resolution | 1 \% |  |  |  |
| Minimum short-circuit current Isc |  |  |  |  |
| Setting range | In to 999 kA |  |  |  |
| Resolution | de 1 to 9.99 0.01 <br> de 10 to 99.9 0.1 <br> de 100 to 999 1 <br> Minimum interval 0.1 A |  |  |  |
| Characteristic times |  |  |  |  |
| Operation time | pick-up $<40 \mathrm{~ms}$ at 2 Is (typically 25 ms ) <br> confirmed instantaneous: <br> inst. $<55 \mathrm{~ms}$ at 2 Is for Is $\geqslant 0.3 \mathrm{In}$ (typically 35 ms ) <br> inst. $<70 \mathrm{~ms}$ at 2 Is for $\mathrm{Is}<0.3 \ln$ (typically 50 ms ) |  |  |  |
| Overshoot time | $<50 \mathrm{~ms}$ at 2 Is |  |  |  |
| Reset time | $<50 \mathrm{~ms}$ at 2 Is (for $\mathrm{T} 1=0$ ) |  |  |  |
| Inputs |  |  |  |  |
| Designation | Syntax | Equations | Logipam |  |
| Protection reset | P50/51_x_101 | ■ | - |  |
| Protection inhibition | P50/51_x_113 | ■ | ■ |  |
| Outputs |  |  |  |  |
| Designation | Syntax | Equations | Logipam | Matrix |
| Instantaneous output (pick-up) | P50/51_x_1 | ■ | $\square$ |  |
| Delayed output | P50/51_x_3 | - | - | - |
| Drop out | P50/51_x_4 | - | $\square$ |  |
| Phase 1 fault | P50/51_x_7 | $\square$ | $\square$ |  |
| Phase 2 fault | P50/51_x_8 | - | - |  |
| Phase 3 fault | P50/51_x_9 | - | - |  |
| Protection inhibited | P50/51_x_16 | - | ■ |  |
| $\bar{x}$ : unit number. <br> (1) Under reference conditions (IEC 60255-6). <br> (2) Setting ranges in TMS (Time Multiplier Setting) mode |  |  |  |  |
|  |  |  |  |  |
|  |  |  |  |  |
| ■ Inverse (SIT) and IEC SIT/A: 0.04 to 4.20 |  |  |  |  |
| - Very inverse (VIT) and IEC VIT/B: 0.07 to 8.33 |  |  |  |  |
| - Very inverse (LTI) and IEC LTI/B: 0.01 to 0.93 |  |  |  |  |
| - Ext. inverse (EIT) and IEC EIT/C: 0.13 to 15.47 |  |  |  |  |
| - IEEE moderately inverse: 0.42 to 51.86 |  |  |  |  |
| - IEEE very inverse: 0.73 to 90.57 |  |  |  |  |
| - IEEE extremely inverse: 1.24 to 154.32 |  |  |  |  |
| - IAC inverse: 0.34 to 42.08 |  |  |  |  |
| - IAC very inverse: 0.61 to 75.75 |  |  |  |  |
| IAC extremely inverse: 1.08 to 134.4 . <br> (3) Only for standardized tripping curves of the IEC, IEEE and IAC types. |  |  |  |  |

## Protection against earth faults.

## Description

Earth fault protection based on measured neutral, zero sequence or earth fault tank earth leakage protection) current:

- the protection function has a definite or IDMT time delay.
- each of the eight units has two groups of settings. Switching to setting group A
or B can be carried out by a logic input or a remote control order, depending on the settings.
- The protection function includes a harmonic 2 restraint which can be set to provide greater saturation stability of the CT phases when transformers are energized.
The protection function includes a harmonic 2 restraint which prevents an incorrect residual current from being measured on the sum of the 3 CT phases when transformers are energized.
- The restraint value can be set in the configuration. The harmonic 2 restraint is used
to trigger the protection on intermittent earth faults.
- the customized curve, defined point by point, can be used with this protection function.
- an adjustable timer hold, definite or IDMT, can be used for coordination with electromagnetic relays and to detect restriking faults.
- each unit can be independently set to one of the two measurement channels 10 or I'O or to the sum of the phase currents on the main or additional channels. By mixing the possibilities on the different units, it is possible to have:
- different dynamic set points
- different applications, e.g. zero sequence and tank earth leakage protection.

| Tripping curve | Timer hold curve |
| :--- | :--- |
| Definite time (DT) | Definite time |
| Standard inverse time (SIT) | Definite time |
| Very inverse time (VIT or LTI) | Definite time |
| Extremely inverse time (EIT) | Definite time |
| Ultra inverse time (UIT) | Definite time |
| RI curve | Definite time |
| IEC inverse time SIT / A | Definite time or IDMT |
| IEC very inverse time VIT or LTI / B | Definite time or IDMT |
| IEC extremely inverse time EIT / C | Definite time or IDMT |
| IEEE moderately inverse (IEC / D) | Definite time or IDMT |
| IEEE very inverse (IEC / E) | Definite time or IDMT |
| IEEE extremely inverse (IEC / F) | Definite time or IDMT |
| IAC inverse | Definite time or IDMT |
| IAC very inverse | Definite time or IDMT |
| IAC extremely inverse | Definite time or IDMT |
| EPATR-B | Definite time |
| EPATR-C | Definite time |
| Customized | Definite time |

Block diagram

$x$ : unit number.
(1) Under reference conditions (IEC 60255-6).
(2) Setting ranges in TMS (Time Multiplier Setting) mode

■ Inverse (SIT) and IEC SIT/A: 0.04 to 4.20

- Very inverse (VIT) and IEC VIT/B: 0.07 to 8.33
- Very inverse (LTI) and IEC LTI/B: 0.01 to 0.93
- Ext. inverse (EIT) and IEC EIT/C: 0.13 to 15.47
- IEEE moderately inverse: 0.42 to 51.86
- IEEE very inverse: 0.73 to 90.57
- IEEE extremely inverse: 1.24 to 154.32
- IAC inverse: 0.34 to 42.08
- IAC very inverse: 0.61 to 75.75
- IAC extremely inverse: 1.08 to 134.4.
(3) Only for standardized tripping curves of the IEC, IEEE and IAC types.

Characteristics

| Settings |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Measurement origin |  |  |  |  |
| Setting range | ```IO I'0 IO\Sigma (sum of the main phase channels) I'O\Sigma (sum of the additional phase channels)``` |  |  |  |
| Tripping curve |  |  |  |  |
| Setting range | See previous page |  |  |  |
| Is0 setting |  |  |  |  |
| Definite time setting range | $0.01 \mathrm{ln} 0 \leqslant \mathrm{Is} 0 \leqslant 15 \mathrm{In} 0(\mathrm{~min} .0 .1 \mathrm{~A})$ expressed in amperes |  |  |  |
|  | Sum of CTs $\quad 0.01 \mathrm{ln} \leqslant \mathrm{Is} 0 \leqslant 15 \ln (\mathrm{~min} .0 .1 \mathrm{~A})$ |  |  |  |
|  | With CSH sensor  <br> 2 A rating 0.1 to 30 A <br> 20 A rating 0.2 to 300 A |  |  |  |
|  | CT | $0.01 \mathrm{ln} 0 \leqslant \mathrm{ls} 0 \leqslant 15 \mathrm{In} 0(\mathrm{~min} .0 .1 \mathrm{~A})$ |  |  |
|  | $\begin{aligned} & \text { Core balance CT } \\ & + \text { ACE990 } \\ & \hline \end{aligned}$ | $0.01 \ln 0 \leqslant \operatorname{ls} 0 \leqslant 15 \ln 0(\mathrm{~min} .0 .1 \mathrm{~A})$ |  |  |
| IDMT setting range | $0.01 \mathrm{In} 0 \leqslant \mathrm{Is} 0 \leqslant \mathrm{In} 0(\mathrm{~min} .0 .1 \mathrm{~A})$ expressed in amperes |  |  |  |
|  | Sum of CTs | $0.01 \mathrm{ln} \leqslant \mathrm{Is} 0 \leqslant \ln (\mathrm{~min} .0 .1 \mathrm{~A})$ |  |  |
|  | With CSH sensor  <br> 2 A rating 0.1 to 2 A <br> 20 A rating 0.2 to 20 A |  |  |  |
|  | CT | $0.01 \mathrm{ln} 0 \leqslant \mathrm{ls} 0 \leqslant \ln 0(\mathrm{~min} .0 .1 \mathrm{~A})$ |  |  |
|  | $\begin{aligned} & \text { Core balance CT } \\ & + \text { ACE990 } \\ & \hline \end{aligned}$ | $0.01 \mathrm{In} 0 \leqslant \operatorname{ls} 0 \leqslant \ln 0(\mathrm{~min} .0 .1 \mathrm{~A})$ |  |  |
| EPATR <br> Setting range | CSH sensor 20 A rating | 0.6 to 5 A |  |  |
|  | Core balance CT $\quad 0.6$ to 5 Awith ACE990and $15 \mathrm{~A} \leqslant \operatorname{In} 0 \leqslant 50 \mathrm{~A}$ |  |  |  |
| Accuracy ${ }^{(1)}$ | $\pm 5 \%$ or $\pm 0.004 \mathrm{ln} 0$ |  |  |  |
| Resolution | 1 A or 1 digit |  |  |  |
| Drop out/pick up ratio | $93.5 \% \pm 5 \%$ or > (1-0.005 $\mathrm{In} 0 / \mathrm{ls} 0) \times 100 \%$ |  |  |  |
| Time delay $\mathbf{T}$ (operation time at 10 ls 0 ) |  |  |  |  |
| Setting range | Definite time | Inst, $50 \mathrm{~ms} \leqslant \mathrm{~T} \leqslant 300 \mathrm{~s}$ |  |  |
|  | IDMT $100 \mathrm{~ms} \leqslant \mathrm{~T} \leqslant 12.5 \mathrm{~s}$ or TMS ${ }^{(2)}$ |  |  |  |
|  | EPATR-B | 0.5 to 1 s |  |  |
|  |  | 0.1 to 3 s |  |  |
| Accuracy ${ }^{(1)}$ | Definite time | $\pm 2 \%$ or from $-10 \mathrm{~ms} \mathrm{to}+25 \mathrm{~ms}$ |  |  |
|  | IDMT | Class 5 or from $-10 \mathrm{~ms} \mathrm{to}+25 \mathrm{~ms}$ |  |  |
| Resolution | 10 ms or 1 digit |  |  |  |
| Advanced settings |  |  |  |  |
| Harmonic 2 restraint |  |  |  |  |
| Fixed threshold | $17 \% \pm 3$ \% |  |  |  |
| Timer hold T1 |  |  |  |  |
| Setting range | Definite time | 0; 0.05 to 300 s |  |  |
|  | IDMT ${ }^{(3)}$ | 0.5 to 20 s |  |  |
| Resolution | 10 ms or 1 digit |  |  |  |
| Characteristic times |  |  |  |  |
| Operation time | Pick-up $<40 \mathrm{~ms}$ at 2 IsO (typically 25 ms ) <br> Confirmed instantaneous: <br> ■ inst $<55 \mathrm{~ms}$ at 2 IsO for Is $\geqslant 0.3 \mathrm{In} 0$ (typically 35 ms ) <br> - inst < 70 ms at 2 IsO for Is $<0.3 \mathrm{In} 0$ (typically 50 ms ) |  |  |  |
| Overshoot time | $<40 \mathrm{~ms}$ at 2 ls 0 |  |  |  |
| Reset time | $<50 \mathrm{~ms}$ at 2 Is 0 (for T1 $=0$ ) |  |  |  |
| Inputs |  |  |  |  |
| Designation | Syntax | Equations Logipam |  |  |
| Protection reset | P50N/51N_x_101 | ■ | $\square$ |  |
| Protection inhibition | P50N/51N_x_113 | $\square$ | $\square$ |  |
| Outputs |  |  |  |  |
| Designation | Syntax | Equations | Logipam | Matrix |
| Instantaneous output (pick-up) | P50N/51N_x_1 | ■ | ■ |  |
| Delayed output | P50N/51N_x_3 | $\square$ | $\square$ | ■ |
| Drop out | P50N/51N_x_4 | $\square$ | $\square$ |  |
| Protection inhibited | P50N/51N_x_16 | $\square$ | ■ |  |
| 15 A set point output | P50N/51N_x_56 | - | $\square$ |  |



## EPATR-B curves

EPATR-B tripping curves are defined from the following equations:

- for Is $0 \leqslant 10 \leqslant 6.4 \mathrm{~A}$
- for $6.4 \mathrm{~A} \leqslant 10 \leqslant 200 \mathrm{~A}$
- for $10>200 \mathrm{~A}$

$$
\begin{aligned}
& t=\frac{85,386}{10^{0,(708)}} \times \frac{T}{0,8} \\
& t=\frac{140,213}{10^{0,975}} \times \frac{T}{0,8} \\
& t=T
\end{aligned}
$$



## EPATR-C curves

EPATR-C tripping curves are defined from the following equations:
■ for Is $0 \leqslant 10 \leqslant 200 \mathrm{~A}$
$t=\frac{72}{10^{2 / 3}} \times \frac{T}{2,10}$

- for $10>200 \mathrm{~A}$
$t=T$

EPATR-C standard curve (log scales)
Curve (1): $I \mathrm{~s} O=5 \mathrm{~A}$ and $T=3 \mathrm{~s}$
Curve (2): $I \mathrm{~s} O=0.6 \mathrm{~A}$ and $T=0.1 \mathrm{~s}$
Curve (3): $\mathrm{Is} O$ and $T$

Generator protection against close short-circuits.


Set point adjustment.

## Description

The voltage-restrained overcurrent protection function is used to protect generators. The operation set point is adjusted according to the voltage to take into account cases of faults close to the generator which cause voltage dips and short-circuit current:

- the protection function is three-phase and has a definite or IDMT time delay
- the customized curve, defined point by point, may be used with this protection function
■ an adjustable timer hold, definite time or IDMT, can be used for coordination with electromagnetic relays and to detect restriking faults
■ the set point is adjusted according to the lowest of the phase-to-phase voltages measured. The adjusted set point $l_{\mathrm{s}}^{*}$ is defined by the following equation:
$I_{s}^{*}=\frac{\mathrm{Is}}{3} \times\left(4 \frac{\mathrm{U}}{\mathrm{Un}}-0.2\right)$

| Tripping curve | Timer hold |
| :--- | :--- |
| Definite time (DT) | Definite time |
| Standard inverse time (SIT) | Definite time |
| Very inverse time (VIT or LTI) | Definite time |
| Extremely inverse time (EIT) | Definite time |
| Ultra inverse time (UIT) | Definite time |
| RI curve | Definite time |
| IEC inverse time SIT / A | Definite time or IDMT |
| IEC very inverse time VIT or LTI / B | Definite time or IDMT |
| IEC extremely inverse time EIT / C | Definite time or IDMT |
| IEEE moderately inverse (IEC / D) | Definite time or IDMT |
| IEEE very inverse (IEC / E) | Definite time or IDMT |
| IEEE extremely inverse (IEC / F) | Definite time or IDMT |
| IAC inverse | Definite time or IDMT |
| IAC very inverse | Definite time or IDMT |
| IAC extremely inverse | Definite time or IDMT |
| Customized | Definite time |

Block diagram


## Characteristics

| Settings |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Measurement origin |  |  |  |  |
| Setting range | Main channels (I) / Additional channels (l') |  |  |  |
| Tripping curve |  |  |  |  |
| Setting range | See previous page |  |  |  |
| Is set point |  |  |  |  |
| Setting range | Definite time | $0.5 \mathrm{ln} \leqslant \mathrm{Is} \leqslant 24 \mathrm{ln}$ expressed in amperes |  |  |
|  | IDMT | $0.5 \mathrm{ln} \leqslant \mathrm{Is} \leqslant 2.4 \mathrm{In}$ expressed in amperes |  |  |
| Accuracy ${ }^{(1)}$ | $\pm 5$ \% |  |  |  |
| Resolution | 1 A or 1 digit |  |  |  |
| Drop out/pick up ratio | 93.5 \% (with min. reset variance of 0.015 In ) |  |  |  |
| Time delay T (operation time at 10 ls ) |  |  |  |  |
| Setting range | Definite time | Inst, $50 \mathrm{~ms} \leqslant \mathrm{~T} \leqslant 300 \mathrm{~s}$ |  |  |
|  | IDMT | $100 \mathrm{~ms} \leqslant \mathrm{~T} \leqslant 12.5 \mathrm{~s}$ or TMS ${ }^{(2)}$ |  |  |
| Accuracy ${ }^{(1)}$ | Definite time | $\pm 2 \%$ or from -10 ms to +25 ms |  |  |
|  | IDMT | Class 5 or from -10 ms to +25 ms |  |  |
| Resolution | 10 ms or 1 digit |  |  |  |
| Advanced settings |  |  |  |  |
| Timer hold T1 |  |  |  |  |
| Setting range | Definite time | 0; 0.05 to 300 s |  |  |
|  | IDMT time ${ }^{(3)}$ | 0.5 to 20 s |  |  |
| Resolution | 10 ms or 1 digit |  |  |  |
| Characteristic times |  |  |  |  |
| Operation time | Pick-up < 35 ms at 2 Is (typically 25 ms ) Inst. < 50 ms at 2 Is (confirmed instantaneous) (typically 35 ms ) |  |  |  |
| Overshoot time | $<50 \mathrm{~ms}$ |  |  |  |
| Reset time | $<50 \mathrm{~ms}$ (for T1 = 0) |  |  |  |
| Inputs |  |  |  |  |
| Designation | Syntax | Equations | Logipam |  |
| Protection reset | P50V/51V_x_101 | ■ | $\square$ |  |
| Protection inhibition | P50V/51V_x_113 | $\square$ | $\square$ |  |
| Outputs |  |  |  |  |
| Designation | Syntax | Equations | Logipam | Matrix |
| Instantaneous output (pick-up) | P50V/51V_x_1 | ■ | $\square$ |  |
| Delayed output | P50V/51V_x_3 | $\square$ | - | - |
| Drop out | P50V/51V_x_4 | $\square$ | $\square$ |  |
| Phase 1 fault | P50V/51V_x_7 | $\square$ | $\square$ |  |
| Phase 2 fault | P50V/51V_x_8 | $\square$ | $\square$ |  |
| Phase 3 fault | P50V/51V_x_9 | $\square$ | $\square$ |  |
| Protection inhibited | P50V/51V_x_16 | $\square$ | $\square$ |  |
| $x$ : unit number. |  |  |  |  |
| (1) Under reference conditions (IEC 60255-6). |  |  |  |  |
| (2) Setting ranges in TMS (Time Multiplier Setting) mode |  |  |  |  |
| - Inverse (SIT) and IEC SIT/A: 0.04 to 4.20 |  |  |  |  |
| - Very inverse (VIT) and IEC VIT/B: 0.07 to 8.33 |  |  |  |  |
| - Very inverse (LTI) and IEC LTI/B: 0.01 to 0.93 |  |  |  |  |
| - Ext. inverse (EIT) and IEC EIT/C: 0.13 to 15.47 |  |  |  |  |
| - IEEE moderately inverse: 0.42 to 51.86 |  |  |  |  |
| ■ IEEE very inverse: 0.73 to 90.57 |  |  |  |  |
| - IEEE extremely inverse: 1.24 to 154.32 |  |  |  |  |
| - IAC inverse: 0.34 to 42.08 |  |  |  |  |
| - IAC very inverse: 0.61 to 75.75 |  |  |  |  |
| - IAC extremely inverse: 1.08 to 134.4. <br> (3) Only for standardized tripping curves of the IEC, IEEE and IAC types. |  |  |  |  |
|  |  |  |  |  |

## Protection functions

Detection of capacitor bank internal faults by measurement of the unbalance current flowing between the 2 neutral points of a double-star connected capacitor bank.

## Description

The capacitor bank unbalance function detects unbalance current flowing between the two neutral points of double-star connected capacitor banks.

The protection function is activated when the unbalance current is higher than the Is current set point during tripping time T .

## Block diagram



## Characteristics

| Settings |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Set point Is |  |  |  |  |
| Setting range | 0.02 I'n to 2 l'n with a minimum value of 0.05 A |  |  |  |
| Accuracy ${ }^{(1)}$ | $\pm 5 \%$ |  |  |  |
| Resolution | 0.01 A |  |  |  |
| Drop out/pick up ratio | 93.5 \% |  |  |  |
| Time delay |  |  |  |  |
| Setting range | 0.1 to 300 s |  |  |  |
| Accuracy ${ }^{(1)}$ | $\pm 2 \%$ or $\pm 25 \mathrm{~ms}$ |  |  |  |
| Resolution | 10 ms or 1 digit |  |  |  |
| Characteristic times ${ }^{(1)}$ |  |  |  |  |
| Operation time | Pick-up < 35 ms |  |  |  |
| Overshoot time | $<35 \mathrm{~ms}$ |  |  |  |
| Reset time | < 50 ms |  |  |  |
| Inputs |  |  |  |  |
| Designation | Syntax | Equations | Logipam |  |
| Protection reset | P51C_x_101 | - | $\square$ |  |
| Protection inhibition | P51C_x_113 | - | - |  |
| Outputs |  |  |  |  |
| Designation | Syntax | Equations | Logipam | Matrix |
| Instantaneous output | P51C_x_1 | ■ | $\square$ |  |
| Tripping output | P51C_x_3 | $\square$ | $\square$ | - |
| Protection inhibed | P51C_x_16 | $\square$ | $\square$ |  |
| $x$ : unit number. <br> (1) Under reference conditions | 255-6). |  |  |  |

## Overvoltage (L-L or L-N) <br> ANSI code 59

Protection against phase-to-neutral or phase-to-phase overvoltages.

## Operation

Protection against overvoltages or check that there is sufficient voltage present to authorize a source transfer:
■ it is single-phase and operates on phase-to-neutral or phase-to-phase voltage
■ it includes a time delay $T$ with definite time
■ when operating on phase-to-neutral voltage, it indicates the faulty phase in the alarm associated with the fault.
Whether it operates on phase-to-neutral or phase-to-phase voltage depends on the connection chosen for the voltage inputs.

It can be used for monitoring unbalance in the capacitor banks on each of the phases, when they are fitted with VTs, using the additional channels in the B83 application.

Block diagram


Connection conditions

| Type of <br> connection | V1, V2, V3 ${ }^{(1)}$ | U21, U32 <br> + V0 | U21, <br> U32 | U21 (1) | V1 (1) |
| :--- | :--- | :--- | :--- | :--- | :--- |
| Phase-to-neutral <br> operation | YES | YES | NO | NO | On V1 only |
| Phase-to-phase <br> operation | YES | YES | YES | On U21 <br> only | NO |

(1) With or without VO.

## Characteristics

| Settings |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Measurement origin |  |  |  |  |
| Setting range | Main channels (U) / Additional channels (U') |  |  |  |
| Voltage mode |  |  |  |  |
| Setting range | Phase-to-phase voltage / Phase-to-neutral voltage |  |  |  |
| Us (or Vs) set point |  |  |  |  |
| Setting range | $50 \%$ to $150 \%$ of Unp (or Vnp) if Uns < 208 V |  |  |  |
|  | $50 \%$ to $135 \%$ of Unp (or Vnp) if Uns $\geqslant 208 \mathrm{~V}$ |  |  |  |
| Accuracy ${ }^{(1)}$ | $\pm 2$ \% |  |  |  |
| Resolution | 1 \% |  |  |  |
| Drop out/pick up ratio | $97 \% \pm 1$ \% |  |  |  |
| U's (or V's) set point for additional channels of the B83 application |  |  |  |  |
| Setting range | 1.5 \% to $150 \%$ of Unp (or Vnp) if Uns < 208 V |  |  |  |
|  | 1.5 \% to $135 \%$ of Unp (or Vnp) if Uns $\geqslant 208 \mathrm{~V}$ |  |  |  |
|  | minimum setting $=1.5 \mathrm{~V}$ |  |  |  |
| Accuracy ${ }^{(1)}$ | $2 \%$ or 0.002 Unp , |  |  |  |
| Resolution | 0.2 \% between 1.5 \% and 9.9 \% Unp (Vnp) |  |  |  |
|  | 0.5 \% if Unp (Vnp) > 10 \% |  |  |  |
| Drop-out/pick-up ratio |  |  |  |  |
| Setting range | 97 \% to 99 \% |  |  |  |
| Accuracy | $1 \%$ or > (1-0,002 U'np / V's) x $100 \%$ |  |  |  |
| Resolution | 0,1 \% |  |  |  |
| Time delay ${ }^{\text {T }}$ |  |  |  |  |
| Setting range | 50 ms to 300 s |  |  |  |
| Accuracy ${ }^{(1)}$ | $\pm 2 \%$ or $\pm 25 \mathrm{~ms}$ |  |  |  |
| Resolution | 10 ms or 1 digit |  |  |  |
| Characteristic times |  |  |  |  |
| Operation time | Pick-up < 40 ms from 0.9 Us (Vs) to 1.1 Us (Vs) (typically 25 ms ) |  |  |  |
| Overshoot time | $<40 \mathrm{~ms}$ from 0.9 Us (Vs) to 1.1 Us (Vs) |  |  |  |
| Reset time | $<50 \mathrm{~ms}$ from 1.1 Us (Vs) to 0.9 Us (Vs) |  |  |  |
| Inputs |  |  |  |  |
| Designation | Syntax | Equations | Logipam |  |
| Protection reset | P59_x_101 | $\square$ | $\square$ |  |
| Protection inhibition | P59_x_113 | $\square$ | ■ |  |
| Outputs |  |  |  |  |
| Designation | Syntax | Equations | Logipam | Matrix |
| Instantaneous output (pick-up) | P59_x_1 | ■ | - |  |
| Delayed output | P59_x_3 | $\square$ | $\square$ | - |
| Fault phase $1^{(2)}$ | P59_x_7 | $\square$ | $\square$ |  |
| Fault phase $2^{(2)}$ | P59_x_8 | $\square$ | - |  |
| Fault phase $3^{(2)}$ | P59_x_9 | - | $\square$ |  |
| Protection inhibited | P59_x_16 | - | $\square$ |  |
| Instantaneous output V1 or U21 | P59_x_23 | - | $\square$ |  |
| Instantaneous output V2 or U32 | P59_x_24 | $\square$ | $\square$ |  |
| Instantaneous output V3 or U13 | P59_x_25 | $\square$ | $\square$ |  |
| Delayed output V1 or U21 | P59_x_26 | $\square$ | - |  |
| Delayed output V2 or U32 | P59_x_27 | $\square$ | $\square$ |  |
| Delayed output V3 or U13 | P59_x_28 | ■ | - |  |
| $\bar{x}$ : unit number. <br> (1) Under reference conditions <br> (2)When the protection function | 55-6). <br> for phase-to-n | utral voltage |  |  |

## Description

Protection against insulation faults by measuring the residual voltage V0 or the neutral point voltage Vnt for generators and motors.
The residual voltage is obtained by the vector sum of the phase voltages or by measurements using delta connected VTs.
The neutral point voltage is measured by a VT inserted in the neutral point of the generator or the motor.
The protection function includes a time delay T , either definite or IDMT (dependent on the residual voltage V 0 ) (see tripping curve equation on page 226).
It operates only when a residual or neutral point voltage is available, by connecting V1V2V3, V0 or Vnt.

## Block diagram

## Characteristics

| Settings |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Measurement origin |  |  |  |  |
| Setting range | Main channels (VO) <br> Additional channels (V'0) <br> Neutral-point voltage (Vnt) |  |  |  |
| Tripping curve |  |  |  |  |
| Setting range | Definite time <br> IDMT (dependent on the residual voltage V0) |  |  |  |
| Vs0 set point |  |  |  |  |
| Definite time setting range | 2 \% Unp to 80 \% Unp (for residual voltage V0) <br> 2 \% Vntp to 80 \% Vntp (for neutral point voltage Vnt) |  |  |  |
| IDMT setting range | $2 \%$ Unp to 10 \% Unp (for residual voltage V0) <br> 2 \% Vntp to 10 \% Vntp (for neutral point voltage Vnt) |  |  |  |
| Accuracy ${ }^{(1)}$ | $\pm 2$ \% or 0.005 Unp |  |  |  |
| Resolution | 1 \% |  |  |  |
| Drop out/pick up ratio | $97 \% \pm 2 \%$ or > (1-0.006 Unp/Vs0) $\times 100 \%$ |  |  |  |
| Time delay $\mathbf{T}$ (tripping time at 2 Vs 0 ) |  |  |  |  |
| Definite time setting range | 50 ms to 300 s |  |  |  |
| IDMT setting range | 100 ms to 10 s |  |  |  |
| Accuracy ${ }^{(1)}$ | $\pm 5 \%$ or $\pm 25 \mathrm{~ms}$ |  |  |  |
| Resolution | 10 ms or 1 digit |  |  |  |
| Characteristic times |  |  |  |  |
| Operation time | pick-up < 45 ms (typically 25 ms ) at 2 Vs 0 |  |  |  |
| Overshoot time | $<40 \mathrm{~ms}$ at 2 Vs 0 |  |  |  |
| Reset time | $<40 \mathrm{~ms}$ at 2 Vs 0 |  |  |  |
| Inputs |  |  |  |  |
| Designation | Syntax | Equations | Logipam |  |
| Protection reset | P59N_x_101 | - | ■ |  |
| Protection inhibition | P59N_x_113 | - | $\square$ |  |
| Outputs |  |  |  |  |
| Designation | Syntax | Equations | Logipam | Matrix |
| Instantaneous output (pick-up) | P59N_x_1 | ■ | ■ |  |
| Delayed output | P59N_x_3 | $\square$ | - | - |
| Protection inhibited | P59N_x_16 | $\square$ | $\square$ |  |

x: unit number.
(1) Under reference conditions (IEC 60255-6).


## Description

The 64G protection function is made of the two independent functions.

- protection function 64G1 which commonly corresponds to a neutral voltage displacement function at the fundamental frequency (ANSI code 59N). It may be implemented by an earth fault protection function (ANSI code 51 N ) when the earth fault current is sufficient.
■ protection function 64G2 which corresponds to a third harmonic undervoltage function (ANSI code 27TN) whose operating principle depends on the type of connection of the generator terminal VTs.
When a single-phase fault occurs, the flow of the zero sequence current increases the potential of the neutral point, detected by protection function 59N. However, given the natural unbalance of the three network phases, the sensitivity set point for 59 N cannot be set under $10 \%$ to $15 \%$ of the phase-to-neutral voltage.
If the single-phase fault occurs on a stator winding near the neutral point, the increase in the potential at the neutral point may be insufficient to trip protection function 59N.
The combination of functions 59 N and 27 TN is the means to protect $100 \%$ of the stator winding. Depending on the settings:
- protection function 59 N protects 85 to $95 \%$ of the stator winding on the terminal side and
■ protection function 27 TN protects 10 to $20 \%$ of the stator winding on the neutral point side.
To create a $100 \%$ stator earth fault protection function, it is necessary to implement the 64G1 ( 59 N or 51 N ) and the 64G2 (27TN) protection functions (see each of these functions for more information).

Protection of three-phase windings against phase-to-earth faults.



## Description

The restricted earth fault protection function detects phase-to-earth faults on threephase windings with earthed neutral. This function protects generators and transformers.
The protected zone is between the 3 phases CTs I1, I2, I3 (or I'1, l'2, I'3) and the neutral point current measurement IO (or l'0).
The vector associated with the current sensors determines the conventional direction of connection.


## Principle

Protection is activated if the following 3 conditions are met:

- IdO $>$ Is 0
- Id $0>1.2 \times$ Istab
- $\Delta I 0>\min (150 / 4,10 \mathrm{~min})$

With:

- Id0: differential residual current
- Is0: adjustable trip set point of the protection function
- Istab: stabilization current
- $\Delta \mathrm{I} 0$ : variation of the neutral point current
- IOmin: nominal current of the neutral point:
- IOmin $=0.05 x \operatorname{In} 0$ si $\operatorname{In} 0>20 \mathrm{~A}$
- $10 \mathrm{~min}=0.10 \times \ln 0$ si $\ln 0 \leq 20 \mathrm{~A}$

Differential residual current Id0
$\operatorname{IdO}=|\overrightarrow{\mathbf{1 0} \Sigma}-\overrightarrow{\mathbf{I O}}|$
With:

- $\overrightarrow{\mathbf{1 0}}$ : neutral point current
- $\overrightarrow{\mathbf{1 0}} \Sigma$ : residuel current calculated using the sum of the 3 phase currents


## Stabilization current Istab

$\operatorname{Istab}(\mathbf{k})=\max (\operatorname{It}(\mathbf{k}), \alpha \cdot \operatorname{Istab}(\mathbf{k}-\mathbf{1}))$
With:

- k: present moment
- k-1: previous moment in the 64REF protective processing cycle
- $\alpha$ : time constant adaptation coefficient of the time memory to cover dips in the through current It, when the CTs are saturated, on an external multi-phase fault
■ It: through current


## Through current It

The through current It provides the protection with discrimination and rendered immunity in relation to external multi-phase faults.
$\mathbf{I t}=\boldsymbol{\operatorname { m a x }}(\mathbf{I R O}, \beta \cdot \mathbf{I R 1})$
With:
■IRO $=|\overrightarrow{\mathbf{1 0}} \Sigma+\overrightarrow{\mathbf{1 0}}| /$ 2: residual component sensitive to single-phase faults
■ IR1 = |Id $|-|\mathbf{I I}|$ : component sensitive to multi-phase faults

- $\beta$ : coefficient depending on the nature of the external fault:
$\square \beta=\boldsymbol{\operatorname { m a x }}(\mathbf{2},|\mathbf{I d}| / \mathbf{l b})$ for two-phase/earth or three-phase/earth faults
- $\beta=0$ for single-phase faults


## Variation of the neutral point current $\Delta I 0$

The neutral point current variation is the difference in the absolute value between the neutral point current before and after the fault has been detected.

## Restricted earth fault differential ANSI code 64REF



## Additional protection on multi-phase faults

When multi-phase/internal earth faults occur, the 64REF protection may experience downgraded operation. The table below defines the usual additional protection for protecting the installation in the event of multi-phase/internal earth faults.


## Dimensioning current sensors

■ The primary current of the neutral point current transformer must comply with the following rule:
$\ln 0 \geqslant 0.1 \times \mathbf{I} \mathbf{1 P}$, where I1p is the phase-to-earth short-circuit current.

- Neutral current transformer must be:
- type 5P20 with an accuracy burden VAct $\geqslant$ Rw.in0 ${ }^{2}$
- or defined by a knee-point voltage $\mathrm{Vk} \geqslant(\mathrm{Rct}+\mathrm{Rw})$.20.in0.

■ Phase current transformers must be:

- type 5P, with an accuracy-limit factor FLP $\geqslant \max \left(20,1.6 \frac{\mathrm{I} 3 \mathrm{P}}{\mathrm{In}}, 2.4 \frac{\mathrm{I} 1 \mathrm{P}}{\mathrm{In}}\right.$ and an accuracy burden VAct $\geqslant$ Rw.in ${ }^{2}$
$\square$ or defined by a knee-point voltage $\mathrm{Vk} \geqslant(\mathrm{RcT}+\mathrm{Rw}) \max \left(\mathbf{2 0}, \mathbf{1 . 6} \frac{\mathrm{I} 3 \mathrm{P}}{\mathrm{In}}, \mathbf{2 . 4} \frac{\mathrm{I} \frac{\mathrm{P}}{\mathrm{In}} \mathrm{in}}{}\right.$.
- Formula legend:
in: phase CT rated secondary current
in0: neutral point CT rated secondary current
Rct: phase CT or neutral CT internal resistance
Rw: resistance of the CT load and wiring
In: phase CT rated primary current
In0: neutral point CT rated primary current
I3P: three-phase short-circuit current
I1P: phase-to-earth short-circuit current
Characteristics

| Settings |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Measurement origin |  |  |  |  |
| Setting range | Main channels (I, IO) <br> Additional channels (l', l'0) |  |  |  |
| Is0 |  |  |  |  |
| Setting range | 0.05 In to 0.8 In for $\mathrm{In} \geqslant 20 \mathrm{~A}$ <br> 0.1 In to 0.8 In for $\mathrm{In}<20 \mathrm{~A}$ |  |  |  |
| Accuracy ${ }^{(1)}$ | 5 \% |  |  |  |
| Resolution | 1 A or 1 digit |  |  |  |
| Drop out/pick up ratio | $93 \% \pm 2$ \% |  |  |  |
| Characteristic times |  |  |  |  |
| Operation time | $<55 \mathrm{~ms}$ at Id0 $=2.4 \mathrm{Istab}$ |  |  |  |
| Overshoot time | $<35 \mathrm{~ms}$ at Id0 $=2.4 \mathrm{Istab}$ |  |  |  |
| Reset time | $<45 \mathrm{~ms}$ at Id0 $=2.4 \mathrm{Istab}$ |  |  |  |
| Inputs |  |  |  |  |
| Designation | Syntax | Equations | Logipam |  |
| Protection reset | P64REF_x_101 | - | ■ |  |
| Protection inhibition | P64REF_x_113 | $\square$ | - |  |
| Outputs |  |  |  |  |
| Designation | Syntax | Equations | Logipam | Matrix |
| Protection output | P64REF_x_3 | $\square$ | $\square$ | $\square$ |
| Protection inhibited | P64REF_x_16 | $\square$ | $\square$ |  |

(1) Under reference conditions (IEC 60255-6).

## Protection functions

## Starts per hour ANSI code 66

Protection of motors against mechanical stress caused by starts that are too close together.

## Operation

The number of starts is incremented if:

- The current taken exceeds $5 \%$ of the current lb after circuit breaker closing (and
the circuit breaker position is hard-wired on inputs I101 and I102).
- The current taken exceeds $5 \%$ of the current lb after re-acceleration.

The number of starts over the period Tcons is limited by:

- the permitted number of consecutive cold starts (Nc)
- the permitted number of successive hot starts (Nh).

The "stop/start" time delay is used to impose a minimum stopping time between each start.

The motor "hot state" data item is determined by the 49RMS motor thermal overload protection. A "hot state" set point can also be configured using this protection function (see page 140).

Note: When the 49RMS generic thermal overload protection is used, if ESO is different from $0 \%$, the ANSI 66 protection function may not work properly
As the "hot state" set point is fixed at $50 \%$ in the ANSI 66 protection function, according
to ESO setting value, the cold state for the 66 protection function may be reduced or not exist. So the number of starts will be limited by the number of consecutive hot starts, with no impact of number of consecutive cold starts setting.
When the motor curves imply to use ESO setting to move the "cold curve", it is highly adviced to use the thermal model based on two time constants, that avoid this setting difficulty.

Block diagram


## Operating information

The following information is available to the operator:

- the number of starts before inhibition
- start inhibit time
(See machine operation help functions on page 58).


## Characteristics

## Settings

| Delay between consecutive starts (Tcons) |
| :--- |
| Setting range <br> Resolution 1 mn to 90 mn |

Resolution
Permitted number of consecutive cold starts ( Nc )
Setting range 1 to 5
Resolution 1

Permitted number of consecutive hot starts (Nh)

| Setting range | 1 to (Nc-1) |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Resolution | 1 |  |  |  |
| Delay between stop/start |  |  |  |  |
| Setting range | 0 to 90 mn (0 no time delay) |  |  |  |
| Resolution | 1 mn |  |  |  |
| Inputs |  |  |  |  |
| Designation | Syntax | Equations | Logipam |  |
| Reset protection | P66_1_101 | ■ | $\square$ |  |
| Motor re-acceleration | P66_1_102 | $\square$ | $\square$ |  |
| Inhibit protection | P66_1_113 | ■ | ■ |  |
| Outputs |  |  |  |  |
| Designation | Syntax | Equations | Logipam | Matrix |
| Protection output | P66_1_3 | ■ | $\square$ | $\square$ |
| Protection inhibited | P66_1_16 | $\square$ | $\square$ |  |
| Stop/start inhibit | P66_1_29 | $\square$ | $\square$ |  |
| Startup total reached | P66_1_30 | $\square$ | $\square$ |  |
| Consecutive startups reached | P66_1_31 | $\square$ | $\square$ |  |

## Help with parameter setting

## Number of consecutive starts

Motor manufacturers state the permitted number of consecutive cold (Nc) and hot ( Nh ) starts in the technical data.

## Delay between consecutive starts

Consecutive starts are starts that are sufficiently close in relation to the rotor cooling time constant.
The delay between consecutive starts (Tcons) must be set to the value of the rotor cooling time constant:
$\tau=(T c-T h) \cdot$ LRT $/ \mathrm{gn}$
Where:
Tc: locked cold rotor limit time in seconds
Th: locked hot rotor limit time in seconds
LRT: locked rotor torque in pu
gn: rated slip in pu

## Motor hot state set point

The motor thermal capacity used varies from 0 to Itrip ${ }^{2}$ (Itrip being the motor thermal overload protection tripping current).
In order to be able to perform a hot start without tripping the thermal overload protection, the motor hot state set point must be configured.
There are 2 different scenarios:

- The motor starting time (tstg) is close to the locked hot rotor limit time (Th).

This scenario corresponds to a motor on which the load's moment of inertia is high, such as a fan. The hot state set point is configured as follows:

$$
\text { Shot }<\text { Itrip }^{2}-\frac{\text { tstg }}{\text { Th }}
$$

$\square$ The motor starting time (tstg) is short compared to the locked hot rotor limit time (Th). The hot state set point is configured as follows:

$$
\text { Nc } \cdot\left(\frac{\operatorname{tstg}^{T c}}{\mathrm{Tc}}\right)<\text { Shot }_{\text {Strip }}{ }^{2}-\left(\text { Nh } \cdot \frac{\text { tstg }}{\text { Th }}\right)
$$

In this scenario, the ANSI 66 protection function is fully involved in limiting the number of starts, because the thermal protection is well below its tripping current set point (Itrip).

## Example 1: 2350 kW / 6 kV motor

## Manufacturer data:

| Locked cold rotor limit time | Tc | 13 s |
| :--- | :--- | :--- |
| Locked hot rotor limit time | Th | 9 s |
| Number of consecutive cold starts | Nc | 3 |
| Number of consecutive hot starts | Nh | 2 |
| Starting time | tstg | 4 s |
| Rated speed | N | 2980 rpm |
| Locked rotor torque | LRT | 0.7 pu |
| Locked rotor current | II | 6 pu |
| Continuous permissible current | Itrip | 1.2 pu |

## Calculating the rotor time constant

The rated slip is given by:
$g_{n}=1-\frac{N \cdot n p}{60 \cdot f n}$
Where:
np : number of poles
fn: network frequency
The number of poles is given by:
$\mathrm{np}=\operatorname{int}\left(\frac{\mathbf{6 0 \cdot \mathbf { f n }}}{\mathrm{N}}\right)$
hence $n p=\operatorname{int}(60.50 / 2980)=1$
Therefore:
$\mathbf{g}_{\mathrm{n}}=1-\frac{2980}{60 \cdot 50}=0,0067$
The rotor constant is given by:
$\tau=(T c-T h)$. LRT / gn
Hence:
$\tau=(13-9) \cdot 0.7 / 0.0067=420 \mathrm{~s}$, or 7 mn
Calculating the hot state set point
The hot state set point is given by:
Nc $\cdot\left(\frac{\text { tdem }^{T}}{\text { Tc }}\right)<$ Schaud $^{2}<$ Itrip $^{2}-\left(\mathrm{Nh} \cdot \frac{\text { tdem }}{\mathrm{Th}}\right)$

Hence:
$3 \cdot\left(\frac{4}{13}\right)<$ Schaud $^{2}<1,2^{2}-\left(2 \cdot \frac{4}{9}\right)$

Or $0.92 \mathrm{lb}<$ Shot $^{2}<0.56 \mathrm{lb}$ which is impossible.
Therefore a more restrictive hot state set point is selected, allowing 1 hot start and 3 cold starts.
Hence:
$3 \cdot\left(\frac{4}{13}\right)<$ Schaud $^{2}<1,2^{2}-\left(1 \cdot \frac{4}{9}\right)$

Or 92.30\% < Shot $^{2}$ < 99.55 \%
Or for the "hot state" set point: $0.96 \mathrm{lb}<$ Shot $<0.99 \mathrm{lb}$

| Example 2: $\mathbf{5 0 6} \mathbf{~ k W} / \mathbf{1 0} \mathbf{~ k V}$ motor <br> Manufacturer data: |  |
| :--- | :--- | :--- |
| Locked cold rotor limit time Tc 60 s <br> Locked hot rotor limit time Th 29 s <br> Number of consecutive cold starts Nc 2 <br> Number of consecutive hot starts Nh 1 <br> Starting time tstg 21 s <br> Rated speed N 993 rpm <br> Locked rotor torque LRT 0.6 pu <br> Locked rotor current II 5.3 pu <br> Continuous permissible current ltrip 1.25 pu $\mathbf{l}$ |  |

## Calculating the rotor time constant

The number of poles equals:
$\mathrm{np}=\operatorname{int}(60.50 / 993)=3$
We can therefore deduce the rated slip:
$g_{n}=1-\frac{993 \cdot 3}{60 \cdot 50}=0,007$
and the rotor cooling constant:
$\tau=(60-29) .0 .6 / 0.007=2657 \mathrm{~s}$, or 44 mn
Calculating the hot state set point
The hot state set point is given by:

$$
2 \cdot\left(\frac{21}{60}\right)<\text { Schaud }^{2}<1,25^{2}-\left(1 \cdot \frac{21}{29}\right)
$$

Or 70 \% < Shot $^{2}<83.83$ \%
Or for the "hot state" set point: $0.83 \mathrm{lb}<$ Shot $<0.91 \mathrm{lb}$
This setting allows 1 hot start and 3 cold starts.

## Protection functions

Directional phase overcurrent ANSI code 67

Phase-to-phase short-circuit protection, with selective tripping according to fault current direction.

## Description

This function comprises a phase overcurrent function associated with direction detection and picks up if the phase overcurrent function in the chosen direction (line or busbar) is activated for at least one of the 3 phases (or two of the three phases, depending on the settings). - the protection function is three-phase and has a definite or IDMT time delay.

- each of the two units has two groups of settings. Switching to setting group A or B can be carried out by a logic input or a remote control order, depending on the settings.
- the customized curve, defined point by point, may be used with this protection function.
- an adjustable timer hold, definite time or IDMT, can be used for coordination with electromagnetic relays and to detect restriking faults.
■ the alarm linked to the protection function indicates the faulty phase or phases.


## Tripping direction

The direction of the current is determined according to the measurement of the phase in relation to a polarization value. It is qualified as busbar direction or line direction according to the following convention:


The tripping zone is set for tripping in busbar zone or tripping in line zone.
The reverse zone is the zone for which the protection function does not trip. The detection of current in the reverse zone is used for indication.

## Polarization value

The polarization value is the phase-to-phase value in quadrature with the current for $\cos \theta=1\left(90^{\circ}\right.$ connection angle). A phase current vector plane is divided into two half-planes that correspond to the line zone and busbar zone. The characteristic angle $\theta$ is the angle of the perpendicular to the boundary line between the 2 zones and the polarization value.

## Voltage memory

Should all the voltages disappear during a 3-phase fault near the busbars, the voltage level may be insufficient for the fault direction to be detected (<1.5 \% Unp). The protection function therefore uses a voltage memory to reliably determine the direction. The fault direction is saved as long as the voltage level is too low and the current is above the Is set point.

## Closing on a pre-existing fault

If the circuit breaker is closed when there is a preexisting 3 -phase fault on the busbars, the voltage memory is blank. As a result, the direction cannot be determined and the protection does not trip. In such cases, a backup 50/51 protection function should be used.


Fault tripping in line zone with $\theta=30^{\circ}$


Fault tripping in line zone with $\theta=45^{\circ}$.


Fault tripping in line zone with $\theta=60^{\circ}$.

## Tripping logic

In certain cases, it is wise to select the "two out of three phases" tripping logic. Such cases may occur when two parallel transformers (Dy) must be protected. For a 2phase fault on a transformer primary winding, there is a 2-1-1 current distribution at the secondary end. The highest current is in the expected zone (operation zone for the faulty incomer, no operation zone for the fault-free incomer).
One of the lowest currents is at the edge of the zone. According to the line parameters, it may even be in the wrong zone.
There is therefore a risk of tripping both incomers.

Block diagram


Grouping of output data.

(1) one out of three
(2) two out of three

## Protection functions

Directional phase overcurrent ANSI code 67
x: unit number
(1) Under reference conditions (IEC 60255-6)
(2) Setting ranges in TMS (Time Multiplier Setting) mode Inverse (SIT) and IEC SIT/A: 0.04 to 4.20 Very inverse (VIT) and IEC VIT/B: 0.07 to 8.33 Very inverse (LTI) and IEC LTI/B: 0.01 to 0.93 Ext. inverse (EIT) and IEC EIT/C: 0.13 to 15.47 IEEE moderately inverse: 0.42 to 51.86 IEEE very inverse: 0.73 to 90.57
IEEE extremely inverse: 1.24 to 154.32
IAC inverse: 0.34 to 42.08 IAC very inverse: 0.61 to 75.75
IAC extremely inverse: 1.08 to 134.4 .
(3) Only for standardized tripping curves of the IEC, IEEE and IAC types.

| Tripping curve | Timer hold |
| :--- | :--- |
| Definite time (DT) | Definite time |
| Standard inverse time (SIT) | Definite time |
| Very inverse time (VIT or LTI) | Definite time |
| Extremely inverse time (EIT) | Definite time |
| Ultra inverse time (UIT) | Definite time |
| RI curve | Definite time |
| IEC inverse time SIT / A | Definite time or IDMT |
| IEC very inverse time VIT or LTI / B | Definite time or IDMT |
| IEC extremely inverse time EIT / C | Definite time or IDMT |
| IEEE moderately inverse (IEC / D) | Definite time or IDMT |
| IEEE very inverse (IEC / E) | Definite time or IDMT |
| IEEE extremely inverse (IEC / F) | Definite time or IDMT |
| IAC inverse | Definite time or IDMT |
| IAC very inverse | Definite time or IDMT |
| IAC extremely inverse | Definite time or IDMT |
| Customized | Definite time |

## Characteristics

## Settings

| Characteristic angle $\theta$ |  |  |
| :---: | :---: | :---: |
| Setting range |  | $30^{\circ}, 45^{\circ}, 60^{\circ}$ |
| Accuracy ${ }^{(1)}$ |  | $\pm 2$ \% |
| Tripping curve |  |  |
| Setting range |  | See list above |
| Is set point |  |  |
| Setting range | definite time | $0.1 \mathrm{ln} \leqslant \mathrm{Is} \leqslant 24 \mathrm{ln}$ in amperes |
|  | IDMT | $0.1 \mathrm{ln} \leqslant \mathrm{Is} \leqslant 2.4 \mathrm{ln}$ in amperes |
| Accuracy ${ }^{(1)}$ |  | $\pm 5 \%$ or $\pm 0.01 \mathrm{ln}$ |
| Resolution |  | 1 A or 1 digit |
| Drop out/pick up ratio |  | $93.5 \% \pm 5 \%$ or > (1-0.015 In/ls) $\times 100 \%$ |
| Time delay T (operation time at 10 ls ) |  |  |
| Setting range | definite time | Inst, $50 \mathrm{~ms} \leqslant \mathrm{~T} \leqslant 300 \mathrm{~s}$ |
|  | IDMT | $100 \mathrm{~ms} \leqslant \mathrm{~T} \leqslant 12.5 \mathrm{~s}$ or TMS ${ }^{(2)}$ |
| Accuracy ${ }^{(1)}$ <br> For $\mathrm{T} \geqslant 100 \mathrm{~ms}$ | definite time ${ }^{(4)}$ | $\pm 2 \%$ or from -10 ms to +25 ms |
|  | IDMT | Class 5 or from -10 ms to +25 ms |
| Resolution |  | 10 ms or 1 digit |


| Advanced settings |  |
| :--- | :--- |
| Tripping direction | Busbar / line |
| Setting range |  |
| Tripping logic | One out of three / two out of three |
| Setting range <br> Timer hold T1 | $0 ; 0.05$ to 300 s |
| Setting range | definite time |
| IDMT $^{(3)}$ | 0.5 to 20 s |
| Resolution | 10 ms or 1 digit |
| Characteristic times |  |


| Operation time |  | pick-up $<75 \mathrm{~ms}$ at 2 Is (typically 65 ms ) Inst. < 90 ms at 2 Is (confirmed instantaneous) (typically 75 ms ) |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Overshoot time |  | $<45 \mathrm{~ms}$ at 2 ls |  |  |
| Reset time |  | $<55 \mathrm{~ms}$ at 2 Is (for T1 = 0) |  |  |
| Inputs |  |  |  |  |
| Designation | Syntax | Equations | Logipam |  |
| Protection reset | P67_x_101 | ■ | - |  |
| Protection inhibition | P67_x_113 | $\square$ | - |  |
| Outputs |  |  |  |  |
| Designation | Syntax | Equations | Logipam | Matrix |
| Instantaneous output (pick-up) | P67_x_1 | ■ | - |  |
| Delayed output | P67_x_3 | $\square$ | - | ■ |
| Drop out | P67_x_4 | $\square$ | $\square$ |  |
| Instantaneous output (reverse zone) | P67_x_6 | $\square$ | ■ |  |
| Phase 1 fault | P67_x_7 | $\square$ | - |  |
| Phase 2 fault | P67_x_8 | $\square$ | $\square$ |  |
| Phase 3 fault | P67_x_9 | $\square$ | - |  |
| Protection inhibited | P67_x_16 | $\square$ | - |  |
| Instantaneous output at 0.8 Is | P67_x_21 | $\square$ | - |  |
| 1 out of 3 delayed output | P67_x_36 | $\square$ | $\square$ |  |
| 2 out of 3 delayed output | P67_x_37 | $\square$ | $\square$ |  |

Earth fault protection, with selective tripping according to fault current direction.

## Description

To adapt to all types of applications and all earthing systems, the protection function operates according to two different types of characteristics, i.e. a choice of: - type 1: the protection function uses 10 vector projection.

This projection method is suitable for radial feeders in resistive, isolated or compensated neutral systems.

- type 2: the protection function uses the 10 vector magnitude and operates like an earth fault protection function with an added direction criterion.
This projection method is suitable for closed ring distribution networks with directly earthed neutral.
■ type 3: the protection function uses the 10 vector magnitude and complies with Italian specification ENEL DK5600. It operates like an earth fault protection function with an added angular direction criterion \{Lim.1, Lim.2\}.
This protection method is suitable for distribution networks in which the neutral earthing system varies according to the operational mode.


## Tripping direction

The direction of the residual current is qualified as busbar direction or line direction according to the following convention:


The tripping zone is set for tripping in busbar zone or tripping in line zone. The reverse zone is the zone for which the protection function does not trip. The detection of current in the reverse zone is used for indication.

## Protection functions

Directional earth fault - Type 1 ANSI code 67N/67NC

Earth fault protection for impedant or compensated neutral systems.


Tripping characteristic of ANSI 67N/67NC type 1 protection (characteristic angle $\theta 0 \neq 0^{\circ}$ ).


Tripping characteristic of ANSI 67N/67NC type 1 protection (characteristic angle $\theta 0=0^{\circ}$ ).

## Description

The function determines the projection of the residual current IO on the characteristic line, the position of which is determined by the setting of characteristic angle $\theta 0$ in relation to the residual voltage. The projection value is compared to the Is0 set point. This protection function is suitable for radial feeders in resistive, isolated or compensated neutral systems.
With compensated neutral systems, it is characterized by its capacity to detect very brief, repetitive faults (recurrent faults). In the case of Petersen coils with no additional resistance, fault detection under steady state conditions is not possible due to the absence of active zero sequence current. The protection function uses the transient current at the beginning of the fault to ensure tripping.
The $\theta 0=0^{\circ}$ setting is suitable for compensated or impedant neutral systems. When this setting is selected, the parameter setting of the sector is used to reduce the protection tripping zone to ensure its stability on fault-free feeders.
The protection function operates with the residual current measured at one of the relay 10 inputs (operation with sum of three currents impossible). The protection function is inhibited for residual voltages below the Vs0 set point. It implements a definite time (DT) delay.
The tripping direction may be set at the busbar end or line end.
Each of the two units has two groups of settings. Switching to setting group A or B can be carried out by a logic input or a remote control order, depending on the settings.

## Memory

The detection of recurrent faults is controlled by the time delay TOmem which extends the transient pick-up information, thereby enabling the operation of the definite time delay even with faults that are rapidly extinguished ( $\approx 2 \mathrm{~ms}$ ) and restrike periodically. Even when a Petersen coil with no additional resistance is used, tripping is ensured due to fault detection during the transient fault appearance. Detection is extended throughout the duration of the fault based on the criterion $\mathrm{V} 0 \geqslant \mathrm{~V} 0 \mathrm{mem}$, within the limit of TOmem. With this type of application, TOmem must be greater than T (definite time delay).

## Block diagram



| Characteristics |  |  |
| :---: | :---: | :---: |
| Settings |  |  |
| Measurement origin |  |  |
| Setting range |  | 10 / l'0 |
| Characteristic angle $\theta$ |  |  |
| Setting range |  | $-45^{\circ}, 0^{\circ}, 15^{\circ}, 30^{\circ}, 45^{\circ}, 60^{\circ}, 90^{\circ}$ |
| Accuracy ${ }^{(1)}$ |  | $\pm 2^{\circ}$ |
| Is0 setting |  |  |
| Setting range |  | $0.01 \ln 0 \leqslant 1 \mathrm{~s} 0 \leqslant 15 \ln 0(\mathrm{~min} .0 .1 \mathrm{~A})$ in amperes |
|  | 2 A rating | 0.1 to 30 A |
|  | 20 A rating | 0.2 to 300 A |
|  |  | $0.01 \mathrm{ln} 0 \leqslant \mathrm{ls} 0 \leqslant 15 \ln 0(\mathrm{~min} .0 .1 \mathrm{~A})$ |
|  | ith ACE990 | $0.01 \mathrm{In} 0 \leqslant \mathrm{ls} 0 \leqslant 15 \mathrm{In} 0(\mathrm{~min} .0 .1 \mathrm{~A})$ |
| Accuracy ${ }^{(1)}$ |  | $\pm 5 \%$ (at $\varphi 0=180^{\circ}$ ) |
| Resolution |  | 0.1 A or 1 digit |
| Drop out/pick up ratio |  | 93.5 \% $\pm 5$ \% |
| Time delay T (definite time (DT) tripping curve) |  |  |
| Setting range |  | Inst, $50 \mathrm{~ms} \leqslant \mathrm{~T} \leqslant 300 \mathrm{~s}$ |
| Accuracy ${ }^{(1)}$ |  | $\pm 2 \%$ or from -10 ms to +25 ms |
| Resolution |  | 10 ms or 1 digit |
| Advanced settings |  |  |
| Tripping direction |  |  |
| Setting range |  | Busbar / line |
| Vs0 set point |  |  |
| Setting range |  | 2 \% Unp to 80 \% Unp |
| Accuracy ${ }^{(1)}$ |  | $\pm 5 \%$ or $\pm 0.005$ Unp |
| Resolution |  | 1 \% |
| Drop out/pick up ratio |  | $\begin{aligned} & 93.5 \% \pm 5 \% \\ & \text { or > (1-0.006 Unp/Vs0) } \times 100 \% \end{aligned}$ |
| Sector |  |  |
| Setting range |  | $86^{\circ}, 83^{\circ}, 76^{\circ}$ |
| Accuracy |  | $\pm{ }^{\circ}$ |
| With CT + CSH30 |  | $\pm 3^{\circ}$ |
| Memory time TOmem |  |  |
| Setting range |  | 0; 0.05 to 300 s |
| Resolution |  | 10 ms or 1 digit |
| Memory voltage VOmem |  |  |
| Setting range |  | 0; 2 to $80 \%$ of Unp |
| Resolution |  | 1\% |
| Characteristic times |  |  |
| Operation time |  | Pick-up < 55 ms at 2 Is0 |
| Overshoot time |  | $<45 \mathrm{~ms}$ at 2 ls 0 |
| Reset time |  | $<65 \mathrm{~ms}$ (at TOmem $=0$ ) |
| Inputs |  |  |
| Designation | Syntax | Equations Logipam |
| Protection reset | P67N_x_101 | ■ ! |
| Protection inhibition | P67N_x_113 | ■ ■ |
| Outputs |  |  |
| Designation | Syntax | Equations Logipam Matrix |
| Instantaneous output (pick-up) | P67N_x_1 | ■ ■ |
| Delayed output | P67N_x_3 | ■ ■ ■ |
| Drop-out | P67N_x_4 | $\square \square$ |
| Instantaneous output (reverse zone) | P67N_x_6 | ■ ■ |
| Protection inhibited | P67N_x_16 | ■ |
| Instantaneous output at 0.8 Is0 | P67N_x_21 | $\square \square$ |
| x: unit number. <br> (1) Under reference conditions (IEC 60255-6). |  |  |

## Standard setting

The settings below are given for usual applications in the different earthing systems.
The shaded boxes represent default settings.

|  | Isolated neutral | Impedant neutral | Compensated <br> neutral |
| :--- | :--- | :--- | :--- |
| Is0 set point | Set according to <br> discrimination study | Set according to <br> discrimination study | Set according to <br> discrimination study |
| Characteristic angle $\theta 0$ | $90^{\circ}$ | $0^{\circ}$ | $0^{\circ}$ |
| Time delay T | Set according to <br> discrimination study | Set according to <br> discrimination study | Set according to <br> discrimination study |
| Direction | Line | Line | Line |
| Vs0 set point | $2 \%$ of Uns | $2 \%$ of Uns | $2 \%$ of Uns |
| Sector | N/A | $86^{\circ}$ | $86^{\circ}$ |
| Memory time TOmem | 0 | 0 | 200 ms |
| Memory voltage | 0 | 0 | 0 |
| Vomem |  |  |  |

## Protection functions

## Directional earth fault - Type 2 <br> ANSI code 67N/67NC

Earth fault protection for impedant or solidly earthed systems.


Example of phase 1 to earth fault - Measurement of the 3 phase voltages.


Tripping characteristic of ANSI 67N/67NC - type 2 protection function.

## Description

The protection function operates like an earth fault protection function with an added direction criterion.
It is suitable for closed ring distribution networks with directly earthed neutral. It has all the characteristics of an earth fault protection function (50N/51N) and can therefore be easily coordinated with that function.
The residual current is the current measured at one of the Sepam IO inputs or calculated using the sum of the main phase currents (I), according to the parameter setting.
The tripping direction may be set at the busbar end or line end.
The protection function has a definite or IDMT time delay
Each of the two units has two groups of settings. Switching to setting group A or B can be carried out by a logic input or a remote control order, depending on the settings.
The customized curve, defined point by point, may be used with this protection function.
An adjustable timer hold, definite time or IDMT, can be used for coordination with electromagnetic relays and to detect restriking faults.

| Tripping curve | Timer hold |
| :--- | :--- |
| Definite time (DT) | Definite time |
| Standard inverse time (SIT) | Definite time |
| Very inverse time (VIT or LTI) | Definite time |
| Extremely inverse time (EIT) | Definite time |
| Ultra inverse time (UIT) | Definite time |
| RI curve | Definite time |
| IEC inverse time SIT / A | Definite time or IDMT |
| IEC very inverse time VIT or LTI / B | Definite time or IDMT |
| IEC extremely inverse time EIT / C | Definite time or IDMT |
| IEEE moderately inverse (IEC / D) | Definite time or IDMT |
| IEEE very inverse (IEC / E) | Definite time or IDMT |
| IEEE extremely inverse (IEC / F) | Definite time or IDMT |
| IAC inverse | Definite time or IDMT |
| IAC very inverse | Definite time or IDMT |
| IAC extremely inverse | Definite time or IDMT |
| Customized | Definite time |

## Block diagram



## Characteristics

$x$ : unit number.
(1) Under reference conditions (IEC 60255-6).
(2) Setting ranges in TMS (Time Multiplier Setting) mode Inverse (SIT) and IEC SIT/A: 0.04 to 4.20
Very inverse (VIT) and IEC VIT/B: 0.07 to 8.33 Very inverse (LTI) and IEC LTI/B: 0.01 to 0.93 Ext. inverse (EIT) and IEC EIT/C: 0.13 to 15.47 IEEE moderately inverse: 0.42 to 51.86 IEEE very inverse: 0.73 to 90.57
IEEE extremely inverse: 1.24 to 154.32
IAC inverse: 0.34 to 42.08
IAC very inverse: 0.61 to 75.75
IAC extremely inverse: 1.08 to 134.4 .
(3) Only for standardized tripping curves of the IEC, IEEE and IAC types.

| Settings |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Measurement origin |  |  |  |  |  |
| Setting range |  |  | $\begin{aligned} & 10 \\ & \text { l'0 } \\ & \text { IOE (sum of th } \end{aligned}$ | e main phas | channels) |
| Characteristic angle $\theta$ |  |  |  |  |  |
| Setting range |  |  | $-45^{\circ}, 0^{\circ}, 15^{\circ}, 30^{\circ}, 45^{\circ}, 60^{\circ}, 90^{\circ}$ |  |  |
| Accuracy ${ }^{(1)}$ |  |  | $\pm 2^{\circ}$ |  |  |
| Tripping curve |  |  |  |  |  |
| Setting range |  |  | See previous page |  |  |
| Is0 set point |  |  |  |  |  |
| Definite time setting range |  |  | $0.01 \ln 0 \leqslant \operatorname{ls} 0 \leqslant 15 \ln 0(\min .0 .1 \mathrm{~A})$ in amperes |  |  |
|  | Sum of CTs |  | $0.01 \mathrm{ln} \leqslant \mathrm{ls} 0 \leqslant 15 \ln (\min .0 .1 \mathrm{~A})$ |  |  |
|  | With CSH sensor | 2 A rating | 0.1 to 30 A |  |  |
|  |  | 20 A rating | 0.2 to 300 A |  |  |
|  | CT |  | $0.01 \mathrm{ln} 0 \leqslant 1 \mathrm{~s} 0 \leqslant 15 \mathrm{In} 0(\mathrm{~min} .0 .1 \mathrm{~A})$ |  |  |
|  | Core balance CT with ACE990 |  | $0.01 \mathrm{ln} 0 \leqslant \mathrm{ls} 0 \leqslant 15 \mathrm{In} 0(\mathrm{~min} .0 .1 \mathrm{~A})$ |  |  |
| IDMT setting range |  |  | $0.01 \ln 0 \leqslant \operatorname{ls} 0 \leqslant \ln 0(\operatorname{mini} 0.1 \mathrm{~A})$ in amperes |  |  |
|  | Sum of CTs |  | $0.01 \mathrm{ln} \leqslant \operatorname{ls} 0 \leqslant \ln (\mathrm{~min} .0 .1 \mathrm{~A})$ |  |  |
|  | With CSH sensor | 2 A rating | 0.1 to 2 A |  |  |
|  |  | 20 A rating | 0.2 to 20 A |  |  |
|  | CT |  | $0.01 \mathrm{ln} 0 \leqslant \operatorname{ls} 0 \leqslant \ln 0(\mathrm{~min} .0 .1 \mathrm{~A})$ |  |  |
|  | Core balance CT with ACE990 |  | $0.01 \mathrm{ln} 0 \leqslant \mathrm{Is} 0 \leqslant \ln 0(\mathrm{~min} .0 .1 \mathrm{~A})$ |  |  |
| Accuracy ${ }^{(1)}$ |  |  | $\pm 5 \%$ or $\pm 0.004 \mathrm{ln} 0$ |  |  |
| Resolution |  |  | 0.1 A or 1 digit |  |  |
| Drop out/pick up ratio |  |  | $\begin{aligned} & 93.5 \% \pm 5 \% \\ & \text { or > }>(1-0.005 \ln 0 / \mathrm{ls} 0) \times 100 \% \end{aligned}$ |  |  |
| Time delay $\mathbf{T}$ (operation time at 10 ls 0 ) |  |  |  |  |  |
| Setting range | definite time |  | Inst, $50 \mathrm{~ms} \leqslant \mathrm{~T} \leqslant 300 \mathrm{~s}$ |  |  |
|  | IDMT |  | $100 \mathrm{~ms} \leqslant \mathrm{~T} \leqslant 12.5 \mathrm{~s}$ or TMS ${ }^{(2)}$ |  |  |
| Accuracy ${ }^{(1)}$ | definite time |  | $\pm 2 \%$ or from -10 ms to +25 ms |  |  |
|  | IDMT |  | Class 5 or from -10 ms to +25 ms |  |  |
| Resolution |  |  | 10 ms or 1 digit |  |  |
| Advanced settings |  |  |  |  |  |
| Tripping direction |  |  |  |  |  |
| Setting range |  |  | Busbar / line |  |  |
| Vs0 set point |  |  |  |  |  |
| Setting range |  |  | 2 \% Unp to 80 \% Unp |  |  |
| Accuracy ${ }^{(1)}$ |  |  | $\pm 5 \%$ or $\pm 0.005$ Unp |  |  |
| Resolution |  |  | 1 \% |  |  |
| Drop out/pick up ratio |  |  | $\begin{aligned} & 93 \% \pm 5 \% \\ & \text { or > }>(1-0.006 \text { Unp/Vs0 }) \times 100 \% \end{aligned}$ |  |  |
| Timer hold T1 |  |  |  |  |  |
| Setting range | definite time |  | 0; 0.05 to 300 s |  |  |
|  | IDMT ${ }^{(3)}$ |  | 0.5 to 20 s |  |  |
| Resolution |  |  | 10 ms or 1 digit |  |  |
| Characteristic times |  |  |  |  |  |
| Operation time |  |  | Pick-up < 40 ms at 2 Is0 (typically 25 ms ) Inst. < 55 ms at 2 Is0 (confirmed instantaneous) (typically 35 ms ) |  |  |
| Overshoot time |  |  | $<35 \mathrm{~ms}$ at 2 Is0 |  |  |
| Reset time |  |  | $<50 \mathrm{~ms}$ at 2 Is 0 (for $\mathrm{T} 1=0$ ) |  |  |
| Inputs |  |  |  |  |  |
| Designation |  | Syntax | Equations Logipam |  |  |
| Protection reset |  | P67N_x_101 | ■ | ■ |  |
| Protection inhibition |  | P67N_x_113 | ■ ■ |  |  |
| Outputs |  |  |  |  |  |
| Designation |  | Syntax | Equations | Logipam | Matrix |
| Instantaneous output (pick-up) |  | P67N_x_1 | ■ | $\square$ |  |
| Delayed output |  | P67N_x_3 | - | $\square$ | ■ |
| Drop out |  | P67N_x_4 | $\square$ | $\square$ |  |
| Instantaneous output (reverse zone) |  | P67N_x_6 | $\square$ | - |  |
| Protection inhibited |  | P67N_x_16 | $\square$ | $\square$ |  |
| Instantaneous output at 0.8 Is0 |  | P67N_x_21 | - | - |  |



## Type 3 operation

This protection operates like an earth fault protection function (ANSI 50N/51N) with an added angular direction criterion \{Lim.1, Lim.2\}.
It is suitable for distribution networks in which the neutral earthing system varies according to the operational mode.
The tripping direction may be set at the busbar end or line end.
The residual current is the current measured at the Sepam IO input.
It has a definite time delay (DT constant).
By choosing an Is0 set point of 0, the protection function behaves like a neutral voltage displacement protection function (ANSI 59N).

## Simplified schematic



## Definite time operation

Is0 corresponds to the operating set point expressed in amps, and T corresponds to the protection operating delay.


Definite time protection principle.

## Type 3 characteristics

Measurement origin 10


| Resolution | 0.1 A or 1 digit |  |
| :--- | :--- | :--- |
| Accuracy | $\pm 5 \%$ |  |
| Drop-out/pick-up ratio | $\geqslant 95 \%$ |  |
| Vs0 set point |  |  |
| Setting | On sum of 3 Vs | $2 \%$ Unp $\leqslant$ Vs0 $\leqslant 80 \%$ Unp |
|  | On external VT | $0.6 \%$ Unp $\leqslant$ Vs $0 \leqslant 80 \%$ Unp |
| Resolution |  | $0.1 \%$ for Vs0 $<10 \%$ |
|  |  | $1 \%$ for Vs0 $\geqslant 10 \%$ |
| Accuracy | $\pm 5 \%$ |  |
| Drop-out/pick-up ratio | $\geqslant 95 \%$ |  |

Time delay 7

| Setting | 0 ms |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Resolution | 10 ms or 1 digit |  |  |  |
| Accuracy | $\leqslant 3 \%$ or $\pm 20 \mathrm{~ms}$ at 2 ls0 |  |  |  |
| Characteristic times |  |  |  |  |
| Operation time | pick-up < 40 ms at 2 ls0 |  |  |  |
|  | instantaneous < 55 ms at 2 Is0 |  |  |  |
| Overshoot time | $<40 \mathrm{~ms}$ |  |  |  |
| Reset time | < 50 ms |  |  |  |
| Inputs |  |  |  |  |
| Designation | Syntax | Equations Logipam |  |  |
| Reset protection | P67N_x_101 | 1 ■ ■ |  |  |
| Inhibit protection | P67N_x_113 | 3 ■ ■ |  |  |
| Outputs |  |  |  |  |
| Designation | Syntax | Equations | Logipam | Matrix |
| Instantaneous output (pick-up) | P67N_x_1 | ■ | $\square$ |  |
| Delayed output | P67N_x_3 | $\square$ | - | - |
| Drop-out | P67N_x_4 | $\square$ | $\square$ |  |
| Instantaneous output (reverse zone) | P67N_x_6 | $\square$ | - |  |
| Protection inhibited | P67N_x_16 | - | - |  |
| Instantaneous output at 0.8 Is0 | P67N_x_21 | $\square$ | $\square$ |  |

(1) Tripping zone Lim.2-Lim. 1 should be $10^{\circ}$ or more.
(2) For ISO $=0$, the protection function behaves like a neutral voltage displacement protection function (59N).
(3) $\operatorname{InO}=k$. $n$ where $n=$ the core balance CT ratio and $k=$ coefficient to be determined according to the wiring of the ACE990 $(0.00578 \leqslant k \leqslant 0.04)$.

## Standard tripping zone setting (line end)

The settings below are given for the usual applications in different types of neutral earthing system.
The shaded boxes represent default settings.

|  | Isolated <br> neutral | Impedant <br> neutral | Directly earthed <br> neutral |
| :--- | :--- | :--- | :--- |
| Lim. 1 angle | $190^{\circ}$ | $100^{\circ}$ | $100^{\circ}$ |
| Lim. 2 angle | $350^{\circ}$ | $280^{\circ}$ | $280^{\circ}$ |

Protection of synchronous motors and generators against loss of synchronism.

## Operation

The loss of synchronism in synchronous motors and generators protection function is based on the value of the active power calculated on the stator winding.
The protection function is made up of three independent protection modules, based on:
■ the internal angle calculation

- the equal-area criterion
- power swings.

Tripping is caused either by one of the above principles, or a combination of several of them, depending on the parameters set.
When using the loss of synchronism in synchronous motors protection function, only power swings should be used if the motor load instantaneous variations exceed 10 \% of its rated power.

## Current sensors

Current transformers must be:
■ either type 5P20, with an accuracy burden of VATC > Rfln²
where VATC: CT rated burden
In : secondary rated current of the CT
Rf: wiring resistance
■ or defined by a kneepoint voltage $\mathrm{Vk} \geqslant(\mathrm{RTC}+\mathrm{Rf})$.20.In
where RTC: CT internal resistance.

## Calculating the internal angle

The algorithm is based on calculating variations in the rotor speed and the internal angle by resolving the fundamental equation relating to mechanical movements:
$J \cdot \Omega_{m} \cdot \frac{\mathbf{d} \Omega_{m}}{\mathbf{d t}}=\mathbf{P}_{\mathbf{m}}-\mathbf{P}_{\mathbf{e}}$
$\Omega_{m}=\frac{d \theta_{m}}{d t}=\frac{d \delta}{d t} \times \frac{1}{n p}$
J : total moment of inertia (generator + turbine or motor + load)
תm: rotor speed
Pm: mechanical power (supplied by the turbine or taken by the motor load)
Pe: active electrical power (supplied by the generator or taken by the motor)
$\theta \mathrm{m}$ : mechanical internal angle of the synchronous machine
$\delta$ : electrical internal angle of the synchronous machine.

## Calculating the internal angle

## Protection tripping

The protection trips if the variation in the internal angle is higher than the configured set point for longer than the confirmation delay.
Initializing calculation
Calculation of variations in the rotor speed and the internal angle is initialized in the event of significant network disturbance:
■ Either $\mathrm{Pa}=\mid \mathrm{Pm}-\mathrm{Pel}$ is more than $25 \%$ of the machine's rated power

- Or the positive sequence impedance enters the power swing polygon, defined using the machine transient reactance $\mathrm{Xd}^{\prime}$.


## Stopping calculation

Calculation of variations in the rotor speed and the internal angle is interrupted either when the network returns to stability, or at the end of the first oscillation period of the mechanical movement (similarly to the equal-area criterion).

## Calculating the mechanical power

The mechanical power Pm supplied by the turbine depends on the nature of the turbine and the type of speed governor. It is estimated by using a 2nd order low-pass filter at the mechanical movement's frequency of oscillation.
The mechanical power Pm taken by the motor + load assembly can vary quickly according to the driven mechanical load. Therefore in order to follow the mechanical power as closely as possible, it is estimated by using a 1st order low-pass filter at the mechanical movement's frequency of oscillation.

## Determination of the frequency of oscillation Tosc

The mechanical movement's frequency of oscillation is determined periodically, before appearance of the disturbance, in order to take account of the initial internal angle and initial field voltage.

## Synchronous machine parameters

Xd : synchronous reactance of the d axis (in pu)
Xd' : transient reactance of the d axis (in pu)
Xq : synchronous reactance of the q axis (in pu)
$J$ : mechanical system moment of inertia (in kg.m²)
N : machine synchronous speed (in rpm)
These parameters are defined by the user in the "Particular characteristics" screen in the SFT2841 parameter-setting software.

## Block diagram



## Equal-area criterion

The algorithm is based on calculating the acceleration area on appearance of a fault, then the braking area on disappearance of the fault.

## Protection tripping

The trip order is given if the braking area is less than the acceleration area.
The function calculates in steady state the average over 4 seconds of active power, which corresponds to the mechanical power before the fault, Pad, supplied by the turbine or taken by the motor load.
Comparison of the areas is initialized when the active power differs from the mechanical power by more than $5 \%$.
A time delay can be used to postpone tripping. The protection function is reset if a return to stability is detected during this time delay.

Block diagram


## IPower swings

The algorithm is based on detecting inversion of the active power sign.
A power swing corresponds to 2 consecutive inversions of the active power sign.
The protection trips when the number of power swings equals the configured set point.
A time delay is used to fix a maximum period between 2 power swings, in order to make the protection immune to low-frequency power swings.

Block diagram


## Characteristics

$\left.\begin{array}{llll}\hline \text { Settings } & & \\ \text { Choosing the type of trip } & & \\ \text { Setting range } & \\ & \begin{array}{l}\text { Internal angle calculation } \\ \text { Equal-area criterion } \\ \text { Power swing }\end{array} \\ & \text { Equal-area criterion and power swing }\end{array}\right)$

## Help with parameter setting

Stabilization delay and oscillation period
The stabilization delay corresponds to the time it takes to estimate the mechanical power Pm, after circuit breaker closing.
The mechanical movement's oscillation period Tosc is calculated using the average of 4 values available every 500 ms .
As the mechanical movement's oscillation period is not available for 2 s after circuit breaker closing, the stabilization delay must be configured with a value between 4 and 5 times the mechanical movement's oscillation period defined by the following expression:

Tosc $=2 \pi \cdot \sqrt{\frac{2 H}{K s \cdot \omega}}$
Where:
$\omega$ electrical network pulsation in $\mathrm{rd} / \mathrm{s}$
H: mechanical system inertia constant in seconds:
$H=\frac{J \cdot(\omega / n p)^{2}}{2 \cdot S n}$
Ks: synchronizing coefficient in pu
np : number of pairs of poles
Sn : synchronous machine apparent power in VA

## Synchronizing coefficient

The synchronizing coefficient Ks characterizes the ability of the synchronous machine to resynchronize itself. It depends on the synchronous machine's operating point before the fault appeared in the network. It is defined by the following expression:
$K s=\frac{E q o \cdot V}{X d^{\prime}} \cdot \cos \delta+V^{2} \cdot\left(\frac{1}{X q}-\frac{1}{X d^{\prime}}\right) \cdot \cos 2 \delta$

Eqo: field voltage, in transient state, in pu of Vn
V : voltage at the machine terminals in pu of Vn
$\delta$ : synchronous machine's electrical internal angle in degrees


Vector representation of the machine's internal angle.

## Field voltage

The field voltage in transient state Eqo is determined by the projecting the next vector on the $q$ axis:
$\overrightarrow{\mathbf{E}}^{\prime}=\overrightarrow{\mathbf{V}}+\mathbf{j} \cdot \mathbf{X d} \cdot \overrightarrow{\mathbf{I}}$
The direction of the q axis is defined by the vector:
$\overrightarrow{\mathbf{E O}}=\overrightarrow{\mathrm{V}}+\mathrm{j} \cdot \mathrm{Xq} \cdot \overrightarrow{\mathbf{l}}$

## Example of parameter setting: 44 MVA / 11 kV generator

## Input data

Xd = 1.67
$\mathrm{Xq}=0.88$
Xd' $=0.23$
$H=10$ seconds
The generator operating point is as follows:
$\mathrm{V}=1 \mathrm{pu}$
$\mathrm{I}=0.7 \mathrm{pu}\left(\varphi=-20^{\circ}\right)$
Calculation results
Eqo = 1.017 pu
$\delta=25.55^{\circ}$ (internal angle)
Pad $=0.658$ pu (active power before fault)
$\mathrm{Ks}=2.98$
Tosc $=0.92$ seconds

In this example, the initial internal angle is $25.55^{\circ}$. According to the graph below, we can see that the active power available when stationary cannot exceed 1.15 pu , whereas in transient state it can reach 5.24 pu.


Representation of the torque as a function of the internal angle in dynamic and static states.

## Machine stability and internal angle

The synchronous machine will always be stable if the electrical torque drift is positive compared to the internal angle. In other words when on an ascending part of the $\mathrm{Ce}(\delta)$ function.
Thus when stationary, the machine will always be stable in the above example, if the internal angle does not exceed $65^{\circ}$. Whereas in transient state, the internal angle can be as large as $115^{\circ}$ without affecting the synchronous machine's stability.

## Setting the power swing parameters

- Maximum time between 2 rotations:

The maximum time between 2 rotations should be configured with a value higher than the mechanical movement's oscillation period Tosc.
■ Number of rotations:
The number of power swings is not directly linked to the number of rotations in the internal angle. Thus the number of rotations should be configured with a value higher than 2.

## Setting the internal angle calculation parameters

## ■ Confirmation delay:

The confirmation delay should be configured with half the mechanical movement's oscillation period Tosc.
■ Maximum internal angle variation:
The majority of generators can tolerate, during a loss of synchronism, 2 rotations of their internal angle. Thus, in the absence of manufacturer data, the maximum internal angle variation should be configured with the value of $300^{\circ}$ (corresponding to 1 rotation of the internal angle).

## Protection functions

Recloser
ANSI code 79

## Recloser with 1 to 4 cycles to clear transients or semi-permanent faults on overhead lines.

## Definition

## Reclaim time

The reclaim time is activated by a circuit breaker closing order given by the recloser. If no faults are detected before the end of the reclaim time, the initial fault is
considered to have been cleared.
Otherwise a new reclosing cycle is initiated.
The delay must be longer than the longest reclosing cycle activation condition.

## Safety time until ready

The safety time is activated by a manual circuit breaker closing order. The recloser is inhibited for the duration of the time
If a fault occurs during this time, no reclosing cycles are initiated and the circuit breaker remains permanently open.

## Dead time

Cycle n dead time is launched by breaking device tripping order given by the recloser during cycle $n$.
The breaking device remains open throughout the time. At the end of the cycle $n$ dead time, the $\mathrm{n}+1$ cycle begins, and the recloser orders the closing of the circuit breaker.

## Description

Automation device used to limit down time after tripping due to transient or semipermanent faults on overhead lines. The recloser orders automatic reclosing of the breaking device after the time delay required to restore the insulation. Recloser operation is easy to adapt for different operating modes by parameter setting.

## Initialization of the recloser

The recloser is ready to operate if all of the following conditions are met:
■ "switchgear control" function activated and recloser in service (not inhibited by the recloser inhibition logic input)

- circuit breaker closed
- the safety time is not running

■ none of the recloser inhibition conditions is true (e.g. trip circuit fault, control fault, SF6 pressure drop).

## Recloser cycles

- case of a fault that is not cleared: following instantaneous or time-delayed tripping by the protection unit, activation of the dead time associated with the first active cycle. At the end of the dead time, a closing order is given, which activates the reclaim time. If the protection unit detects the fault before the end of the time delay, a tripping order is given and the following reclosing cycle is activated. after all the active cycles have been run, if the fault still persists, a final trip order is given, a message appears on the display.
■ case of a cleared fault: Following a reclosing order, if the fault does not appear after the reclaim time has run out, the recloser reinitializes and a message appears on the display (see example 1).
- closing on a fault.

If the circuit breaker closes on a fault, or if the fault appears before the end of the safety time delay, the recloser is inhibited. A final trip message is issued.

## Recloser inhibition conditions

The recloser is inhibited according to the following conditions:

- voluntary open or close order
- recloser put out of service
- receipt of a inhibition order on the logic input
- activation of the breaker failure, such as trip circuit fault, control fault, SF6 pressure drop
- opening of the circuit breaker by a protection unit that does not run reclosing cycles (e.g. frequency protection), by external tripping or by a function set up not to activate reclosing cycles.
In such cases, a final trip message appears.


## Extension of the dead time

If, during a reclosing cycle, reclosing of the circuit breaker is impossible because breaker recharging is not finished (following a drop in auxiliary voltage, recharging time is longer), the dead time may be extended up to the time at which the circuit breaker is ready to carry out an "Open-Close-Open" cycle. The maximum time added to the dead time is adjustable (Twait_max). If, at the end of the maximum waiting time, the circuit breaker is still not ready, the recloser is inhibited (see example 5).

| Characteristics |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Settings |  |  |  |  |
| Number of cycles |  |  |  |  |
| Setting range | 1 to 4 |  |  |  |
| Activation of cycle 1 |  |  |  |  |
| Protection 50/51 units 1 to 4 | inst. / delayed | / no activatio |  |  |
| Protection 50N/51N units 1 to 4 | inst. / delayed | / no activatio |  |  |
| Protection 67 units 1 to 2 | inst. / delayed | / no activatio |  |  |
| Protection 67N/67NC units 1 to 2 | inst. / delayed | / no activatio |  |  |
| Logic equations or Logipam outputs V_TRIPCB | active/inactive |  |  |  |
| Activation of cycles 2, 3 and 4 |  |  |  |  |
| Protection 50/51 units 1 to 4 | inst. / delayed | / no activatio |  |  |
| Protection 50N/51N units 1 to 4 | inst. / delayed | / no activatio |  |  |
| Protection 67 units 1 to 2 | inst. / delayed | / no activatio |  |  |
| Protection 67N/67NC units 1 to 2 | inst. / delayed | / no activatio |  |  |
| Logic equations or Logipam outputs V_TRIPCB | active/inactive |  |  |  |
| Time delays |  |  |  |  |
| Reclaim time | 0.1 to 300 s |  |  |  |
| Dead time | 0.1 to 300 s |  |  |  |
|  | 0.1 to 300 s |  |  |  |
|  | 0.1 to 300 s |  |  |  |
|  | 0.1 to 300 s |  |  |  |
| Safety time until ready | 0 to 60 s |  |  |  |
| Maximum additional dead time | 0.1 to 60 s |  |  |  |
| Accuracy ${ }^{(1)}$ | $\pm 2 \%$ or $\pm 25$ |  |  |  |
| Resolution | 10 ms |  |  |  |
| Inputs |  |  |  |  |
| Designation | Syntax | Equations | Logipam |  |
| Protection inhibition | P79_1_113 | - | $\square$ |  |
| Outputs |  |  |  |  |
| Designation | Syntax | Equations | Logipam | Matrix |
| Recloser in service | P79 _1_201 | - | $\square$ | $\square$ |
| Recloser ready | P79 _1_202 | $\square$ | $\square$ | $\square$ |
| Cleared fault | P79 _1_203 | $\square$ | $\square$ | $\square$ |
| Final trip | P79 _1_204 | $\square$ | $\square$ | $\square$ |
| Closing by recloser | P79 _1_205 | $\square$ | $\square$ |  |
| Reclosing cycle 1 | P79 _1_211 | $\square$ | $\square$ | $\square$ |
| Reclosing cycle 2 | P79 _1_212 | $\square$ | $\square$ | $\square$ |
| Reclosing cycle 3 | P79 _1_213 | $\square$ | $\square$ | $\square$ |
| Reclosing cycle 4 | P79 _1_214 | $\square$ | $\square$ | ■ |

(1) Under reference conditions (IEC 60255-6).

## Protection functions

Recloser
ANSI code 79

Example 1. Fault cleared after the second cycle


Example 2. Fault not cleared


## Example 3. Closing on a fault



## Recloser

ready $\qquad$


## Example 4. No extension of dead time



Example 5. Extension of dead time


## Protection functions

Overfrequency
ANSI code 81H

Detection of abnormally high frequencies.

## Description

Detection of abnormally high frequency compared to the rated frequency, to monitor power supply quality or protect a generator against overspeeds.
The frequency is calculated using voltage V1 or U21 when only one voltage is connected, otherwise the positive sequence voltage is used to procure greater stability. It is compared to the Fs set point.
The protection function is inhibited if the voltage used for calculations is under the adjustable set point Vs.
The protection includes a definite time delay T .

## Block diagram



1) Or U21, or $\sqrt{3} . V 1>V s$ if only one $T P$

## Characteristics



Detection of abnormally low frequency for load shedding using a metric frequency criterion.

## Description

Detection of abnormally low frequency compared to the rated frequency, to monitor power supply quality. The protection may be used for overall tripping or load shedding.
The frequency is calculated using voltage V1 or U21 when only one voltage is connected, otherwise the positive sequence voltage is used to procure greater stability. It is compared to the Fs set point.
The protection function is inhibited if the voltage used for calculations is under the adjustable set point Vs.
Protection stability is ensured in the event of the loss of the main source and presence of remanent voltage by a restraint in the event of a continuous decrease of the frequency.
The protection includes a definite (DT) time delay T .

## Block diagram



1) Or U21, or $\sqrt{3} . V 1>$ Vs if only one $T P$.

## Characteristics

| Settings |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Measurement origin |  |  |  |  |
| Setting range | Main channels (U) / Additional channels (U') |  |  |  |
| Fs set point |  |  |  |  |
| Setting range | 40 to 51 Hz or 50 to 61 Hz |  |  |  |
| Accuracy ${ }^{(1)}$ | $\pm 0.01 \mathrm{~Hz}$ |  |  |  |
| Resolution | 0.01 |  |  |  |
| Pick up / drop out difference | $0.05 \mathrm{~Hz} \pm 0.015 \mathrm{~Hz}$ |  |  |  |
| Time delay T |  |  |  |  |
| Setting range | 100 ms to 300 s |  |  |  |
| Accuracy ${ }^{(1)}$ | $\pm 2 \%$ or $\pm 25 \mathrm{~ms}$ |  |  |  |
| Resolution | 10 ms or 1 digit |  |  |  |
| Advanced settings |  |  |  |  |
| Vs set point |  |  |  |  |
| Setting range | 20 \% Un to 90 \% Un |  |  |  |
| Accuracy ${ }^{(1)}$ | 2 \% |  |  |  |
| Resolution | $1 \%$ |  |  |  |
| Restraint on frequency variation |  |  |  |  |
| Setting | With / without |  |  |  |
| dFs/dt set point | $1 \mathrm{~Hz} / \mathrm{s}$ to $15 \mathrm{~Hz} / \mathrm{s}$ |  |  |  |
| Accuracy ${ }^{(1)}$ | $\pm 1 \mathrm{~Hz} / \mathrm{s}$ |  |  |  |
| Resolution | $\pm 1 \mathrm{~Hz} / \mathrm{s}$ |  |  |  |
| Characteristic times |  |  |  |  |
| Operation time | Pick-up $<90 \mathrm{~ms}$ from Fs +0.5 Hz to Fs -0.5 Hz |  |  |  |
| Overshoot time | $<50 \mathrm{~ms}$ from Fs +0.5 Hz to Fs -0.5 Hz |  |  |  |
| Reset time | $<55 \mathrm{~ms}$ from Fs -0.5 Hz to Fs +0.5 Hz |  |  |  |
| Inputs |  |  |  |  |
| Designation | Syntax | Equations Logipam |  |  |
| Protection reset | P81L_x_101 | ■ | $\square$ |  |
| Protection inhibition | P81L_x_113 | - | $\square$ |  |
| Outputs |  |  |  |  |
| Designation | Syntax | Equations | Logipam | Matrix |
| Instantaneous output (pick-up) | P81L_x_1 | ■ | $\square$ |  |
| Delayed output | P81L_x_3 | $\square$ | $\square$ | - |
| Protection inhibited | P81L_x_16 | $\square$ | $\square$ |  |

$x$ : unit number.
(1) Under reference conditions (IEC 60255-6) and df/dt < $3 \mathrm{~Hz} / \mathrm{s}$.

## Protection functions

Rate of change of frequency ANSI code 81R

## Protection function based on the calculation

 of the frequency variation, used to rapidly disconnect a source supplying a network or to control load shedding.
## Operation

The rate of change of frequency protection function is complementary to the under and overfrequency protection functions in detecting network configurations that require load shedding or disconnection.

The function is activated when the "rate of change of frequency" df/dt of the positive sequence voltage is higher than a set point. It includes a definite (DT) time delay.

The protection function operates if:

- the positive sequence voltage is greater than $50 \%$ of the rated phase-to-neutral voltage
- the network frequency is between 42.2 Hz and 56.2 Hz for 50 Hz networks and between 51.3 Hz and 65 Hz for 60 Hz networks.


## Block diagram



## Characteristics

| Settings |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| dfs/dt set point |  |  |  |  |
| Setting range | 0.1 to $10 \mathrm{~Hz} / \mathrm{s}$ |  |  |  |
| Accuracy ${ }^{(1)}$ | $\pm 5 \%$ or $\pm 0,1 \mathrm{~Hz}$ |  |  |  |
| Resolution | 0.01 Hz |  |  |  |
| Drop out/pick up ratio | 93 \% |  |  |  |
| Temporisation |  |  |  |  |
| Setting range | 0.15 to 300 s |  |  |  |
| Accuracy ${ }^{(1)}$ | $\pm 2 \%$ or -10 at +25 ms |  |  |  |
| Resolution | 10 ms or 1 digit |  |  |  |
| Characteristic times ${ }^{(1)}$ |  |  |  |  |
| Operation time | Pick-up < 150 ms (typically 130 ms ) |  |  |  |
| Overshoot time | < 100 ms |  |  |  |
| Reset time | < 100 ms |  |  |  |
| Inputs |  |  |  |  |
| Designation | Syntax | Equations | Logipam |  |
| Protection reset | P81R_x_101 | - | - |  |
| Protection inhibition | P81R_x_113 | - | ■ |  |
| Outputs |  |  |  |  |
| Designation | Syntax | Equations | Logipam | Matrix |
| Instantaneous output (pick-up) | P81R_x_1 | ■ | $\square$ |  |
| Tripping output | P81R_x_3 | $\square$ | $\square$ | - |
| Protection inhibited | P81R_x_16 | $\square$ | - |  |
| Invalid voltage | P81R_x_42 | - | $\square$ |  |
| Invalid frequency | P81R_x_43 | $\square$ | $\square$ |  |
| Positive df/dt | P81R_x_44 | $\square$ | $\square$ |  |
| Negative df/dt | P81R_x_45 | $\square$ | $\square$ |  |
| $x$ : unit number. <br> (1) Under reference conditions | and df/dt | $\mathrm{Hz} / \mathrm{s}$. |  |  |

## Disconnection application

This function is used on incomers of installations that include generators that can operate in parallel with the distribution network.
The role of the function is to detect utility failures, i.e. operation of the generator as an autonomous isolated system. If the power flow from the utility prior to autonomous generator operation was not zero, the generator frequency changes.
The rate of change of frequency protection function detects autonomous generator operation more rapidly than conventional frequency protection functions.

Other disturbances such as short-circuits, load fluctuations and switching may cause changes of frequency. The low set point may be reached temporarily due to these disturbances and a time delay is necessary. In order to maintain the advantage of the speed of the rate of change of frequency protection in comparison to conventional frequency protection functions, a second, higher set point with a short time delay may be added.

The rate of change of frequency is actually not constant. Often, the rate of change of frequency is at its highest at the beginning of the disturbance after which it decreases. This extends the tripping time of frequency protection functions but does not affect the tripping time of the rate of change of frequency protection function.

## Low set point setting

■ Follow the utility's instructions, if there are any.

- If there are no utility instructions, proceed as follows:
$\square$ if the maximum rate of change of frequency on the network under normal conditions is known, dfs/dt should be set above it.
$\square$ if no information on the network is available, the low set point may be set according to generator data.
A good approximation of the rate of change of frequency after a utility failure resulting in a load variation $\Delta \mathrm{P}$ is:

| $\Delta \mathbf{P} \times \mathbf{f n}$ | where Sn |
| :---: | :---: |
| $\underline{2 \times \mathrm{Sn} \times \mathrm{H}}$ | fn : rated frequency |
|  | onstan |

Typical value of the inertia constant (in MWs/MVA):

- $0.5 \leqslant \mathrm{H} \leqslant 1.5$ for diesel and low-power generators ( $\leqslant 2 \mathrm{MVA}$ )
- $2 \leqslant \mathrm{H} \leqslant 5$ for gas turbines and medium-power generators ( $\leqslant 40$ MVA)
$\mathbf{H}=\frac{\mathbf{J} \times \Omega^{2}}{2 \times \mathbf{S n}} \quad$ where J : moment of inertia
$2 \times \mathbf{S n} \quad \Omega$ machine speed
Examples

| Rated power | 2 MVA | 20 MVA |
| :--- | :--- | :--- |
| Inertia constant | $0.5 \mathrm{MWs} / \mathrm{MVA}$ | $2 \mathrm{MWs} / \mathrm{MVA}$ |
| Power variation | 0.1 MVA | 1 MVA |
| $\mathrm{dt} / \mathrm{dt}$ | $-2.5 \mathrm{~Hz} / \mathrm{s}$ | $-0.6 \mathrm{~Hz} / \mathrm{s}$ |

## Low set point delay setting

For good protection stability during short-circuits or transient disturbances, the recommended time delay is 300 ms or more. If an automatic recloser is in service upstream of the installation, the detection of autonomous generator operation and the opening of the coupling circuit breaker must take place during the recloser isolation time.

High set point setting
The second set point may be chosen so that the rate of change of frequency tripping curve remains below the under and overfrequency protection curves.
If the frequency protection units are set to $\mathrm{fn} \pm 0.5 \mathrm{~Hz}$ and the low set point of the rate of change of frequency is T , the high set point may be set to $0.5 / \mathrm{T}$.

## High set point delay setting

No particular recommendantions.

| Setting recommendations when no other information is available |  |  |  |
| :--- | :--- | :--- | :--- |
|  | Generator power | $\mathbf{2}$ to $\mathbf{1 0} \mathbf{~ M V A}$ | $\mathbf{> 1 0 ~ M V A ~}$ |
| Settings |  | $0.5 \mathrm{~Hz} / \mathrm{s}$ | $0.2 \mathrm{~Hz} / \mathrm{s}$ |
| Low set point | dfs/dt | 500 ms | 500 ms |
|  | T | $2.5 \mathrm{~Hz} / \mathrm{s}$ | $1 \mathrm{~Hz} / \mathrm{s}$ |
| High set point | $\mathrm{dfs} / \mathrm{dt}$ | 150 ms | 150 ms |
|  | T |  |  |

## Rate of change of frequency ANSI code 81R

## Operating precautions:

When the generator connects to the network, power oscillations may occur until the generator becomes fully synchronized. The rate of change of frequency protection function is sensitive to this phenomenon, so it is advisable to inhibit the protection unit for a few seconds after circuit breaker closing.

## Load shedding application

The rate of change of frequency protection function may also be used for load shedding in combination with underfrequency protection. In such cases, it is used on the installation busbars. Only negative frequency derivatives are to be used.

Two principles are available:
■ acceleration of load shedding:
The rate of change of frequency protection functions controls load shedding. It acts faster than underfrequency protection functions and the value measured (df/dt) is directly proportional to the load to be shed

- load shedding inhibition:

This principle is included in underfrequency protection functions. It consists of activating the frequency variation restraint and does not call for implementation of the rate of change of frequency protection function.

Phase-to-phase short-circuit protection for generators and motors.

## Description

Phase-to-phase short-circuit protection, based on phase by phase comparison of the currents on motor and generator windings.
This function picks up if the difference in current is greater than the set point defined by:

- a percentage-based curve

■ a differential curve (high set point).
Tripping restraint ensures stability due to:
■ detection of an external fault or machine starting

- detection of CT saturation
- fast detection of CT loss
- detection of transformer energizing.



## Percentage-based differential

The percentage-based tripping characteristic compares the through current to the differential current.
According to the current measurement convention, shown in the diagram and respecting the recommended wiring system, the differential and through currents are calculated by:

- differential current:
$\boldsymbol{I d} \mathbf{x}=\left|\overrightarrow{\boldsymbol{I}}_{\mathbf{x}}+\overrightarrow{\boldsymbol{I}}_{\mathbf{x}}\right|$ where $\mathrm{x}=1,2,3$
- through current

Itx $=\frac{\left|\vec{I}_{x}-\vec{I}_{x}\right|}{2}$ where $x=1,2,3$
The percentage-based characteristic is made up to two half curves defined according to the following formulas:

- $1^{\text {st }}$ half curve depending on the Is set point
$\mathbf{I d} \mathbf{x}^{\mathbf{2}}-\frac{\mathbf{I t x}^{2}}{\mathbf{3 2}}>\mathbf{I s}^{2}$ where $\mathbf{0} \leqslant \boldsymbol{I t x} \leqslant \sqrt{2} \ln$ and $x=1,2,3$
- $2^{\text {nd }}$ half curve
$\frac{\mathbf{I d x}}{8}-\frac{\mathbf{I t x}^{2}}{32}>(0.05 \ln )^{2} \quad$ where $\sqrt{2} \ln <\operatorname{ltx}$ and $x=1,2,3$.



## Differential high set point.

To avoid any delay for major asymmetrical faults, a differential high set point, without restraint, is used.
The characteristic of this set point is:
$\operatorname{Id} \mathbf{x}>5.5$ $\mathbf{I n}$ and $\frac{\mathbf{I d} \mathbf{x}}{\mathbf{I t} \mathbf{x}}>\mathbf{1}$ where $\mathrm{x}=1,2,3$

## Tripping restraints

- Restraint for external faults or machine starting

During starting or an external fault, the through current is much higher than 1.5 In . As long as the CTs do not saturate, the differential current is low. This transient state is detected by the following characteristic:
$\frac{\mathbf{I d x}^{2}}{2}-\frac{\mathbf{I t x}^{2}}{\mathbf{3 2}}<-(\mathbf{0 . 2 5} \mathbf{~ I n})^{2} \quad$ where $\mathrm{x}=1,2,3$
An external fault can be followed by a short, but high differential current, that is why a 200 ms restraint is used to ensure protection stability for this type of fault.

- Restraint on CT saturation

CT saturation can result in a false differential current and nuisance tripping. The restraint analyses the asymmetry of the signals and restrains the tripping order if a CT is saturated.

- Restraint on CT loss

CT loss can result in a false differential current and nuisance tripping. This restraint is the means to detect a measurement that abnormally drops to zero (sample analysis).

- Restraint on transformer energizing
this restraint ensures that the H 2 level of the differential current is greater than $15 \%$ :
$\frac{\mathbf{I d x h} 2}{\mathbf{I d} \mathbf{x}}>0.15$ where $\mathrm{x}=1,2,3$.
Block diagram


CT loss can result in a false differential current and nuisance tripping. This restraint is activated if the following 3 criteria are met. The first two criteria identify the potentially defective CT; the third confirms the CT loss.

1) A residual current (SUM3I) is detected from one side of the windings and only one. $|\vec{l} 1+\vec{l} 2+\vec{l} 3|>\mid$ so $\oplus\left|\overrightarrow{r^{\prime}} 1+\overrightarrow{l^{\prime}} 2+\overrightarrow{l^{\prime}} 3\right|>$ Iso (Iso: internal threshold, non-adjustable)
2) The differential current is higher than the threshold Is on one phase and only one. Id $1>$ Is $\oplus$ Id $2>$ Is $\oplus$ Id $3>$ Is
3) Abnormal number of zero value samples $(|i x|<0.02 \times \ln )$ is measured on the considered input.
The restraint is disabled if one criterion is not met.
$\oplus$ = Exclusive OR (XOR)

## Dimensioning phase-current sensors

Current transformers must be either:

- type 5P20, with an accuracy burden VAct $\geqslant$ Rw.in ${ }^{2}$

■ or defined by a knee-point voltage $\mathrm{Vk} \geqslant(\mathrm{Rct}+\mathrm{Rw}) .20$.in.
The equations apply to the phase current transformers placed on either side of the machine.
in is the CT rated secondary current.
Rct is the CT internal resistance.
Rw is the resistance of the CT load and wiring.
The setting range of the is set point depends on the rated values of the current sensors on the main channels I1, I2, I3 and the additional channels I'1, I'2, I'3. The setting range is the intersection of [ 0.05 In 0.5 In ] with [ 0.05 I n 0.5 I n ]. When the rated values are identical, the setting range is optimum. If there is no intersection, the function cannot be used.

## Characteristics

| Settings |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Is set point |  |  |  |  |
| Setting range | $\mathrm{In} \leq 20 \mathrm{~A}: \max (0.1 \mathrm{In} ; 0.1 \mathrm{I} \mathrm{n}) \leqslant \mathrm{Is} \leqslant \min (0.5 \mathrm{In} ; 0.5 \mathrm{I} \mathrm{n})$ $\mathrm{In}>20 \mathrm{~A}: \max (0.05 \mathrm{In} ; 0.05 \mathrm{I} \mathrm{n}) \leq \mathrm{Is} \leq \max (0.5 \mathrm{In} ; 0.5 \mathrm{I} \mathrm{n})$ |  |  |  |
| Accuracy (1) | $\pm 5 \%$ Is or $\pm 0.4$ \% In |  |  |  |
| Resolution | 1 A or 1 digit |  |  |  |
| Drop out/pick up ratio | 93.5 \% $\pm 5$ \% |  |  |  |
| Pick-up of restraint on CT loss |  |  |  |  |
| Characteristic times |  |  |  |  |
| Operation time | Operation time of differential current function |  |  |  |
| Overshoot time | $<45 \mathrm{~ms}$ at 2 ls |  |  |  |
| Designation | Syntax | Equations | Logipam |  |
| Protection reset | P81L_x_101 | - | ■ |  |
| Designation | Syntax | Equations | Logipam | Matrix |
| Protection output | P87M_1_3 | ■ | - | - |
| Phase 1 fault | P87M_1_7 | $\square$ | $\square$ |  |
| Phase 2 fault | P87M _1_8 | $\square$ | - |  |
| Phase 3 fault | P87M _1_9 | $\square$ | - |  |
| Protection inhibited | P87M_1_16 | $\square$ | $\square$ |  |
| High set point | P87M_1_33 | $\square$ | - |  |
| Percentage-based set point | P87M_1_34 | $\square$ | $\square$ |  |
| CT loss | P87M_1_39 | $\square$ | $\square$ |  |
| (1) Under reference condition | 60255-6). |  |  |  |

## Protection functions

Phase-to-phase short-circuit protection for transformers and transformer-machine units (2 windings)

## Operation

This protection function protects the zone between the sensors for the main currents $\mathrm{I} 1, \mathrm{I} 2, \mathrm{I} 3$ on the one hand and the sensors for the additional currents l'1, l'2, l'3 on the other.
It adjusts both the amplitude and phase of the currents in each winding according to the vector shift and the transformer rated power, as well as the set voltage and current values.
It then compares the matched currents phase by phase.


## Transformer differential ANSI code 87T

## Definitions

The terms winding 1 and winding 2 are used in the following manner:
■ winding 1: corresponds to the circuit to which the main currents I1, I2, I3 and the voltage measurements V1, V2, V3 or U21, U32 are connected
■ winding 2: corresponds to the circuit to which the additional currents I'1, I'2, I'3 are connected.

The transformer electrical parameters must be set on the "Particular characteristics" screen in the SFT2841 software:
■ winding 1 voltage: Un1
■ winding 2 voltage: Un2

- vector shift
- transformer rated power S.

To assist during the setup procedure, the screen shows:
■ the transformer rated current value for windings 1 and $2: \ln 1, \ln 2$
■ the value set on the "CT-VT Sensors" screen for the base current lb of winding 1

- the value calculated using the transformation ratio for the base current l'b of winding 2.


## Matching

## Principle

The currents in windings 1 and 2 cannot be compared directly due to the transformation ratio and the phase displacement introduced by the power transformer.
Sepam does not use matching CTs. Sepam uses the rated power and winding voltage data to calculate the transformation ratio and, therefore, to match current amplitude. The vector shift is used to match the phase currents.

## Winding 1 current matching

Winding 1 is always matched in the same way, whatever the vector shift of the transformer. The matching is made by clearing the zero-sequence current in order to make the protection function immune to external earth faults.
$\overrightarrow{1} 1 m=\frac{\overrightarrow{1} 1}{\ln 1}-\frac{\overrightarrow{1} 1+\overrightarrow{1} 2+\overrightarrow{1} 3}{3 \ln 1}$
$\overrightarrow{\vec{l}} 2 \mathrm{~m}=\frac{\vec{l} 2}{\ln 1}-\frac{\overrightarrow{\overrightarrow{1}} 1+\vec{l} 2+\vec{l} 3}{3 \ln 1}$
$\overrightarrow{\vec{l}} 3 \mathrm{~m}=\frac{\overrightarrow{1} 3}{\ln 1}-\frac{\overrightarrow{1} 1+\overrightarrow{1} 2+\vec{l} 3}{3 \ln 1}$

## Winding 2 current matching and vector shift

The matching of winding 2 affects the amplitude and phase and takes account of the vector shift of the transformer.
Standard IEC 60076-1 assumes that the vector shift is given for a transformer connected to a power source with a phase-rotation sequence of 123. Sepam uses this vector shift value for both 123 and 132 type networks.
It is, therefore, not necessary to complement this value by 12 for a 132 type network. When the current sensor connections are correct, the vector shift matching to be made is the result of the phase-displacement measurement taken by Sepam between the currents in winding 1 and winding 2 , divided by $30^{\circ}$.
The table on the next page contains vectorial diagrams and matching formulae based on the vector shift of the transformer for networks with type 123 phase-rotation sequences.

## Notation

S: HV/LV transformer rated power
Un1: Winding 1 rated voltage
Un2: Winding 2 rated voltage
In1: Winding 1 rated current
In2: Winding 2 rated current
In: Winding 1 CT rated primary current
I'n: Winding 2 CT rated primary current
in: Winding 1 CT rated secondary current
i'n: Winding 2 CT rated secondary current
VАст: Current transformer accuracy burden
Rw: Resistance of the current transformer load (including wiring)
$\mathbf{R}_{\mathbf{C r}}$ : Current transformer secondary resistance
FLP: Current transformer accuracy-limit factor
Vk: Current transformer knee-point voltage

## Transformer differential ANSI code 87T

| Calculation of matched currents for winding 2 |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Vector shift | Winding 1 | Winding 2 | Matching | Vector shift | Winding 1 | Winding 2 | Matching |
| 0 |  |  | $\begin{aligned} & \overrightarrow{I^{\prime}} 1 \text { rec }=\frac{\overrightarrow{l_{1}} 1}{\ln 2}-\frac{\overrightarrow{l^{\prime}} 1+\overrightarrow{I_{2}} 2+\overrightarrow{I^{\prime}}}{3 \ln 2} \\ & \overrightarrow{I^{\prime}} 2 \text { rec }=\frac{\overrightarrow{l^{\prime}} 2}{\ln 2}-\frac{\overrightarrow{l_{1}} 1+\overrightarrow{I^{\prime}} 2+\overrightarrow{I^{\prime}}}{\ln 2} \\ & \overrightarrow{I^{\prime}} 3 \text { rec }=\frac{\overrightarrow{l_{2}} 3}{\ln 2}-\frac{\overrightarrow{l^{\prime}} 1+\overrightarrow{I^{\prime}} 2+\overrightarrow{I^{\prime}}}{3 \ln 2} \end{aligned}$ | 6 |  |  | $\begin{aligned} & \overrightarrow{I^{\prime}} 1 \text { rec }=-\frac{\overrightarrow{l_{1}} 1}{\ln 2}+\frac{\overrightarrow{l_{1}} 1+\overrightarrow{Y^{\prime}} 2+\overrightarrow{I^{\prime}}}{3 \ln 2} \\ & \overrightarrow{I^{\prime}} 2 \text { rec }=-\frac{\overrightarrow{l^{\prime}} 2}{\ln 2}+\frac{\overrightarrow{r^{\prime}} 1+\overrightarrow{I_{2}} 2+\overrightarrow{I^{\prime}}}{3 \ln 2} \\ & \overrightarrow{I^{\prime}} 3 \mathrm{rec}=-\frac{\overrightarrow{l^{\prime}} 3}{\ln 2}+\frac{\overrightarrow{r_{1}} 1+\overrightarrow{\mathrm{I}^{\prime}} 2+\overrightarrow{I^{\prime}}}{3 \ln 2} \end{aligned}$ |
| 1 |  |  | $\begin{aligned} & \overrightarrow{l^{\prime}} 1 \text { rec }=\frac{\overrightarrow{r_{1}} 1-\overrightarrow{l^{\prime}} 2}{\sqrt{3} \ln 2} \\ & \overrightarrow{l^{\prime}} 2 \text { rec }=\frac{\overrightarrow{l^{\prime}} 2-\overrightarrow{l^{\prime}} 3}{\sqrt{3} \ln 2} \\ & \overrightarrow{r^{\prime}} 3 \text { rec }=\frac{\overrightarrow{r_{1}} 3-\overrightarrow{l_{1}} 1}{\sqrt{3} \ln 2} \end{aligned}$ | 7 |  |  | $\begin{aligned} & \overrightarrow{r^{\prime}} 1 \text { rec }=\frac{\overrightarrow{r^{\prime}} 2-\overrightarrow{I_{1}} 1}{\sqrt{3} \ln 2} \\ & \overrightarrow{I^{\prime}} 2 \text { rec }=\frac{\overrightarrow{l^{\prime}} 3-\overrightarrow{r^{\prime}} 2}{\sqrt{3} \ln 2} \\ & \overrightarrow{r^{\prime}} 3 \text { rec }=\frac{\overrightarrow{r_{1}} 1-\overrightarrow{r^{\prime}} 3}{\sqrt{3} \ln 2} \end{aligned}$ |
| 2 |  |  | $\begin{aligned} & \overrightarrow{I^{\prime}} 1 \text { rec }=-\frac{\overrightarrow{l^{\prime}} 2}{\ln 2}+\frac{\overrightarrow{l^{\prime}} 1+\overrightarrow{I_{2}} 2+\overrightarrow{I^{\prime}}}{3 \ln 2} \\ & \overrightarrow{I^{\prime}} 2 \text { rec }=-\frac{\overrightarrow{l^{\prime}} 3}{\ln 2}+\frac{\overrightarrow{l_{1}} 1+\overrightarrow{I^{\prime}} 2+\overrightarrow{I^{\prime}}}{3 \ln 2} \\ & \overrightarrow{I^{\prime}} 3 \text { rec }=-\frac{\overrightarrow{l_{1}} 1}{\ln 2}+\frac{\overrightarrow{l^{\prime}} 1+\overrightarrow{l_{2}} 2+\overrightarrow{I^{\prime}}}{3 \ln 2} \end{aligned}$ | 8 |  |  | $\begin{aligned} & \overrightarrow{I^{\prime}} \text { rec }=\frac{\overrightarrow{l_{2}} 2}{\ln 2}-\frac{\overrightarrow{l^{\prime}} 1+\overrightarrow{I^{\prime}} 2+\overrightarrow{I^{\prime}}}{3 \ln 2} \\ & \overrightarrow{I^{\prime}} 2 \text { rec }=\frac{\overrightarrow{l^{\prime}} 3}{\ln 2}-\frac{\overrightarrow{I_{1}} 1+\overrightarrow{I^{\prime}} 2+\overrightarrow{I^{\prime}}}{\ln 2} \\ & \overrightarrow{I^{\prime}} 3 \text { rec }=\frac{\overrightarrow{l_{1}} 1}{\ln 2}-\frac{\overrightarrow{l^{\prime}} 1+\overrightarrow{I^{\prime}} 2+\overrightarrow{I^{\prime}}}{3 \ln 2} \end{aligned}$ |
| 3 |  |  | $\begin{aligned} & \overrightarrow{l^{\prime}} 1 \text { rec }=\frac{\overrightarrow{l_{1}} 3-\overrightarrow{l^{\prime}} 2}{\sqrt{3} \ln 2} \\ & \overrightarrow{l^{\prime}} 2 \text { rec }=\frac{\overrightarrow{l^{\prime}} 1-\overrightarrow{l^{\prime}} 3}{\sqrt{3} \ln 2} \\ & \overrightarrow{r^{\prime}} 3 \text { rec }=\frac{\overrightarrow{r_{2}} 2-\overrightarrow{l^{\prime}} 1}{\sqrt{3} \ln 2} \end{aligned}$ | 9 |  |  | $\begin{aligned} & \overrightarrow{r^{\prime}} 1 \text { rec }=\frac{\overrightarrow{r^{\prime}} 2-\overrightarrow{l^{\prime}} 3}{\sqrt{3} \ln 2} \\ & \overrightarrow{r^{\prime}} \text { 2rec }=\frac{\overrightarrow{l^{\prime}} 3-\overrightarrow{r^{\prime}} 1}{\sqrt{3} \ln 2} \\ & \overrightarrow{r^{\prime}} 3 \text { rec }=\frac{\overrightarrow{r^{\prime}} 1-\overrightarrow{l^{\prime}} 2}{\sqrt{3} \ln 2} \end{aligned}$ |
| 4 |  |  | $\begin{aligned} & \overrightarrow{I^{\prime}} 1 \text { rec }=\frac{\overrightarrow{l^{\prime}} 3}{\ln 2}-\frac{\overrightarrow{l^{\prime}} 1+\overrightarrow{l^{\prime}} 2+\overrightarrow{I^{\prime}}}{3 \ln 2} \\ & \overrightarrow{I^{\prime}} 2 \text { rec }=\frac{\overrightarrow{l^{\prime}} 1}{\ln 2}-\frac{\overrightarrow{l^{\prime}} 1+\overrightarrow{Y^{\prime}} 2+\overrightarrow{l^{\prime}} 3}{3 \ln 2} \\ & \overrightarrow{I^{\prime}} 3 \text { rec }=\frac{\overrightarrow{l^{\prime}} 2}{\ln 2}-\frac{\overrightarrow{l_{1}} 1+\overrightarrow{Y^{\prime}} 2+\overrightarrow{I^{\prime}}}{3 \ln 2} \end{aligned}$ | 10 |  |  | $\begin{aligned} & \overrightarrow{I^{\prime}} 1 \text { rec }=-\frac{\overrightarrow{l_{2}} 3}{\ln 2}+\frac{\overrightarrow{l^{\prime}} 1+\overrightarrow{Y^{\prime}} 2+\overrightarrow{I^{\prime}}}{3 \ln 2} \\ & \overrightarrow{I^{\prime}} 2 \text { rec }=-\frac{\overrightarrow{l^{\prime}} 1}{\ln 2}+\frac{\overrightarrow{l^{\prime}} 1+\overrightarrow{I^{\prime}} 2+\overrightarrow{I^{\prime}}}{3 \ln 2} \\ & \overrightarrow{I^{\prime}} 3 \mathrm{rec}=-\frac{\overrightarrow{l_{2}} 2}{\ln 2}+\frac{\overrightarrow{r_{1}} 1+\overrightarrow{I^{\prime}} 2+\overrightarrow{I^{\prime}}}{3 \ln 2} \end{aligned}$ |
| 5 |  |  | $\begin{aligned} & \overrightarrow{l^{\prime}} 1 \text { rec }=\frac{\overrightarrow{l^{\prime}} 3-\overrightarrow{l^{\prime}} 1}{\sqrt{3} \ln 2} \\ & \overrightarrow{l^{\prime}} 2 \text { rec }=\frac{\overrightarrow{r_{1}} 1-\overrightarrow{l^{\prime}} 2}{\sqrt{3} \ln 2} \\ & \overrightarrow{l^{\prime}} 3 \text { rec }=\frac{\overrightarrow{l_{1}} 2-\overrightarrow{l^{\prime}} 3}{\sqrt{3} \ln 2} \end{aligned}$ | 11 |  |  |  |

## Test mode

Two operating modes are available to facilitate maintenance and startup operations:
■ normal mode: the protection function controls the tripping and indication outputs based on the settings.
This is the standard operating mode

- test mode: the protection function controls the tripping and indication outputs based on the test mode settings.
This mode can only be accessed via the SFT2841 software, once it has been connected and the Protection setting password entered.
The system returns to normal mode when the software is disconnected.
Transfer from normal mode to test mode can result in nuisance tripping if the protected transformer is energized.
Test mode settings:

> ■n1 $=\frac{S}{\ln \times \sqrt{3}}$
> ■Un2 $=\frac{S}{I^{\prime} n \times \sqrt{3}}$

■ vector shift $=0$.

## Transformer differential ANSI code 87T

## High set point

A non-restrained differential current set point will ensure fast tripping in the event of significant fault currents. This threshold must be set to a value higher than that of the inrush current.

## Percentage-based curve

The percentage-based curve comprises a number of segments, which are defined as follows:

- a low set point (lds)
- 2 straight lines crossing zero and with adjustable slopes (Id/It and Id/It2)

■ the slope change point.
The curve must be set so that it can protect itself against current-sensor measurement errors and transformation errors, which can be attributed to the tap changer. Furthermore, the protection function must be made immune to power shunts on auxiliary windings.


## Self-adaptive restraint

Self-adaptive restraint is particularly suitable for transformers where the peak inrush current in Amps is less than $8 \ln 1$ or $8 \ln 2$, depending on the winding by which the transformer is energized.
This neuronal network restraint ensures stability in the event of an external fault by analyzing the second- and fifth-harmonic factors, the differential currents and the through currents.
It ensures stability:

- in the event of the transformer closing
- in the event of an asymmetrical fault outside the zone, which saturates the current sensors
■ in the event of the transformer being operated on a voltage supply, which is too high (overfluxing).
Detecting the presence of harmonics and taking into account the through and differential currents, the restraint automatically increases the low set point and the percentage-based slopes.
It is also more sensitive than the high set point. There is therefore no point in using the high set point when this restraint is active. Furthermore, as the restraint integrates the stabilization slope for high through currents, which can saturate the current sensors, slope Id/It2 does not have to be activated.


## Conventional restraint

The conventional restraint comprises a second-harmonic set point for each phase and a fifth-harmonic set point for each phase.
The second-harmonic set point ensures that the protection function will not pick up in the event of the transformer closing or the current sensors becoming saturated.
The restraint can be global (cross-blocking: all three phases are restrained as soon as the harmonic in one phase exceeds the set point) or phase-specific (no
cross-blocking: only the phase with a harmonic exceeding the set point is restrained). Cross-blocking is recommended for transformers used in three-phase mode. The fifth-harmonic set point ensures that the protection function will not pick up in the event of the transformer being connected to a voltage supply, which is too high.
The restraint can be global (i.e., all three phases are restrained) or phase-specific (only the phase with a harmonic exceeding the set point is restrained). Restraint without cross-blocking is recommended for normal operation.

The CTs are dimensioned on the basis of the transformer inrush current, which differs according to the winding by which the transformer is energized.


## Restraint on closing

In some cases, the harmonic content of the transformer inrush current is not sufficient to activate harmonic restraints. An additional restraint can be activated: ■ when the through current exceeds an adjustable set point Isinr
■ by an internal variable, P87T_1_118, controlled by logic equations or Logipam. This restraint is applied to the percentage-based differential elements for an adjustable time period T . It is not applied to the high set point.


## Restraint on CT loss

CT loss can distort the differential current and cause nuisance tripping. This restraint detects a measurement dropping to zero abnormally by analyzing sampled differential and through currents.

## Dimensioning phase-current sensors

## Calculating inrush currents

- Energization by winding 1:
- Inrush current depends on the transformer rated current:

$$
\hat{\mathrm{i} i n r}=\frac{\text { peak inrush current in Amps }}{\ln 1 \cdot \sqrt{2}}
$$

- Inrush current depends on the CT rated current:
$\hat{\text { innr }} / T C=\frac{\text { peak inrush current in Amps }}{\operatorname{In} \cdot \sqrt{2}}$
- Energization by winding 2 :
- Inrush current depends on the transformer rated current:
$\hat{\mathrm{i}} \mathrm{inr}=$ peak inrush current in Amps
In2. $\sqrt{2}$
- Inrush current depends on the CT rated current:
$\hat{i i n r} / T C=\frac{\text { peak inrush current in Amps }}{I^{\prime}}$
$I^{\prime}$ n. $\sqrt{2}$


## Transformer differential ANSI code 87T

## CT rated primary currents

The rated primary current of the current transformers is governed by the following rule:

- Winding 1 end:
$0.1 \times \frac{S}{U n 1 \times \sqrt{3}} \unlhd n \leq 2.5 \times \frac{S}{U n 1 \times \sqrt{3}}$
$■$ Winding 2 end: $0.1 \times \frac{\mathrm{S}}{\mathrm{Un} 2 \times \sqrt{3}} \unlhd^{\prime} \mathrm{n} \leq 2.5 \times \frac{\mathrm{S}}{\mathrm{Un} 2 \times \sqrt{3}}$


## Other characteristics of the CTs at the transformer energized end

■ Scenario 1: iinr/ TC $<6.7$
Only the following current transformers can be selected:

- Either type 5P20 with an accuracy burden of $\mathbf{V A}_{\mathbf{C T}} \geq \mathbf{R w} \cdot \mathbf{i n}^{\mathbf{2}}$
$\square$ Or defined by a knee-point voltage $\mathbf{V k} \geq\left(\mathbf{R}_{\mathbf{C T}}{ }^{+} \mathbf{R w}\right) \cdot(\mathbf{2 0 i n})$
- Scenario 2: $\quad \hat{i} i n r / T C \geq 6.7$

Only the following current transformers can be selected:

- Either type 5P with an accuracy burden of $\mathbf{V A}_{\mathbf{C T}} \geq \mathbf{R w} \cdot \mathbf{i n}^{2}$

And an accuracy-limit factorFLP $\geq 3$. iinn/ TC
■ Or defined by a knee-point voltagek $\geq\left(\mathbf{R}_{\mathbf{C T}}+\mathbf{R w}\right) \cdot \mathbf{3} \cdot \hat{\mathbf{i}} \mathbf{i n r} / \mathbf{T C} \cdot \mathbf{i n}$

Other characteristics of the CTs at the transformer non-energized end Only the following current transformers can be selected:

- Either type 5P20 with an accuracy burden of VA $\mathbf{C T}^{\geq R w . i n}{ }^{\mathbf{2}}$
$■$ Or defined by a knee-point voltage $\mathbf{V k} \geq\left(\mathbf{R}_{\mathbf{C T}}+\mathbf{R w}\right) .20$ in


## Setting the Ids low set point

b: tap changer peak deviation [as a \% of Un]
$\alpha$ : Composite error at the current sensor accuracy-limit current at the HV end [as a \% of $\ln$ ]
$\beta$ : Composite error at the current sensor accuracy-limit current at the LV end [as a \% of I'n]

Referring to standard IEC 60044-1, the composite error at the accuracy-limit current is $5 \%$ for type 5P CTs. For the CTs specified according to class Px , the maximum error is deemed to equal $5 \%$.

The minimum set point for Ids is found by adding together the errors below:
■ Measurement: $100 \times\left[\frac{(100+\beta)}{100}-\frac{(100-\alpha)}{(100+b)}\right]$
■ Relay: $2 \%$
Example: Transformer equipped with a tap changer of $\mathbf{- 1 0 \% / + 1 5 \%}$.
Using type 5P CTs, the error on the current is:
$00 \times(105 / 100-95 / 115)+2=24.4 \%$
The Ids low set point should therefore be set to the minimum value of $\mathbf{3 0 \%}$.

## Setting the first Id/It slope

b: tap changer peak deviation [as a \% of Un]
$\alpha$ : Composite error at the current sensor accuracy-limit current at the HV end [as a \% of In]
$\beta$ : Composite error at the current sensor accuracy-limit current at the LV end [as a \% of I'n]

Referring to standard IEC 60044-1, the composite error at the accuracy-limit current is $5 \%$ for type 5P CTs. For the CTs specified according to class Px, the maximum error is deemed to equal $5 \%$.

The minimum slope for $\mathbf{I d} / \mathbf{I t}$ is found by adding together the errors below:
■ Measurement: $100 \times\left[1-\frac{(100-\alpha) \cdot 100}{(100+b) \cdot(100+\beta)}\right]$
■ Relay: 2\%
■ Safety margin: 5\%
Example: Transformer equipped with a tap changer of $\mathbf{- 1 0 \% / + 1 5 \%}$.
Using type 5P CTs, the error on the slope is:
$00 \times(1-100 \times 95 / 115 / 105)+2+5=28.3 \%$
The first Id/It slope should therefore be set to $\mathbf{2 8 \%}$.

## Setting the second-harmonic restraint set point

To ensure sufficient stability of the differential protection when the transformer closes, we recommend that the second-harmonic restraint set point is set to $\mathbf{2 0 \%}$, with global restraint.

## Setting the fifth-harmonic restraint set point

To ensure stability of the protection function in the event of an abnormal increase in the voltage or a drop in the network frequency, we recommend that the fifthharmonic restraint set point is set to $35 \%$, with phase-specific restraint.

## Setting the Idmax high set point

The Idmax set point is applied to the non-restrained differential current. It ensures that 87T protection function trips quickly.
The Idmax set point is set as follows: Idmax $\geq \hat{\mathbf{i}} \mathrm{inr}$

## Setting the second Id/It2 slope and the slope change point

The second slope on the percentage-based characteristic ensures sufficient stability of the protection in the event of an external fault resulting in the current sensors becoming saturated.

■ The slope change point is set as a function of the value of the first Id/It slope and the transformer inrush current.
$($ Slope change point $) \leq 2+\frac{3}{4}(\hat{\mathrm{i} i n r})^{4 / 3} \cdot \frac{(\mathrm{ld} / \mathrm{It})}{100}$

- The value of the second slope is:

Id/It2 $\geq 100-3.75 \cdot \hat{i} \mathrm{inr}$ as a \%, with a minimum at $75 \%$.

## Setting the restraint on closing

This is inactive by default. It should only be used in exceptional cases, where the second harmonic is low on closing.
The decision to activate this restraint delays tripping of the 87T protection function by the value of the selected time delay, when there is a pre-existing closure on an internal fault.

## Transformer differential ANSI code 87T

## Characteristics



Second-harmonic restraint for conventional restraint
Setting range Phase-specific/Global

Fifth-harmonic set point for conventional restraint

| Setting range | None, 5 to $40 \%$ |
| :--- | :--- |
| Accuracy ${ }^{(1)}$ | $\pm 5 \%$ |
| Resolution | $1 \%$ |
| Drop-out/pick-up ratio | $90 \% \pm 5 \%$ |

Fifth-harmonic restraint for conventional restraint

| Setting range |  | Phase-specific/Global |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Characteristic times |  |  |  |  |
| Operating time high set point |  | $<45 \mathrm{~ms}$ at 2 ld |  |  |
| Operating time percentage-based curve |  | $<45 \mathrm{~ms}$ at 2 ld |  |  |
| Reset time |  | $<45 \mathrm{~ms}$ at 2 ld |  |  |
| Inputs |  |  |  |  |
| Designation | Syntax | Equations | Logipam |  |
| Protection reset | P87T_1_101 | ■ | $\square$ |  |
| Protection inhibition | P87T_1_113 | - | $\square$ |  |
| Restraint on closing | P87T_1_118 | ■ | ■ |  |
| Outputs |  |  |  |  |
| Designation | Syntax | Equations | Logipam | Matrix |
| Protection output | P87T_1_3 | ■ | $\square$ | $\square$ |
| Protection inhibited | P87T_1_16 | - | $\square$ | - |
| High set point | P87T_1_33 | - | $\square$ | - |
| Percentage-based threshold | P87T_1_34 | - | $\square$ | - |
| CT loss | P87T_1_39 | - | - | - |
| Test mode | P87T_1_41 | $\square$ | $\square$ | - |



## Example 1

■ The transformer is energized at the winding 1 end.

- The inrush current is $\mathbf{8 2 0} \mathbf{A}$.
- This transformer does not feature a tap changer or an auxiliary winding.


## Sensor selection

The rated currents of the windings are:
$\operatorname{In} 1=\frac{4 \mathrm{MVA}}{\sqrt{3} \cdot 20 \mathrm{kV}}=115.5 \mathrm{~A}$ and $\operatorname{In} 2=\frac{4 \mathrm{MVA}}{\sqrt{3} \cdot 1 \mathrm{kV}}=2310 \mathrm{~A}$

The sensor rated current is selected at the next highest standardized values: In = 150 A and $\mathrm{I}^{\prime} \mathrm{n}=3000 \mathrm{~A}$.

Inrush current:
$\hat{\mathbf{i}} \mathrm{inr}=\frac{820}{115.5 \sqrt{2}}=5:$ depending on the transformer rated current
$\hat{\mathbf{i}} \mathrm{inr} / \mathrm{TC}=\frac{820}{150 \sqrt{2}}=3.9$ depending on the CT rated current

■ Winding 1 end,iinr/ TC < 6.7: type 5P20 current transformers are suitable.
■ Winding 2 end, transformer not energized: type 5P20 current transformers are also suitable.

To sum up, the following sensors are selected:
■ Winding 1 end: 150A/1A, 5P20
■ Winding 2 end: 3000A/1A, 5P20

## Setting the Ids low set point

Tap changer peak deviation: $\mathbf{b}=\mathbf{0}$ (no tap changer)
CT error, winding 1: $\alpha=5 \%$
CT error, winding 2: $\beta=5 \%$
Measurement error: $100 \times\left[\frac{(100+\beta)}{100}-\frac{(100-\alpha)}{(100+b)}\right]=10 \%$
Relay error: 2\%
Total error $=\mathbf{1 2 \%}$
Ids should be set to its minimum value of $\mathbf{3 0 \%}$.

## Setting the first Id/lt slope

Measurement error: $100 \times\left[1-\frac{(100-\alpha) .100}{(100+b) \cdot(100+\beta)}\right]=9.5 \%$
Relay error: 2\%
Safety margin: 5\%
Total error: 16.5\%
$\mathrm{Id} / \mathrm{It}$ should be set to the value of $17 \%$.
Selection of restraint $\hat{\mathbf{i}} \mathbf{i n r}<\mathbf{8}$, the self-adaptive restraint is selected.
Thus the second slope on the percentage-based curve and the high set point are not necessary.

## Transformer differential ANSI code 87T



## Example 2

■ The transformer is energized at the winding 1 end.

- The inrush current is 942 A.

Sensor selection
The rated currents of the windings are:
$\operatorname{In} 1=\frac{2.5 \mathrm{MVA}}{\sqrt{3} \cdot 20.8 \mathrm{kV}}=69.4 \mathrm{~A}$ and $\operatorname{In} 2=\frac{2.5 \mathrm{MVA}}{\sqrt{3} \cdot 0.42 \mathrm{kV}}=3440 \mathrm{~A}$

The sensor rated current is selected at the next highest standardized values:
$\mathbf{I n}=100 \mathrm{~A}$ and $\mathrm{I} \mathrm{n}=3500 \mathrm{~A}$.
Inrush current:
$\hat{\mathrm{i}} \mathrm{inr}=\frac{942}{69.4 \cdot \sqrt{2}}=9.6:$ depending on the transformer rated current
$\hat{\mathbf{i}} \mathrm{in} / \mathrm{TC}=\frac{942}{100 \cdot \sqrt{2}}=6.66:$ depending on the CT rated current

■ Winding 1 end, iinr/ TC $<6.7$ : type 5P20 current transformers are suitable.
■ Winding 2 end, transformer not energized: type 5P20 current transformers are also suitable.

## Setting the Ids low set point

Tap changer peak deviation: $\mathbf{b}=15 \%$
CT error, winding 1: $\alpha=5 \%$
CT error, winding 2: $\beta=5 \%$
Measurement error: $100 \times\left[\frac{(100+\beta)}{100}-\frac{(100-\alpha)}{(100+b)}\right]=22.4 \%$
Relay error: 2\%
Total error = 24.4\%

Ids should be set to its minimum value of $\mathbf{3 0 \%}$.

## Setting the first Id/lt slope

Measurement error: $100 \times\left[1-\frac{(100-\alpha) \cdot 100}{(100+b) \cdot(100+\beta)}\right]=21.3 \%$
Relay error: 2\%
Safety margin: 5\%
Total error: 28.3\%

Id/It should be set to the value of $\mathbf{2 9 \%}$.
$\hat{\mathrm{i}} \mathrm{inr}>\mathbf{8}$, the conventional restraint is selected.

## Setting the slope change point

Point de changement de pente $=2+\frac{3}{4}(\hat{\text { iinr }})^{4 / 3} \cdot \frac{(\text { ld } / \text { It })}{100}$

$$
=6.4 \ln 1
$$

Setting the second slope
$100-(3.75 \cdot \hat{\mathbf{i}} \mathrm{inr})=64 \%$
Choose the minimum advised value: $\mathrm{Id} / \mathrm{It} \mathbf{2}=\mathbf{7 5} \%$

Setting the Idmax high set point
Idmax $=\hat{\mathbf{i}} \mathbf{i n r}=9.6 \ln 1$

Setting the harmonic restraints
■ Set point H2 = 20\%, with global restraint

- Set point H5 = 35\%, with phase-specific restraint

Presentation of tripping curve operation and settings for protection functions using:

## - definite time

- IDMT
- timer hold.


## Definite time protection

The tripping time is constant. The time delay is started when the set point is overrun.


Definite time protection principle.

## IDMT protection

The operation time depends on the protected value (phase current, earth fault current, etc.) in accordance with standards IEC 60255-3, BS 142 and IEEE C-37112.
Operation is represented by a characteristic curve, e.g.:
■ $t=f(I)$ curve for the phase overcurrent function
■ $t=f(I 0)$ curve for the earth fault function.
The rest of the document is based on $t=f(I)$; the reasoning may be extended to other variables 10 , etc.
The curve is defined by:
■ its type (standard inverse, very inverse, extremely inverse, etc.)

- current setting Is which corresponds to the vertical asymptote of the curve
- time delay T which corresponds to the operation time for $\mathrm{I}=10 \mathrm{Is}$.

These 3 settings are made chronologically in the following order: type, Is current, time delay T .
Changing the time delay $T$ setting by $x \%$ changes all of the operation times in the curve by $\mathrm{x} \%$.


IDMT protection principle.
The tripping time for $1 / I s$ values less than 1.2 depends on the type of curve selected.

| Name of curve | Type |
| :--- | :--- |
| Standard inverse time (SIT) | 1,2 |
| Very inverse time (VIT or LTI) | 1,2 |
| Extremely inverse time (EIT) | 1,2 |
| Ultra inverse time (UIT) | 1,2 |
| RI curve | 1 |
| IEC inverse time SIT / A | 1 |
| IEC very inverse time VIT or LTI / B | 1 |
| IEC extremely inverse time EIT / C | 1 |
| IEEE moderately inverse (IEC / D) | 1 |
| IEEE very inverse (IEC / E) | 1 |
| IEEE extremely inverse (IEC / F) | 1 |
| IAC inverse | 1 |
| IAC very inverse | 1 |
| IAC extremely inverse | 1 |

■ when the monitored value is more than 20 times the set point, the tripping time is limited to the value corresponding to 20 times the set point.
■ if the monitored value exceeds the measurement capacity of Sepam ( 40 In for the phase current channels, 20 InO for the residual current channels), the tripping time is limited to the value corresponding to the largest measurable value ( $40 \ln$ or $20 \ln 0$ ).

## Protection functions

General
Tripping curves

## Current IDMT tripping curves

Multiple IDMT tripping curves are offered, to cover most applications:

- IEC curves (SIT, VIT/LTI, EIT)
- IEEE curves (MI, VI, EI)
- commonly used curves (UIT, RI, IAC).

IEC curves

| Equation | Curve type | Coefficient values |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  | k | $\alpha$ | $\beta$ |
| $t_{d}(I)=\frac{k}{\left(\frac{I}{I_{s}}\right)^{\alpha}-1} \times \frac{T}{\beta}$ | Standard inverse / A | 0.14 | 0.02 | 2.97 |
|  | Very inverse / B | 13.5 | 1 | 1.50 |
|  | Long time inverse / B | 120 | 1 | 13.33 |
|  | Extremely inverse / C | 80 | 2 | 0.808 |
|  | Ultra inverse | 315.2 | 2.5 | 1 |

RI curve
Equation: $\quad t_{d}(I)=\frac{1}{0.339-0.236\left(\frac{I}{I_{s}}\right)^{-1}} \times \frac{T}{3.1706}$
IEEE curves

|  | IEEE curves |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Equation | Curve type | Coefficient values |  |  |  |
|  |  | A | B | p | $\beta$ |
|  | Moderately inverse | 0.010 | 0.023 | 0.02 | 0.241 |
| A $\mathrm{B}^{\text {a }}$ | Very inverse | 3.922 | 0.098 | 2 | 0.138 |
| $t_{\text {d }}(\mathrm{I})=\frac{A}{\text { I }} \mathbf{p}+B \times \frac{1}{\beta}$ | Extremely inverse | 5.64 | 0.0243 | 2 | 0.081 |


|  | IAC curves |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Equation | Curve type | Coefficient values |  |  |  |  |  |
|  |  | A | B | C | D | E | $\beta$ |
|  | Inverse | 0.208 | 0.863 | 0.800 | -0.418 | 0.195 | 0.297 |
|  | Very inverse | 0.090 | 0.795 | 0.100 | -1.288 | 7.958 | 0.165 |
|  | Extremely inverse | 0.004 | 0.638 | 0.620 | 1.787 | 0.246 | 0.092 |

$t_{d}(I)=\left(A+\frac{B}{\left(\frac{I}{I_{s}}-C\right)}+\frac{D}{\left(\frac{I}{I_{s}}-C\right)^{2}}+\frac{E}{\left(\frac{I}{I_{s}}-C\right)^{3}}\right) \times \frac{T}{\beta}$

## Voltage IDMT tripping curves

Equation for ANSI 27 - Undervoltage
Equation for ANSI 59N - Neutral voltage displacement
$\mathrm{t}_{\mathrm{d}}(\mathbf{V})=\frac{\mathbf{T}}{1-\left(\frac{\mathbf{V}}{\mathbf{V}_{\mathrm{s}}}\right)}$
$t_{d}(V)=\frac{T}{\left(\frac{V}{V_{s}}\right)-1}$

Voltage/frequency ratio IDMT tripping curves
Equation for ANSI 24 - Overfluxing (V/Hz)
Where $\mathrm{G}=\mathrm{V} / \mathrm{f}$ or U/f
$t_{d}(G)=\frac{1}{\left(\frac{G}{G_{s}}-1\right)^{p}} \times T$

| Curve type | $\mathbf{p}$ |
| :--- | :--- |
| A | 0.5 |
| $B$ | 1 |
| C | 2 |

## Protection functions

General
Tripping curves


Example.


Detection of restriking faults with adjustable timer hold.


Timer hold dependent on current I .


Customized tripping curve set using SFT2841 software.

Setting of IDMT tripping curves, time delay T or TMS factor
The time delays of current IDMT tripping curves (except for customized and RI curves) may be set as follows:

- time T , operating time at 10 x Is
- TMS factor, factor shown as $T / \beta$ in the equations on the left.

Example: $\mathbf{t}(\mathrm{I})=\frac{13.5}{\frac{\mathrm{I}}{\mathrm{Is}}-1} \times$ TMS whereTMS $=\frac{\mathrm{T}}{1.5}$.
The IEC curve of the VIT type is positioned so as to be the same with $\mathrm{TMS}=1$ or $\mathrm{T}=1.5 \mathrm{~s}$.

## Timer hold

The adjustable timer hold T1 is used for:
■ detection of restriking faults (DT curve)

- coordination with electromechanical relays (IDMT curve).
- Timer hold may be inhibited if necessary.


## Equation for IDMT timer hold curve

Equation: $\mathbf{t}_{\mathbf{r}}(\mathbf{I})=\frac{\mathbf{T} \mathbf{1}}{\mathbf{1}-\left(\frac{\mathbf{I}}{\mathbf{I s}}\right)^{2}} \times \frac{\mathbf{T}}{\beta}$ where $\frac{\mathbf{T}}{\beta}=\mathbf{T M S}$.
$\mathrm{T} 1=$ timer hold setting (timer hold for I reset $=0$ and TMS = 1)
$\mathrm{T}=$ tripping time delay setting (at 10 Is )
$b=$ basic tripping curve value at $\frac{k}{10^{\alpha}-1}$.


Constant timer hold.

## Customized tripping curve

Defined point by point using the SFT2841 setting and operating software tool (application menu), this curve may be used to solve all special cases involving protection coordination or installation renovation.
It offers between 2 and 30 points whose coordinates must be:

- increasing on the I/Is axis
- decreasing on the t axis.

The two end points define the curve asymptotes.
There must be at least one point on the horizontal coordinate $10 \mathrm{l} / \mathrm{ls}$. It serves as a reference point to set the function time delay by curve shifting.

## Implementing IDMT curves: examples of problems to be solved.

## Problem 1.

Given the type of IDMT, determine the Is current and time delay T settings.
Theoretically, the Is current setting corresponds to the maximum continuous current: it is generally the rated current of the protected equipment (cable,
transformer).
The time delay T corresponds to operation at 10 Is on the curve. This setting is determined taking into account the constraints involved in discrimination with the upstream and downstream protection devices. The discrimination constraint leads to the definition of point $A$ on the operation curve (IA, tA), e.g. the point that corresponds to the maximum fault current for the downstream protection device.

## Problem 2.

Given the type of IDMT, the Is current setting and a point $k(l k, t k)$ on the operation curve, determine the time delay setting T .
On the standard curve of the same type, read the operation time tsk that corresponds to the relative current Ik/Is and the operation time Ts10 that corresponds to the relative current $\mathrm{I} / \mathrm{Is}=\mathbf{1 0}$.

The time delay setting to be used so that the operation curve passes through the point k ( $\mathrm{lk}, \mathrm{tk}$ ) is:

$$
T=T s 10 \times \frac{t k}{t s k}
$$



## Another practical method:

the table below gives the values of $K=\mathbf{t s} / \mathbf{t s} 10$ as a function of $I / I \mathbf{s}$.
In the column that corresponds to the type of time delay, read the value $\mathbf{K}=\mathbf{t s k} / \mathbf{T} \mathbf{s} 10$ on the line for Ik/ls.
The time delay setting to be used so that the operation curve passes through point $k(l k, t k)$ is: $\mathbf{T}=\mathbf{t k} / \mathbf{k}$.

## Example

Data:

- type of time delay: standard inverse time (SIT)
- set point: Is
- a point k on the operation curve: k ( $3.5 \mathrm{Is} ; 4 \mathrm{~s}$ )

Question: What is the time delay T setting (operation time at 10 Is )?
Reading the table: SIT column, line $\mathrm{I} / \mathrm{Is}=\mathbf{3 . 5}$ therefore $\mathrm{K}=1.858$
Answer: The time delay setting is $\mathrm{T}=4 / 1.858=2.15 \mathrm{~s}$

## Protection functions

General
Tripping curves

Problem 3.
Given the Is current and time delay T settings for a type of time delay (standard inverse, very inverse, extremely inverse), find the operation time for a current value IA. On the standard curve of the same type, read the operation time tsA that corresponds to the relative current $\mathrm{IA} / \mathrm{Is}$ and the operation time Ts10 that corresponds to the relative current $\mathrm{I} / \mathrm{l}=\mathbf{1 0}$.
The operation time $t A$ for the current IA with the Is and T settings is $\mathrm{tA}=\mathrm{tsA} \times \mathrm{T} / \mathrm{Ts} 10$.


## Another practical method:

the table below gives the values of $\mathbf{K}=\mathbf{t s} / \mathrm{Ts} 10$ as a function of I/ls.
In the column that corresponds to the type of time delay, read the value $\mathrm{K}=\mathbf{t s A} / \mathrm{Ts} 10$ on the line for IA/Is, the operation time tA for the current IA with the Is and T settings is $t A=K$. $T$.

## Example

Data:

- type of time delay: very inverse time (VIT)
- set point: Is
- time delay $\mathrm{T}=0.8 \mathrm{~s}$.

Question: What is the operation time for the current IA = 6 Is ?
Reading the table: VIT column, line $\mathrm{I} / \mathrm{Is}=6$, therefore $\mathrm{k}=1.8$
Answer: The operation time for the current IA is $t=1.80 \times 0.8=1.44 \mathrm{~s}$.

Table of $K$ values

| I/ls | SIT <br> and IEC/A | VIT, LTI <br> and IEC/B | EIT <br> and IEC/C | UIT | RI | IEEE MI (IEC/D) | IEEE VI (IEC/E) | IEEE EI <br> (IEC/F) | IAC I | IAC VI | IAC EI |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1.0 | $\infty^{(1)}$ | $\infty^{(1)}$ | $\infty^{(1)}$ | - | 3.062 | $\infty$ | $\infty$ | $\infty$ | 62.005 | 62.272 | 200.226 |
| 1.1 | $24.700{ }^{(1)}$ | $90.000{ }^{(1)}$ | $471.429{ }^{(1)}$ | - | 2.534 | 22.461 | 136.228 | 330.606 | 19.033 | 45.678 | 122.172 |
| 1.2 | 12.901 | 45.000 | 225.000 | 545.905 | 2.216 | 11.777 | 65.390 | 157.946 | 9.413 | 34.628 | 82.899 |
| 1.5 | 5.788 | 18.000 | 79.200 | 179.548 | 1.736 | 5.336 | 23.479 | 55.791 | 3.891 | 17.539 | 36.687 |
| 2.0 | 3.376 | 9.000 | 33.000 | 67.691 | 1.427 | 3.152 | 10.199 | 23.421 | 2.524 | 7.932 | 16.178 |
| 2.5 | 2.548 | 6.000 | 18.857 | 35.490 | 1.290 | 2.402 | 6.133 | 13.512 | 2.056 | 4.676 | 9.566 |
| 3.0 | 2.121 | 4.500 | 12.375 | 21.608 | 1.212 | 2.016 | 4.270 | 8.970 | 1.792 | 3.249 | 6.541 |
| 3.5 | 1.858 | 3.600 | 8.800 | 14.382 | 1.161 | 1.777 | 3.242 | 6.465 | 1.617 | 2.509 | 4.872 |
| 4.0 | 1.676 | 3.000 | 6.600 | 10.169 | 1.126 | 1.613 | 2.610 | 4.924 | 1.491 | 2.076 | 3.839 |
| 4.5 | 1.543 | 2.571 | 5.143 | 7.513 | 1.101 | 1.492 | 2.191 | 3.903 | 1.396 | 1.800 | 3.146 |
| 5.0 | 1.441 | 2.250 | 4.125 | 5.742 | 1.081 | 1.399 | 1.898 | 3.190 | 1.321 | 1.610 | 2.653 |
| 5.5 | 1.359 | 2.000 | 3.385 | 4.507 | 1.065 | 1.325 | 1.686 | 2.671 | 1.261 | 1.473 | 2.288 |
| 6.0 | 1.292 | 1.800 | 2.829 | 3.616 | 1.053 | 1.264 | 1.526 | 2.281 | 1.211 | 1.370 | 2.007 |
| 6.5 | 1.236 | 1.636 | 2.400 | 2.954 | 1.042 | 1.213 | 1.402 | 1.981 | 1.170 | 1.289 | 1.786 |
| 7.0 | 1.188 | 1.500 | 2.063 | 2.450 | 1.033 | 1.170 | 1.305 | 1.744 | 1.135 | 1.224 | 1.607 |
| 7.5 | 1.146 | 1.385 | 1.792 | 2.060 | 1.026 | 1.132 | 1.228 | 1.555 | 1.105 | 1.171 | 1.460 |
| 8.0 | 1.110 | 1.286 | 1.571 | 1.751 | 1.019 | 1.099 | 1.164 | 1.400 | 1.078 | 1.126 | 1.337 |
| 8.5 | 1.078 | 1.200 | 1.390 | 1.504 | 1.013 | 1.070 | 1.112 | 1.273 | 1.055 | 1.087 | 1.233 |
| 9.0 | 1.049 | 1.125 | 1.238 | 1.303 | 1.008 | 1.044 | 1.068 | 1.166 | 1.035 | 1.054 | 1.144 |
| 9.5 | 1.023 | 1.059 | 1.109 | 1.137 | 1.004 | 1.021 | 1.031 | 1.077 | 1.016 | 1.026 | 1.067 |
| 10.0 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 |
| 10.5 | 0.979 | 0.947 | 0.906 | 0.885 | 0.996 | 0.981 | 0.973 | 0.934 | 0.985 | 0.977 | 0.941 |
| 11.0 | 0.959 | 0.900 | 0.825 | 0.787 | 0.993 | 0.963 | 0.950 | 0.877 | 0.972 | 0.957 | 0.888 |
| 11.5 | 0.941 | 0.857 | 0.754 | 0.704 | 0.990 | 0.947 | 0.929 | 0.828 | 0.960 | 0.939 | 0.841 |
| 12.0 | 0.925 | 0.818 | 0.692 | 0.633 | 0.988 | 0.932 | 0.912 | 0.784 | 0.949 | 0.922 | 0.799 |
| 12.5 | 0.910 | 0.783 | 0.638 | 0.572 | 0.985 | 0.918 | 0.896 | 0.746 | 0.938 | 0.907 | 0.761 |
| 13.0 | 0.895 | 0.750 | 0.589 | 0.518 | 0.983 | 0.905 | 0.882 | 0.712 | 0.929 | 0.893 | 0.727 |
| 13.5 | 0.882 | 0.720 | 0.546 | 0.471 | 0.981 | 0.893 | 0.870 | 0.682 | 0.920 | 0.880 | 0.695 |
| 14.0 | 0.870 | 0.692 | 0.508 | 0.430 | 0.979 | 0.882 | 0.858 | 0.655 | 0.912 | 0.868 | 0.667 |
| 14.5 | 0.858 | 0.667 | 0.473 | 0.394 | 0.977 | 0.871 | 0.849 | 0.631 | 0.905 | 0.857 | 0.641 |
| 15.0 | 0.847 | 0.643 | 0.442 | 0.362 | 0.976 | 0.861 | 0.840 | 0.609 | 0.898 | 0.846 | 0.616 |
| 15.5 | 0.836 | 0.621 | 0.414 | 0.334 | 0.974 | 0.852 | 0.831 | 0.589 | 0.891 | 0.837 | 0.594 |
| 16.0 | 0.827 | 0.600 | 0.388 | 0.308 | 0.973 | 0.843 | 0.824 | 0.571 | 0.885 | 0.828 | 0.573 |
| 16.5 | 0.817 | 0.581 | 0.365 | 0.285 | 0.971 | 0.834 | 0.817 | 0.555 | 0.879 | 0.819 | 0.554 |
| 17.0 | 0.808 | 0.563 | 0.344 | 0.265 | 0.970 | 0.826 | 0.811 | 0.540 | 0.874 | 0.811 | 0.536 |
| 17.5 | 0.800 | 0.545 | 0.324 | 0.246 | 0.969 | 0.819 | 0.806 | 0.527 | 0.869 | 0.804 | 0.519 |
| 18.0 | 0.792 | 0.529 | 0.307 | 0.229 | 0.968 | 0.812 | 0.801 | 0.514 | 0.864 | 0.797 | 0.504 |
| 18.5 | 0.784 | 0.514 | 0.290 | 0.214 | 0.967 | 0.805 | 0.796 | 0.503 | 0.860 | 0.790 | 0.489 |
| 19.0 | 0.777 | 0.500 | 0.275 | 0.200 | 0.966 | 0.798 | 0.792 | 0.492 | 0.855 | 0.784 | 0.475 |
| 19.5 | 0.770 | 0.486 | 0.261 | 0.188 | 0.965 | 0.792 | 0.788 | 0.482 | 0.851 | 0.778 | 0.463 |
| 20.0 | 0.763 | 0.474 | 0.248 | 0.176 | 0.964 | 0.786 | 0.784 | 0.473 | 0.848 | 0.772 | 0.450 |

(1) Values suitable only for IEC $A, B$ and $C$ curves.

## Protection functions

## General

Tripping curves

Standard inverse time SIT curve

## Very inverse time VIT or LTI curve

## RI curve



IEEE curves


Extremely inverse time EIT curve
Ultra inverse time UIT curve


IAC curves

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Control and monitoring functions

Maximum Sepam series 80 configuration with 3 MES120 modules: 42 inputs and 23 outputs.


## Description

Sepam performs all the control and monitoring functions required for electrical network operation:
■ the main control and monitoring functions are predefined and fit the most frequent cases of use. They are ready to use and are implemented by simple parameter setting after the necessary logic inputs / outputs are assigned.
■ the predefined control and monitoring functions can be adapted for particular needs using the SFT2841 software, which offers the following customization options: - logic equation editor, to adapt and complete the predefined control and monitoring functions
$\square$ creation of personalized messages for local annunciation
$\square$ creation of personalized mimic diagrams corresponding to the controlled devices - customization of the control matrix by changing the assignment of output relays, LEDs and annunciation messages

- with the Logipam option, Sepam can provide the most varied control and monitoring functions, programmed using the SFT2885 programming software that implements the Logipam ladder language.


## Operating principle

The processing of each control and monitoring function may be broken down into 3 phases:

- acquisition of input data:
$\square$ results of protection function processing
- external logic data, connected to the logic inputs of an optional MES120 input / output module
- local control orders transmitted by the mimic-based UMI
$\square$ remote control orders (TC) received via the communication link
- actual processing of the control and monitoring function
- utilization of the processing results:
- activation of output relays to control a device
- information sent to the facility manager:
- by message and/or LED on the Sepam display and SFT2841 software
- by remote indication (TS) via the communication link
- by real-time indications on device status on the animated mimic diagram.


## Wired logic inputs and outputs

The number of Sepam inputs / outputs must be adapted to fit the control and monitoring functions used.
The 5 outputs included in the Sepam series 80 base unit may be extended by adding 1,2 or 3 MES120 modules with 14 logic inputs and 6 output relays.
After the number of MES120 modules required for the needs of an application is set, the logic inputs are assigned to functions. The functions are chosen from a list which covers the whole range of possible uses. The functions are adapted to meet needs within the limits of the logic inputs available. The inputs may also be inverted for undervoltage type operation.
A default input / output assignment is proposed for the most frequent uses.

## GOOSE logic inputs and outputs

GOOSE logic inputs are used with the IEC 61850 communication protocol.
The GOOSE inputs are divided between the 2 GSE virtual modules with 16 logic inputs.
An example of implementing logic discrimination with GOOSE logic inputs is given on page 212.

Control and monitoring functions

This page gives the meaning of the symbols used in the block diagrams illustrating the different control and monitoring functions in this chapter.

## Logic functions

■ "OR"


Equation: $S=X+Y+Z$.

## ■ "AND"



Equation: $S=X \times Y \times Z$.

- exclusive "XOR"

$S=1$ if one and only one input is set to 1 ( $\mathrm{S}=1$ if $\mathrm{X}+\mathrm{Y}+\mathrm{Z}=1$ ).


## - Complement

These functions may use the complement of one or more input values.


Equation: $S=\bar{X}(S=1$ if $X=0)$.

## Delay timers

Two types of delay timers:
■ "on" delay timer: used to delay the appearance of a signal by a time $T$


■ "off" delay timer: used to delay the disappearance of a signal by a time $T$.


Inputs and outputs may be assigned to predefined control and monitoring functions using the SFT2841 software, according to the uses listed in the table below. The control logic of each input may be inverted for undervoltage type operation. All the logic inputs, whether or not assigned to predefined functions, may be used for the customization functions according to specific application needs:

- in the control matrix (SFT2841 software), to connect an input to a logic output, a LED on the front of Sepam or a message for local indication on the display - in the logic equation editor (SFT2841 software), as logic equation variables - in Logipam (SFT2885 software) as input variables for the program in ladder language.

Logic output ( Ox ) assignment table


Note: The logic outputs assigned by default may be freely reassigned.

## Assignment table for logic inputs (Ix) common to all

 applications| Functions | S80 | S81 | S82 | S84 | T81 | $\begin{aligned} & \text { T82 } \\ & \text { T87 } \end{aligned}$ | M87 | M81 <br> M88 | G87 | G82 <br> G88 | B80 | B83 | C86 | Assignment |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Closed circuit breaker | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ |  | $\square$ |  | $\square$ |  | $\square$ | $\square$ | $\square$ | 1101 |
| Open circuit breaker | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | 1102 |
| Synchronization of Sepam internal clock via external pulse | - | $\square$ | - | - | - | $\square$ | $\square$ | - | - | - | $\square$ | $\square$ | $\square$ | 1103 |
| Switching of groups of settings $A / B$ | $\square$ | - | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | Free |
| External reset | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | Free |
| Earthing switch closed | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | Free |
| Earthing switch open | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | Free |
| External trip 1 | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | Free |
| External trip 2 | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | Free |
| External trip 3 | $\square$ | - | $\square$ | $\square$ | - | $\square$ | $\square$ | $\square$ | $\square$ | - | - | $\square$ | $\square$ | Free |
| End of charging position | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | Free |
| Inhibit remote control (Local) | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | Free |
| SF6 pressure default | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | Free |
| Inhibit closing | $\square$ | - | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | Free |
| Open order | $\square$ | $\square$ | - | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | Free |
| closeorder | $\square$ | ! | $\square$ | $\square$ | n | $\square$ |  | $\underline{\square}$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | Free |
| Phase VT fuse blown | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | Free |
| V0 VT fuse blown | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | Free |
| External positive active energy meter | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | Free |
| External negative active energy meter | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | Free |
| External positive reactive energy meter | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | Free |
| External negative reactive energy meter | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\ldots$ | Free |
| Racked out circuit breaker | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | Free |
| Switch A closed | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | Free |
| Switch A open | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | - | $\square$ | $\square$ | Free |
| Switch B closed | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | Free |
| Switch B open |  |  |  | $\square$ |  | $\square$ |  | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | Free |
| Closing-coil monitoring |  |  |  |  |  |  |  |  |  |  |  |  |  | Free |


| Assignment table for logic inputs (Ix) common to all applications |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Functions ${ }^{\text {S80 }}$ | 580 | S8 |  | S8 | 82 | S8 |  | T81 | $\left\lvert\, \begin{aligned} & \text { T82 } \\ & \text { T87 } \end{aligned}\right.$ | M87 | $\left\|\begin{array}{l} \text { M81 } \\ \text { M88 } \end{array}\right\|$ | G87 | $\begin{aligned} & \text { G82 } \\ & \text { G88 } \end{aligned}$ | B80 | B83 | C86 | Assignment |
| Data log activation | $\square$ | $\square$ |  | $\square$ |  | $\square$ |  | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | Free |
| Phase rotation direction 123 ■ | - | $\square$ |  | $\square$ |  | $\square$ |  | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | Free |
|  | - | $\square$ |  | $\square$ |  | $\square$ |  | $\square$ | - | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | Free |
| Assignment table for logic inputs (lx) by application |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Functions |  | 0 | S8 |  | S82 | 2 | 84 | T8 | $\begin{array}{\|l\|l} \text { T82 } \\ \text { T87 } \end{array}$ | M87 | $\left\lvert\, \begin{aligned} & \text { M81 } \\ & \text { M88 } \end{aligned}\right.$ | \| G87 | G82 | B80 | B83 | C86 | Assignment |
| Inhibit recloser | $\square$ |  | $\square$ |  | $\square$ | $\square$ |  |  |  |  |  |  |  |  |  |  | Free |
| Inhibit thermal overload |  |  | $\square$ |  | $\square$ | $\square$ |  | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ |  |  | $\square$ | Free |
| Switching of thermal settings |  |  |  |  |  |  |  | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ |  |  |  | Free |
| Blocking reception 1 | $\square$ |  | $\square$ |  | $\square$ | $\square$ |  | $\square$ | $\square$ |  |  | $\square$ | $\square$ | $\square$ | $\square$ |  | Free |
| Blocking reception 2 |  |  |  |  | $\square$ | $\square$ |  |  | $\square$ |  |  | $\square$ | $\square$ |  |  |  | Free |
| Buchholz trip |  |  |  |  |  |  |  | $\square$ | $\square$ |  | $\square$ |  | $\square$ |  |  |  | Free |
| Thermostat trip |  |  |  |  |  |  |  | $\square$ | $\square$ |  | $\square$ |  | $\square$ |  |  |  | Free |
| Pressure trip |  |  |  |  |  |  |  | $\square$ | $\square$ |  | $\square$ |  | $\square$ |  |  |  | Free |
| Thermistor trip |  |  |  |  |  |  |  | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ |  |  |  | Free |
| Buchholz alarm |  |  |  |  |  |  |  | $\square$ | $\square$ |  | $\square$ |  | $\square$ |  |  |  | Free |
| Thermostat alarm |  |  |  |  |  |  |  | $\square$ | $\square$ |  | $\square$ |  | $\square$ |  |  |  | Free |
| Pressure alarm |  |  |  |  |  |  |  | $\square$ | $\square$ |  | $\square$ |  | $\square$ |  |  |  | Free |
| Thermistor alarm |  |  |  |  |  |  |  | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ |  |  |  | Free |
| Rotor speed measurement |  |  |  |  |  |  |  |  |  | $\square$ | $\square$ | $\square$ | $\square$ |  |  |  | 1104 |
| Rotor rotation detection |  |  |  |  |  |  |  |  |  | $\square$ | $\square$ |  |  |  |  |  | Free |
| Motor re-acceleration |  |  |  |  |  |  |  |  |  | $\square$ | $\square$ |  |  |  |  |  | Free |
| Load shedding request |  |  |  |  |  |  |  |  |  | $\square$ | $\square$ |  |  |  |  |  | Free |
| Inhibit undercurrent |  |  |  |  |  |  |  |  |  | $\square$ | $\square$ |  |  |  |  |  | Free |
| Trigger Motor start report |  |  |  |  |  |  |  |  |  | - | $\square$ |  |  |  |  |  | Free |
| Authorize emergency restart |  |  |  |  |  |  |  |  |  | - | $\square$ |  |  |  |  |  | Free |
| Priority genset shutdown |  |  |  |  |  |  |  |  |  |  |  | $\square$ | $\square$ |  |  |  | Free |
| De-excitation |  |  |  |  |  |  |  |  |  |  |  | $\square$ | $\square$ |  |  |  | Free |
| Close enable (ANSI 25) | $\square$ |  | $\square$ |  | $\square$ | $\square$ |  | $\square$ | $\square$ |  |  | $\square$ | $\square$ | $\square$ | $\square$ |  | Free |
| Inhibit opposite-side remote control (local) | $\square$ |  | $\square$ |  | $\square$ | $\square$ |  | $\square$ | $\square$ |  |  | $\square$ | $\square$ | $\square$ | $\square$ |  | Free |
| Inhibit remote-control coupling (local) | $\square$ |  | $\square$ |  | $\square$ | $\square$ |  | $\square$ | $\square$ |  |  | $\square$ | $\square$ | $\square$ | $\square$ |  | Free |
| Coupling open | $\square$ |  | $\square$ |  | $\square$ | $\square$ |  | $\square$ | $\square$ |  |  | $\square$ | $\square$ | $\square$ | $\square$ |  | Free |
| Coupling closed | $\square$ |  | $\square$ |  | $\square$ | $\square$ |  | - | $\square$ |  |  | $\square$ | $\square$ | $\square$ | $\square$ |  | Free |
| Opposite side open | $\square$ |  | $\square$ |  | $\square$ | $\square$ |  | $\square$ | $\square$ |  |  | $\square$ | $\square$ | $\square$ | $\square$ |  | Free |
| Opposite side closed | $\square$ |  | $\square$ |  | $\square$ | $\square$ |  | $\square$ | $\square$ |  |  | $\square$ | $\square$ | $\square$ | $\square$ |  | Free |
| Selector set to Manual (ANSI 43) | $\square$ |  | $\square$ |  | $\square$ | $\square$ |  | $\square$ | $\square$ |  |  | $\square$ | $\square$ | $\square$ | $\square$ |  | Free |
| Selector set to Auto (ANSI 43) | $\square$ |  | $\square$ |  | $\square$ | $\square$ |  | $\square$ | $\square$ |  |  | $\square$ | $\square$ | $\square$ | $\square$ |  | Free |
| Selector set to Circuit breaker (ANSI 10) | $\square$ |  | $\square$ |  | $\square$ | $\square$ |  | $\square$ | $\square$ |  |  | $\square$ | $\square$ | $\square$ | $\square$ |  | Free |
| Selector set to Coupling (ANSI 10) | $\square$ |  | $\square$ |  | $\square$ | $\square$ |  | $\square$ | $\square$ |  |  | $\square$ | $\square$ | $\square$ | $\square$ |  | Free |
| Opposite-side circuit breaker disconnected | - |  | $\square$ |  | $\square$ | $\square$ |  | $\square$ | $\square$ |  |  | $\square$ | $\square$ | $\square$ | $\square$ |  | Free |
| Coupling circuit breaker disconnected | $\square$ |  | $\square$ |  | $\square$ | $\square$ |  | $\square$ | $\square$ |  |  | $\square$ | $\square$ | $\square$ | $\square$ |  | Free |
| Coupling close order | $\square$ |  | $\square$ |  | $\square$ | $\square$ |  | - | $\square$ |  |  | $\square$ | $\square$ | $\square$ | $\square$ |  | Free |
| Opposite-side voltage OK | $\square$ |  | $\square$ |  | $\square$ | $\square$ |  | $\square$ | $\square$ |  |  | $\square$ | $\square$ | $\square$ | $\square$ |  | Free |
| Inhibit closing of coupling | $\square$ |  | $\square$ |  | $\square$ | $\square$ |  | $\square$ | $\square$ |  |  | $\square$ | $\square$ | $\square$ | $\square$ |  | Free |
| Automatic closing order | $\square$ |  | $\square$ |  | $\square$ | $\square$ |  | $\square$ | $\square$ |  |  | $\square$ | $\square$ | $\square$ | $\square$ |  | Free |
| External closing order 1 |  |  |  |  |  |  |  |  |  |  |  |  |  | $\square$ | $\square$ |  | Free |
| External closing order 2 |  |  |  |  |  |  |  |  |  |  |  |  |  | $\square$ | $\square$ |  | Free |
| Additional phase voltage transformer fuse blown |  |  |  |  |  |  |  |  |  |  |  |  |  | $\square$ | $\square$ |  | Free |
| Additional V0 voltage transformer fuse blown |  |  |  |  |  |  |  |  |  |  |  |  |  |  | $\square$ |  | Free |


|  | Assignment table for logic inputs (lx) by application |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Functions | S80 | S81 | S82 | S84 | T81 | $\left\|\begin{array}{l} \text { T82 } \\ \text { T87 } \end{array}\right\|$ | M87 | $\left\|\begin{array}{l} \text { M81 } \\ \text { M88 } \end{array}\right\|$ | G87 | $\begin{array}{\|l\|l\|} \text { G82 } \\ \text { G88 } \end{array}$ | B80 | B83 | C86 | Assignment |
| Capacitor step 1 open |  |  |  |  |  |  |  |  |  |  |  |  | $\square$ | Free |
| Capacitor step 1 closed |  |  |  |  |  |  |  |  |  |  |  |  | $\square$ | Free |
| Capacitor step 2 open |  |  |  |  |  |  |  |  |  |  |  |  | $\square$ | Free |
| Capacitor step 2 closed |  |  |  |  |  |  |  |  |  |  |  |  | - | Free |
| Capacitor step 3 open |  |  |  |  |  |  |  |  |  |  |  |  | $\square$ | Free |
| Capacitor step 3 closed |  |  |  |  |  |  |  |  |  |  |  |  | $\square$ | Free |
| Capacitor step 4 open |  |  |  |  |  |  |  |  |  |  |  |  | - | Free |
| Capacitor step 4 closed |  |  |  |  |  |  |  |  |  |  |  |  | - | Free |
| Step 1 opening order |  |  |  |  |  |  |  |  |  |  |  |  | - | Free |
| Step 2 opening order |  |  |  |  |  |  |  |  |  |  |  |  | $\square$ | Free |
| Step 3 opening order |  |  |  |  |  |  |  |  |  |  |  |  | $\square$ | Free |
| Step 4 opening order |  |  |  |  |  |  |  |  |  |  |  |  | - | Free |
| Step 1 closing order |  |  |  |  |  |  |  |  |  |  |  |  | - | Free |
| Step 2 closing order |  |  |  |  |  |  |  |  |  |  |  |  | - | Free |
| Step 3 closing order |  |  |  |  |  |  |  |  |  |  |  |  | $\square$ | Free |
| Step 4 closing order |  |  |  |  |  |  |  |  |  |  |  |  | $\square$ | Free |
| Step 1 external trip |  |  |  |  |  |  |  |  |  |  |  |  | $\square$ | Free |
| Step 2 external trip |  |  |  |  |  |  |  |  |  |  |  |  | $\square$ | Free |
| Step 3 external trip |  |  |  |  |  |  |  |  |  |  |  |  | $\square$ | Free |
| Step 4 external trip |  |  |  |  |  |  |  |  |  |  |  |  | $\square$ | Free |
| Capacitor step 1 VAR control |  |  |  |  |  |  |  |  |  |  |  |  | $\square$ | Free |
| Capacitor step 2 VAR control |  |  |  |  |  |  |  |  |  |  |  |  | $\square$ | Free |
| Capacitor step 3 VAR control |  |  |  |  |  |  |  |  |  |  |  |  | $\square$ | Free |
| Capacitor step 4 VAR control |  |  |  |  |  |  |  |  |  |  |  |  | - | Free |
| External capacitor step control inhibit |  |  |  |  |  |  |  |  |  |  |  |  | - | Free |
| Manual capacitor step control |  |  |  |  |  |  |  |  |  |  |  |  | $\square$ | Free |
| Automatic capacitor step control |  |  |  |  |  |  |  |  |  |  |  |  | - | Free |

Assignment table for GOOSE logic inputs (Gx) (IEC 61850) by application

| Functions | S80 | S81 | S82 | S84 | T81 | $\left\lvert\, \begin{aligned} & \text { T82 } \\ & \text { T87 } \end{aligned}\right.$ | M87 | $\left\lvert\, \begin{aligned} & \text { M81 } \\ & \text { M88 } \end{aligned}\right.$ | G87 | $\begin{aligned} & \text { G82 } \\ & \text { G88 } \end{aligned}$ | B80 | B83 | C86 | Assignment |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Blocking reception 1 | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ |  |  | $\square$ | $\square$ | $\square$ | $\square$ |  | Free |
| Blocking reception 2 |  |  | $\square$ | $\square$ |  | $\square$ |  |  | $\square$ | $\square$ |  |  |  | Free |
| External trip 2 | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | Free |
| Inhibit closing | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | Free |
| Load shedding request |  |  |  |  |  |  | $\square$ | $\square$ |  |  |  |  | $\square$ | Free |
| GOOSE reception fault | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | Free |
| GOOSE reception indicator | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | Free |
| Other use | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | Free |
| ACE850 presence | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | G516 |
| Data log activation | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | Free |
| Phase rotation direction 123 | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | Free |
| Phase rotation direction 132 | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | $\square$ | Free |
| Trigger Motor start report |  |  |  |  |  |  | $\square$ | $\square$ |  |  |  |  |  | Free |

Note: GOOSE IEC 61850 logic inputs/outputs can only be used with the ACE850TP or ACE850FO communication interface and only with Sepam series 80.

## Standard logic input (Ix) assignment

The table below lists the logic input (Ix) assignments obtained with the SFT2841 configuration software by clicking on the "standard assignment" button.

| Functions | Standard assignment | Application |
| :---: | :---: | :---: |
| Closed circuit breaker | 1101 | All |
| Open circuit breaker | 1102 | All |
| Blocking reception 1 | 1103 | All except M8x |
| Blocking reception 2 | 1104 | $\begin{aligned} & \text { All except } \\ & \text { S80, S81,T81, M8x, } \\ & \text { B8x, C86 } \end{aligned}$ |
| Close enable (ANSI 25) | 1104 | S80, S81, T81, B8x |
| SF6 pressure default | 1105 | All |
| Open order | 1106 | All |
| Close order | 1107 | All |
| Inhibit recloser | 1108 | S80, S81 |
| Buchholz trip | 1108 | T8x, M88, G88 |
| Thermostat trip | 1109 | T8x, M88, G88 |
| Pressure trip | 1110 | T8x, M88, G88 |
| Thermistor trip | 1111 | T8x, M88, G88 |
| Buchholz alarm | 1112 | T8x, M88, G88 |
| Thermostat alarm | 1113 | T8x, M88, G88 |
| Pressure alarm | 1114 | T8x, M88, G88 |
| Selector set to Circuit Breaker (ANSI 10) | 1201 | S8x, T8x, G8x, B8x |
| Selector set to Coupling (ANSI 10) | 1202 | S8x, T8x, G8x, B8x |
| Selector set to Auto (ANSI 43) | 1203 | S8x, T8x, G8x, B8x |
| Selector set to Manual (ANSI 43) | 1204 | S8x, T8x, G8x, B8x |
| Opposite side closed | 1205 | S8x, T8x, G8x, B8x |
| Opposite side open | 1206 | S8x, T8x, G8x, B8x |
| Opposite-side voltage OK | 1207 | S8x, T8x, G8x, B8x |
| Inhibit opposite side remote control (local) | 1208 | S8x, T8x, G8x, B8x |
| Automatic closing order | 1209 | S8x, T8x, G8x, B8x |
| Coupling open | 1210 | S8x, T8x, G8x, B8x |
| Coupling closed | 1211 | S8x, T8x, G8x, B8x |
| Inhibit closing of coupling | 1212 | S8x, T8x, G8x, B8x |
| Coupling close order | 1213 | S8x, T8x, G8x, B8x |
| Inhibit remote-control coupling (local) | 1214 | S8x, T8x, G8x, B8x |

## Standard GOOSE logic input (Gx) assignment

The table below lists the GOOSE logic input (Gx) assignments obtained with the SFT2841 configuration software by clicking on the "standard assignment" button.

| Functions | Standard assignment | Application <br> All except <br> M87, M81, M88, <br> Blocking reception 1 |
| :--- | :--- | :--- |
|  | G401 | C86 |

Any of 31 GOOSE logic inputs can be selected, from G401 to G416 and G501 to G515.

Control and monitoring functions

## Switchgear control ANSI code 94/69

## Predefined circuit breaker or contactor control function.

## Operation

The Switchgear control function can control the following types of breaking device:

- circuit breakers with shunt trip or undervoltage coils
- latching contactors with shunt trip coils

■ contactors with latched orders.

This function comprises two parts:

- processing of internal switchgear control orders:

ם open $\mathbf{1}, \mathbf{2}, 3$
$\square$ close with or without synchro-check $6,7,8$
$\square$ inhibit closing 4,5

- execution of internal orders by control logic outputs according to the type of device to be controlled.


## Processing of internal switchgear control orders

The Switchgear control function processes all breaking device closing and tripping conditions, based on:

- protection functions (configured to trip the breaking device)
- breaking device status data
- remote control via the communication link
- local control orders by logic input (Ix or Gx), or by
mimic-based UMI
■ internal control orders created by logic equation or
Logipam
■ specific predefined control functions for each
application:
- recloser
$\square$ genset shutdown, de-excitation
- load shedding
- synchro-check
- automatic transfer
- capacitor step control.

The function also inhibits breaking device closing, according to the operating conditions.

## Anti-pumping function

To prevent simultaneous breaking device open and close orders and to give priority to open orders, breaker device close orders are of the pulse type.

## Switchgear control with lockout function (ANSI 86)

The ANSI 86 function traditionally performed by lockout relays may be ensured by Sepam using the Switchgear control function, with latching of all the tripping conditions (protection function outputs and logic inputs).
Sepam performs:

- grouping of all the tripping conditions and breaking device control
- latching of the tripping order, with inhibition of closing, until the cause of tripping
disappears and is acknowledged by the user (see Latching / acknowledgement function)
- indication of the cause of tripping:
- locally by LEDs (Trip and others) and by messages on the display
- remotely by remote indications (see Indications function).


## Closing with synchro-check 9

The Synchro-check function checks the voltages upstream and downstream of a circuit breaker to ensure safe closing.
It is put into service by parameter setting.
For it to operate, one of the "Close enable" logic outputs of an MCS025 remote module must be connected to a Sepam logic input assigned to the Close enable function.
If it is necessary to close the circuit breaker without taking into account the synchronization conditions, this may be done by a logic equation or by Logipam via the V_CLOSE_NOCTRL input.

## Control of logic outputs

Logic orders from the Switchgear control function are used to control the Sepam logic outputs that control breaking device opening and closing.
Logic output control is set up to match the device to be controlled, i.e. a circuit breaker or contactor.

## Control of capacitor banks

The Sepam C86 Switchgear control function can control the breaking device and 1 to 4 capacitor step switches.
This particular function is described separately.

Control and monitoring functions

## Switchgear control ANSI code 94/69



## Control of logic outputs

Control of a circuit breaker or contactor with mechanical latching
The block diagram below represents the following parameter setting:

- type of switchgear = Circuit Breaker
- output $\mathrm{O} 1=$ trip
- output O 2 = close inhibit
- output O3 = close.


Control of a contactor without mechanical latching
The block diagram below represents the following parameter setting:
■ type of switchgear = Contactor
■ output O1 = open / close.


Control and monitoring functions

## Switchgear control ANSI code 94/69

Processing of internal switchgear control orders Block diagram


## Close enable by the Synchro-check function

## Operation

The close request, made locally or remotely, is maintained by Sepam during the close request delay and triggers the appearance of a "SYNC.IN PROCESS" message. It is deactivated when a tripping order or circuit breaker inhibition order is received and triggers the "STOP SYNC." message.

The closing order is given if the close enable is received before the close request delay runs out. When this is the case, the message "SYNC. OK" is displayed.

If the close enable is not received, the message "SYNC. FAILURE" is displayed. When possible and if the MCS025 remote module is connected by the CCA785 cord to the Sepam to which the close request has been made, an additional message indicates the type of synchronization failure:
■ "SYNC. FAILED dU" for too high a voltage difference
■ "SYNC. FAILED dF" for too high a frequency difference
■ "SYNC. FAILED dPhi" for too high a phase difference.
An additional delay is used to confirm the close enable to guarantee that the closing conditions last long enough.

Block diagram


Control and monitoring functions

## Switchgear control ANSI code 94/69

Sepam hardware |General characteristics |CTVVT sensors | CT/NT Supervisin

## Predefined control logic


-Logic discrimination
V On

SFT2841: parameter setting of Switchgear control.

Sepam hardware $\mid$ General characteristics $\mid$ CTVT sensors $\mid$ CT,
Logic input/output assignment

|  | Used | Charact. | Pulse |
| :--- | :--- | :--- | :--- |
| O1 | Yes | NO |  |
| O2 | Yes | NC |  |
| O3 | Yes | NO |  |
| O4 | No |  |  |
| O5 | Yes | NC |  |


| Pulse duration 01 | $\boxed{200} \sqrt{\mathrm{~ms}} \div \cdot$ |
| :--- | :--- | :--- |

SFT2841: default parameter setting of the logic outputs assigned to Switchgear control.

## Parameter setting

The Switchgear control function is set up and adapted to match the type of breaking device to be controlled using the SFT2841 software.

## "Control logic" tab

- activation of the Switchgear control function
- choice of the type of breaking device to be controlled: circuit breaker (by default)
or contactor
■ activation of the Synchro-check function, if necessary.
"Logic I/Os" tab
- assignment of the logic inputs required
- definition of logic output behavior.

By default, the following outputs are used:

| Logic output | Associated internal order Circuit breaker coil |  |
| :--- | :--- | :--- |
| O1 | Trip <br> (V_TRIPPED) | Shunt trip coil |
| O2 | Close inhibit <br> (V_CLOSE_INHIBITED) | Undervoltage coil |
|  | Close | Shunt trip coil |
| O3 | (V_CLOSED) |  |

■ the Trip order is always associated with output O1.
If output O1 is set up for pulse type operation, the pulse order duration may be set up

- the optional Close inhibit and Close orders may be assigned to any logic output.
"Matrix" screen, "Logic" button
Modification of the default internal order assignment to outputs O 2 and O3, if necessary.

Control and monitoring functions

Switchgear control ANSI code 94/69

## Characteristics

| Settings |  |  |  |
| :---: | :---: | :---: | :---: |
| Switchgear control |  |  |  |
| Setting range | On / Off |  |  |
| Type of device |  |  |  |
| Setting range | Circuit breaker / Contactor |  |  |
| Tripping pulse duration (output 01) |  |  |  |
| Setting range | 200 ms to 300 s |  |  |
| Accuracy ${ }^{(1)}$ | $\pm 2$ \% or from -10 ms to +25 | ms |  |
| Resolution | 10 ms or 1 digit |  |  |
| Closing with synchro-check |  |  |  |
| Setting range | On / Off |  |  |
| Close request time delay Tdf |  |  |  |
| Setting range | 0 to 300 s |  |  |
| Accuracy ${ }^{(1)}$ | $\pm 2$ \% or from -10 ms to +25 |  |  |
| Resolution | 10 ms or 1 digit |  |  |
| Synchro confirmation time delay Tcs |  |  |  |
| Setting range | 0 to 300 s |  |  |
| Accuracy (1) | $\pm 2$ \% or from -10 ms to +25 | ms |  |
| Resolution | 10 ms or 1 digit |  |  |
| Inputs |  |  |  |
| Designation | Syntax Equations | Logipam |  |
| Tripping, opening | V_TRIPCB ■ | $\square$ |  |
| Inhibit closing | V_INHIBECLOSE ■ | $\square$ |  |
| Closing | V_CLOSECB $\quad$ - | ■ |  |
| Closing without synchro-check | V_CLOSE_NOCTRL ■ | $\square$ |  |
| Outputs |  |  |  |
| Designation | Syntax Equations | Logipam | Matrix |
| Switchgear control on | V_SWCTRL_ON | ■ |  |
| Tripping, opening | V_TRIPPED ■ | $\square$ | ■ |
| Inhibit closing | V_CLOSE_INHIBITED ■ | $\square$ | $\square$ |
| Closing | V_CLOSED ■ | $\square$ | ■ |
| Contactor control | V_CONTACTOR | $\square$ | ■ |
| Synchro-check on | V_SYNC_ON | $\square$ | ■ |
| Sychrochecked close request in process | V_SYNC_INPROC | $\square$ | ■ |
| Synchrochecked close request stop | V_SYNC_STOP | $\square$ | ■ |
| Synchrochecked close request successful | V_SYNC_OK | ■ | ■ |
| Synchrochecked close request failure | V_NOSYNC | ■ | ■ |
| Synchrochecked close request failure - Voltage difference too high | V_NOSYNC_DU | ■ | ■ |
| Synchrochecked close request failure - Frequency difference too high | V_NOSYNC_DF | ■ | ■ |
| Synchrochecked close request failure - Phase difference too high | V_NOSYNC_DPHI | ■ | ■ |

## TS/TC equivalence for each protocol

| Modbus | DNP3 | IEC 60870-5-103 | IEC 61850 |
| :--- | :--- | :--- | :--- |
| TC | Binary Output | ASDU, FUN, INF | LN.DO.DA |
| TC1 | BO0 | $20,21,1$ (OFF) | CSWI1.Pos.ctIVal |
| TC2 | BO1 | $20,21,1($ ON) | CSWI1.Pos.ctIVal |
| TS | Binary Input | ASDU, FUN, INF | LN.DO.DA |
| TS233 | BI334 | $2,160,68$ | - |

Control and monitoring functions

Capacitor bank switchgear control ANSI code 94/69

Predefined function for the control of circuit breakers protecting capacitor banks and the switches of each capacitor bank step. This function only concerns Sepam C86 units.


Example of a Sepam C86 application: circuit breaker protection of a 4-step capacitor bank.

## Operation

The Sepam C86 Switchgear control function performs:
■ control of the circuit breaker protecting the capacitor bank (circuit breaker with
shunt trip or undervoltage coil)

- control of the capacitor bank step switches (maximum of 4 steps), with processing of:
$\square$ voluntary manual control orders
$\square$ automatic control orders, received from reactive-energy regulators


## Control of logic outputs

The logic orders from the Switchgear control function are used to control the Sepam logic outputs which control:

- opening and closing of the circuit breaker.
- opening and closing of each capacitor step switch.

Logic output control is set up to match the type of device to be controlled, i.e. a circuit breaker or capacitor step switch.

Control and monitoring
functions

Capacitor bank switchgear control ANSI code 94/69

Block diagram


## Control of the circuit breaker

This function comprises two parts:
■ processing of internal circuit breaker control orders:
$\square$ open circuit breaker $1,2,2$
$\square$ close circuit breaker $6,7,8$
$\square$ inhibit circuit breaker closing 4,5

- execution of internal orders by control logic outputs according to the type of device to be controlled.


## Processing of internal circuit breaker control orders

The Switchgear control function processes all the circuit breaker close and trip conditions, based on

- protection functions (configured to trip the circuit breaker)
- circuit breaker and capacitor step switch status data
- remote control orders via the communication link

■ local control orders by logic input or mimic-based UMI
■ internal control orders created by logic equation or Logipam.
The function also inhibits circuit breaker closing according to the operating conditions.

## Circuit breaker opening

- Voluntary open:

A circuit breaker open order triggers the staggered opening of capacitor step switches. This order is maintained for a time T1, the time required for the staggered opening of the capacitor step switches and the circuit breaker. The circuit breaker opens after all the capacitor step switches to avoid breaking the capacitive current. - Trip:

The protection functions (units configured to trip the circuit breaker and external protection units) send a tripping order to the circuit breaker. After the circuit breaker opens, an open order is sent to all the capacitor step switches at the same time.

## Circuit breaker closing

The circuit breaker only closes if all the capacitor step switches are open.

## Anti-pumping function

To prevent simultaneous breaking device open and close orders and to give priority to open orders, breaker device close orders are of the pulse type

## Switchgear control with lockout function (ANSI 86)

The ANSI 86 function traditionally performed by lockout relays may be provided by Sepam using the Switchgear control function, with latching of all the tripping conditions (protection function outputs and logic inputs).
Sepam performs:

- grouping of all the tripping conditions and circuit breaker control
- latching of the tripping order, with inhibition of closing, until the cause of tripping disappears and is acknowledged by the user (see Latching / acknowledgement function)
- indication of the cause of tripping:
- locally by LEDs (Trip and others) and by messages on the display
- remotely by remote indications (see Indications function).

Block diagram


## Capacitor step control

## Automatic control

When the "Automatic capacitor step control" logic input is on, each step may be controlled automatically by the reactive energy regulator (VAR). In this case, one input per step is used to open and close one capacitor step switch:

- input in state 1: closing of capacitor step $x$ switch

■ input in state 0 : opening of capacitor step x switch.

## Manual control

When the "Manual capacitor step control" logic input is on, each step may be opened and closed manually:
■ locally by specific logic inputs (one open input and one close input per step)

- remotely by remote control.

Inhibition of voluntary capacitor step control
Voluntary capacitor step switch control may be inhibited by a logic input. However, this input does not inhibit fault tripping or opening after circuit breaker opening.

## Capacitor step opening

Any opening of a capacitor step, whether voluntary or by tripping, activates a discharge time delay which inhibits closing to ensure that the step capacitors discharge correctly.
■ voluntary open: manual or automatic capacitor step switch control order

- trip, triggered by:
- ANSI 51C unbalance protection units associated with the capacitor step and configured to trip the step 13
- "Tripping of step x" logic input (one input per capacitor step) 12
$\square$ logic equation or Logipam 13 .
Latched trip orders inhibit capacitor step closing until the orders are reset 14 .
Open orders must be at least as long as the duration of open and close control pulses.

Capacitor step closing 15
Close orders are always voluntary, for manual and automatic control. They are as long as the duration of open and close control pulses.
Capacitor step switches only close after the capacitor step discharge time delay has run out and after the circuit breaker has closed, if there is no protection fault or inhibition.

## Capacitor step switch matching fault 16

This function checks that the capacitor step switch positions match, when the positions are set up on logic inputs (Ix).
In the event of a capacitor step switch matching fault, the switch close order is inhibited.

Control and monitoring
functions

Capacitor bank switchgear control ANSI code 94/69

Block diagram


Control and monitoring functions

Capacitor bank switchgear control ANSI code 94/69

Sepam hardware $\mid$ General characteristics $\mid$ CT-VT sensors $\mid$ CTNT Supervisi

## - Logic discrimination <br> 「 On

SFT2841: parameter setting of Switchgear control.

Sepam hardware $\mid$ General characteristics $\mid$ CT.VT sensors $\mid$ CT,
Logic inputooutput assignment

|  | Used | Charact. | Pulse |
| :--- | :--- | :--- | :--- |
| O1 | Yes | NO |  |
| O2 | Yes | NC |  |
| O3 | Yes | NO |  |
| $O 4$ | No |  |  |
| 05 | Yes | NC |  |

Pulse duration 01 $\sqrt{200} \sqrt{\mathrm{~ms}} \div$
SFT2841: default parameter setting of the logic outputs assigned to Switchgear control.


[^0] function.

## Parameter setting of circuit breaker control

The function is set up and adapted to match the type of circuit breaker to be controlled using the SFT2841 software.
"Control logic" tab

- activation of the Switchgear control function

■ type of device to be controlled: Circuit breaker.
"Logic I/Os" tab

- assignment of the logic inputs required
- definition of logic output behavior.

By default, the following outputs are used:

| Logic output | Associated internal order Circuit breaker coil |  |
| :--- | :--- | :--- |
| O1 | Trip <br> (V_TRIPPED) | Shunt trip coil |
| O2 | Close inhibit <br> (V_CLOSE_INHIBITED) | Undervoltage coil |
| O3 | Close <br> (V_CLOSED) | Shunt trip coil |

■ the Trip order is always associated with output O1.
If output 01 is set up for pulse type operation, the pulse order duration may be set up.

- the optional Close inhibit and Close orders may be assigned to any logic output.


## "Matrix" screen, "Logic" button

Modification of the default internal order assignment to outputs O 2 and O 3 , if necessary.

## Parameter setting of capacitor step control

The function is set up and adapted using the SFT2841 software.

## "Particular characteristics" tab

Setup of the capacitor bank, with setting of the number of steps.

## "Control logic" tab

Setup of capacitor step control:

- activation of the Capacitor step control function
- setting of capacitor step staggered opening times, capacitor step discharge times and capacitor step switch control pulse duration.


## "Logic I/Os" tab

■ assignment of the logic inputs required

- definition of the behavior of logic outputs assigned to capacitor step control.


## Characteristics

| Settings |  |
| :---: | :---: |
| Switchgear control |  |
| Setting range | On / Off |
| Type of device |  |
| Setting range | Circuit breaker / Contactor |
| Tripping pulse duration (output O1) |  |
| Setting range | 200 ms to 300 s |
| Accuracy ${ }^{(1)}$ | $\pm 2 \%$ or from -10 ms to +25 ms |
| Resolution | 10 ms or 1 digit |
| Control of capacitor banks |  |
| Setting range | On / Off |
| Staggered capacitor step opening time delay Techx (1 delay per step) |  |
| Setting range | 0 to 300 s |
| Accuracy ${ }^{(1)}$ | $\pm 2$ \% or from -10 ms to +25 ms |
| Resolution | 10 ms or 1 digit |
| Capacitor step discharge time delay Tdx (1 delay per step) |  |
| Setting range | 0 to 300 s |
| Accuracy ${ }^{(1)}$ | $\pm 2$ \% or from -10 ms to +25 ms |
| Resolution | 10 ms or 1 digit |


| Setting range | 0 to 300 s |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Accuracy ${ }^{(1)}$ | $\pm 2 \%$ or from -10 ms to +25 ms |  |  |  |
| Resolution | 10 ms or 1 digit |  |  |  |
| Inputs |  |  |  |  |
| Designation | Syntax | Equations | Logipam |  |
| Tripping, opening | V_TRIPCB | ■ | $\square$ |  |
| Inhibit closing | V_INHIBECLOSE | $\square$ | $\square$ |  |
| Closing | V_CLOSECB | - | - |  |
| Capacitor step 1 tripping | V_TRIP_STP1 |  | $\square$ |  |
| Capacitor step 2 tripping | V_TRIP_STP2 |  | - |  |
| Capacitor step 3 tripping | V_TRIP_STP3 |  | $\square$ |  |
| Capacitor step 4 tripping | V_TRIP_STP4 |  | $\square$ |  |
| Capacitor step 1 closing | V_CLOSE_STP1 |  | $\square$ |  |
| Capacitor step 2 closing | V_CLOSE_STP2 |  | $\square$ |  |
| Capacitor step 3 closing | V_CLOSE_STP3 |  | $\square$ |  |
| Capacitor step 4 closing | V_CLOSE_STP4 |  | ■ |  |
| Outputs |  |  |  |  |
| Designation | Syntax | Equations | Logipam | Matrix |
| Switchgear control on | V_SWCTRL_ON |  | $\square$ | $\square$ |
| Tripping, opening | V_TRIPPED | ■ | $\square$ | $\square$ |
| Inhibit closing | V_CLOSE_INHIBITED | - | $\square$ | $\square$ |
| Closing | V_CLOSED | - | $\square$ | $\square$ |
| Contactor control | V_CONTACTOR |  | $\square$ | $\square$ |
| Capacitor bank control on | V_BANK_ON |  | $\square$ | $\square$ |
| Tripping of capacitor step 1 | V_STP1_TRIPPING |  | $\square$ | $\square$ |
| Tripping of capacitor step 2 | V_STP2_TRIPPING |  | $\square$ | $\square$ |
| Tripping of capacitor step 3 | V_STP3_TRIPPING |  | - | $\square$ |
| Tripping of capacitor step 4 | V_STP4_TRIPPING |  | - | $\square$ |
| Closing of capacitor step 1 | V_STP1_CLOSING |  | $\square$ | $\square$ |
| Closing of capacitor step 2 | V_STP2_CLOSING |  | - | $\square$ |
| Closing of capacitor step 3 | V_STP3_CLOSING |  | - | $\square$ |
| Closing of capacitor step 4 | V_STP4_CLOSING |  | $\square$ | $\square$ |
| Capacitor step 1 matching fault | V_STP1_CTRLFLT |  | - | $\square$ |
| Capacitor step 2 matching fault | V_STP2_CTRLFLT |  | - | $\square$ |
| Capacitor step 3 matching fault | V_STP3_CTRLFLT |  | $\square$ | $\square$ |
| Capacitor step 4 matching fault | V_STP4_CTRLFLT |  | $\square$ | $\square$ |

TS/TC equivalence for each protocol

| Modbus | DNP3 | IEC 60870-5-103 | IEC 61850 |
| :--- | :--- | :--- | :--- |
| TC | Binary Output | ASDU, FUN, INF | LN.DO.DA |
| TC1 | BO0 | $20,21,1($ OFF) | CSWI1.Pos.ctIVal |
| TC2 | BO1 | $20,21,1($ ON | CSWI1.Pos.ctIVal |
| TS | Binary Input | ASDU, FUN, INF | LN.DO.DA |
| TS233 | BI334 | $2,160,68$ | - |

## Operation

The tripping outputs of all the protection functions and all the logic inputs (Ix) may be latched individually.
Logic outputs may not be latched. Logic outputs set up as pulse-type outputs maintain pulse-type operation even when they are linked to latched data.
Latched data are saved in the event of an auxiliary power failure.
All latched data are acknowledged together, at the same time. Acknowledgement is done:
■ locally on the UMI using the reser key
■ or remotely via a logic input, the SFT2841 software or via the communication link
■ or by logic equation or Logipam.
The remote indication TS5 remains present after latching operations until acknowledgement has taken place.
The Latching/acknowledgement function associated with the Switchgear control function may be used to perform the ANSI 86 Lockout relay function.

## Block diagram



## Characteristics

| Inputs |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Designation | Syntax | Equations | Logipam |  |
| Inhibition of UMI Reset key | V_INHIB_RESET_LOCAL | ■ | $\square$ |  |
| Acknowledgement by logic equation or Logipam | V_RESET | $\square$ | - |  |
| Outputs |  |  |  |  |
| Designation | Syntax | Equations | Logipam | Matrix |
| Reset requested | V_RESET_ORD |  | $\square$ |  |
| Acknowledgement by UMI Reset key | V_KEY_RESET |  | - |  |

TS/TC equivalence for each protocol

| Modbus | DNP3 | IEC 60870-5-103 | IEC 61850 |
| :---: | :--- | :--- | :--- |
| TS | Binary Input | ASDU, FUN, INF | LN.DO.DA |
| TS5 | BIO | 1,160, 19 | LLNO.LEDRs.stVal |
| TC | Binary Output | ASDU, FUN, INF | LN.DO.DA |
| TC3 | BO2 | $20,160,19$ | LLNO.LEDRs.ctIVal |

Control and monitoring functions

TC / switchgear position discrepancy Tripping

## TC / switchgear position discrepancy

## Operation

This function detects a discrepancy between the last remote control order received and the actual position of the circuit breaker or contactor.
The information is accessible in the matrix and via the remote indication TS3.

## Block diagram



Characteristics

| Outputs |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- |
| Designation | Syntax | Equations | Logipam | Matrix |
| TC/ switchgear position <br> discrepancy | V_TC/CBDISCREP |  | $\square$ |  |

TS/TC equivalence for each protocol

| Modbus | DNP3 | IEC 60870-5-103 | IEC 61850 |
| :---: | :--- | :--- | :--- |
| TC | Binary Output | ASDU, FUN, INF | LN.DO.DA |
| TC1 | BO0 | 20, 21, 1 (OFF) | CSWI1.Pos.ctIVal |
| TC2 | BO1 | 20, 21, 1 (ON) | CSWI1.Pos.ctIVal |
| TS | Binary Input | ASDU, FUN, INF | LN.DO.DA |
| TS3 | BI18 | - | - |

## Tripping

## Description

The information can be accessed via remote indication TS233.
It indicates whether a Sepam internal or external protection has tripped.
TS/TC equivalence for each protocol

| Modbus | DNP3 | IEC 60870-5-103 | IEC 61850 |
| :--- | :--- | :--- | :--- |
| TS | Binary Input | ASDU, FUN, INF | LN.DO.DA |
| TS233 | BI334 | $2,160,68$ | - |

## Operation

The recording of analog and logic signals may be triggered by different events, dependent on the control matrix parameter setting or manual action:

- triggering by the grouping of all pick-up signals of the protection functions in service
- triggering by the delayed outputs of selected protection functions
- triggering by selected logic inputs

■ triggering by selected Vx outputs (logic equations)

- manual triggering by a remote control order (TC20)
- manual triggering via the SFT2841 software tool
- manual triggering by Logipam
- triggering by selected logic inputs (Gx) (if recording configured in SFT2841
software disturbance recording screen).
Disturbance recording may be:
■ inhibited via the SFT2841 software or by remote control order (TC18) or by Logipam
■ validated via the SFT2841 software or by remote control order (TC19) or by Logipam.

Block diagram


## Characteristics

| Inputs |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Designation | Syntax | Equations | Logipam |  |
| Inhibits disturbance recording function | V_OPG_INHIBIT |  | - |  |
| Validates disturbance recording function | V_OPG_VALID |  | - |  |
| Manual trigger of disturbance recording function | V_OPG_MANUAL |  | - |  |
| Outputs |  |  |  |  |
| Designation | Syntax | Equations | Logipam | Matrix |
| Disturbance recording function triggered | V_OPG_TRIGGED |  | ■ |  |
| Disturbance recording function inhibited | V_OPG_INHIBITED |  | - | ■ |
| Disturbance recording on | V_OPG_ON |  | $\square$ |  |

TS/TC equivalence for each protocol

| Modbus | DNP3 | IEC 60870-5-103 | IEC 61850 |
| :--- | :--- | :--- | :--- |
| TC | Binary Output | ASDU, FUN, INF | LN.DO.DA |
| TC18 | BO3 | - | RDRE1.Rcdlnh.ctIVal |
| TC19 | BO4 | - | RDRE1.Rcdlnh.ctIVal |
| TC20 | BO5 | - | RDRE1.RcdTrg.ctIVal |

## Switching of groups of settings

 functions
## Operation

There are two groups of settings, group A / group B, for the phase overcurrent, earth fault, directional phase overcurrent and directional earth fault protection functions. Switching from one group of settings to another makes it possible to adapt the protection characteristics to suit the electrical environment of the application (change of earthing system, changeover to local power generation, ...). The switching of settings is global and therefore applies to all the units of the protection functions mentioned above.
The groups of settings switching mode is determined by parameter setting:
■ switching according to the position of a logic input ( $0=$ group $A, 1=$ group $B$ )
■ switching by remote control order (TC33, TC34)

- forced group A or group B.


## Block diagram



## Characteristics

| Outputs |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- |
| Designation | Syntax | Equations | Logipam | Matrix |
| Group of settings A active | V_GROUPA |  | ■ |  |
| Group of settings B active | V_GROUPB |  | $\square$ |  |

TS/TC equivalence for each protocol

| Modbus | DNP3 | IEC 60870-5-103 | IEC 61850 |
| :--- | :--- | :--- | :--- |
| TC | Binary Output | ASDU, FUN, INF | LN.DO.DA |
| TC33 | BO8 | $20,160,23$ | LLN0.SGCB |
| TC34 | BO9 | $20,160,24$ | LLNO.SGCB |

Control and monitoring
functions

## Logic discrimination Principle

## Operation

This function considerably reduces the tripping time of the circuit breakers closest to the source and may be used for logic discrimination in closed ring networks. It applies to the phase 50/51, directional phase overcurrent 67 , earth fault $50 \mathrm{~N} / 51 \mathrm{~N}$ and directional earth fault 67N overcurrent protections, definite time and IDMT.
Sepam series 80 discrimination logic comprises 2 discrimination groups. Each group includes:
■ logic thresholds: protection units that send blocking signals (BSIG) and that may be prevented from tripping by the reception of blocking signals.

- time-based thresholds: protection units that may not be prevented from tripping by blocking signals and that do not send blocking signals. They are used as backup for the logic thresholds.


## When a fault occurs:

- the logic thresholds detecting the fault send blocking signals

■ the logic thresholds detecting the fault send a tripping order if they are not inhibited by blocking signals
■ the time-based (backup) thresholds detecting the fault send a tripping order.
The sending of blocking signals lasts as long as it takes to clear the fault. If Sepam gives a tripping order, they are interrupted after a time delay that takes account of the breaking device operating time and the protection unit reset time. This system guarantees safety in downgraded operating situations (faulty wiring or switchgear).

## Example: Radial distribution with use of logic discrimination



T: protection setting time. As an approximation for definite time curves, this is assumed to be equal to the protection tripping time.

When a fault appears, the protection units that detect it inhibit the upstream protection units. The protection unit furthest downstream trips since it is not blocked by another protection unit. The delays are to be set in accordance with the device to be protected.
In this example, if the fault clearing time for the protection unit furthest downstream is $\mathrm{Xs}=0.2 \mathrm{~s}$, the fault clearing time at the source is $\mathrm{T}=\mathrm{Xs}-0.1 \mathrm{~s}=0.1 \mathrm{~s}$.

Control and monitoring functions

## Operation with logic inputs/outputs (Ix/Ox)

The assignment of protection devices between logic thresholds and time-based thresholds depends on the application and the logic input/output settings.
The first logic group is active if one of the following two conditions is fulfilled:

- blocking reception 1 is assigned to a logic input (Ix) except for motors where this input does not exist
- blocking send 1 is assigned to an output (O102 by default).

The second logic group, when present in the application, is active if one of the following two conditions is fulfilled:

- blocking reception 2 is assigned to a logic input (lx)
- blocking send 2 is assigned to an output (O103 by default).

The SFT2841 software indicates the type of thresholds, logic or time-based, according to the input/output settings.


The assignment of protection devices between the two discrimination groups is fixed and cannot be modified. When logic discrimination is used, it is important to check the concordance between the origin of the measurement and the logic discrimination group to which the unit is assigned.
By default, a single logic discrimination group has the same measurement origin. When several origins are possible, the main channels I1, I2, I3 and IO are assigned by default to the first group and the additional channels I'1, I' $2, I$ I' 3 and I' 0 to the second.
Pilot wire test
The pilot wires may be tested using the output relay test function in the SFT2841 software.

## Logic discrimination Principle

## Operation with GOOSE messages and logic inputs (Gx)

Equipped with the ACE850 interface, Sepam series 80 can be used for logic discrimination with GOOSE logic inputs and the IEC 61850 protocol on Ethernet TCP/IP.

The first logic group is active if one of the following two conditions is fulfilled: ■ blocking reception 1 is assigned to a GOOSE logic input (G401 by default), except for Sepams used in motor applications where this input does not exist $\square$ blocking send 1 is created by sending a GOOSE logic discrimination blocking message over the Ethernet network.
The second logic group, when present in the application, is active if one of the following two conditions is fulfilled:
■ blocking reception 2 is assigned to a GOOSE logic input (G402 by default)

- blocking send 2 is created by sending a GOOSE logic discrimination blocking
message over the Ethernet network.


Logic discrimination using the IEC 61850 protocol and GOOSE logic inputs (Gx)

Control and monitoring
functions

Logic discrimination
S80, S81, T81, B80 and B83
applications

Threshold assignment

| Type of protection | Unit number <br> Time-based | Send logic Group 1 | Group 2 | Reception logic |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Group 1 | Group 2 |
| 50/51 | 3,4,5,6,7,8 | 1.2 | - | 1,2 | - |
| 50N/51N | 3,4,5,6,7,8 | 1.2 | - | 1,2 | - |
| 67N ${ }^{(1)}$ | 2 | 1 | - | 1 | - |

(1) According to application.

## Characteristics

| Settings |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- |
| Activity | On / Off |  |  |  |
| Setting range |  |  |  |  |
| Outputs | Syntax | Equations | Logipam | Matrix |
| Designation | V_LOGDSC_TRIP | ■ | ■ | ■(1) |
| Logic discrimination trip | V_LOGDSC_BL1 | ■ | ■ | ■ |
| Blocking send 1 | V_LOGDSC_ON |  | $\square$ |  |
| Logic discrimination on |  |  |  |  |

(1) Only if switchgear control is not in service.

Block diagram


[^1](2) According to application.
(3) If using the ACE850 communication interface and a GOOSE logic input (IEC 61850).
(4) Condition ignored (always $=1$ ) if no input is assigned to Circuit Breaker closed.

Threshold assignment

| Type of protection | Unit number Time-based | Send logic Group 1 | Group 2 | Reception logic |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Group 1 | Group 2 |
| 50/51 | 3, 4, 5, 6, 7, 8 | 1,2 | - | - | - |
| 50N/51N | 3, 4, 5, 6, 7, 8 | 1,2 | - | - | - |
| 67 N | 2 | 1 | - | - | - |

## Characteristics

| Settings |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- |
| Activity | On / Off |  |  |  |
| Setting range |  |  |  |  |
| Outputs | Syntax | Equations | Logipam | Matrix |
| Designation | V_LOGDSC_TRIP | ■ | ■ ${ }^{(1)}$ |  |
| Logic discrimination trip | V_LOGDSC_BL1 | ■ | ■ |  |
| Blocking send 1 | V_LOGDSC_ON | ■ |  |  |
| Logic discrimination on |  |  |  |  |
| $(1)$ Only if switchgear control is not in service. |  |  |  |  |

## Block diagram



Control and monitoring functions

Logic discrimination S82, S84, T82, T87, G82, G87 and G88 applications


## (1) By default.

(2) According to application.
(3) If using the ACE850 communication interface and a GOOSE logic input (IEC 61850).
(4) Condition ignored (always $=1$ ) if no input is assigned to Circuit Breaker closed.

Control and monitoring Logic discrimination

Threshold assignment

| Type of protection | Unit number Time-based | Send logic Group 1 | Group 2 | Reception logic |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Group 1 | Group 2 |
| 50/51 | 3, 4, 7, 8 | 1,2 | 5,6 | 1,2 | 5,6 |
| 50N/51N | 3, 4, 7, 8 | 1,2 | 5,6 | 1,2 | 5,6 |
| $67{ }^{(1)}$ | - | 1 | 2 | 1 | 2 |
| $67 \mathrm{~N}{ }^{(1)}$ | - | 1 | 2 | 1 | 2 |

(1) According to application.

## Characteristics

## Settings

Activity

| Setting range On / Off   <br> Outputs    <br> Designation Syntax Equations Logipam | Matrix |  |  |
| :--- | :--- | :--- | :--- | :--- |
| Logic discrimination trip | V_LOGDSC_TRIP | ■ | ■ ${ }^{(1)}$ |
| Blocking send 1 | V_LOGDSC_BL1 | ■ | ■ |
| Blocking send 2 | V_LOGDSC_BL2 | ■ | ■ |
| Logic discrimination on | V_LOGDSC_ON | ■ |  |

(1) Only if switchgear control is not in service.

Control and monitoring functions

Logic discrimination
Example of setting: radial network

When a fault occurs in a radial network, the fault current flows through the circuit between the source and the location of the fault:

- the protection units upstream from the fault are triggered
- the protection units downstream from the fault are not triggered
- only the first protection unit upstream from the fault should trip.


## Example of setting

A 20 kV installation, supplied by a transformer, comprises the main busbars which in turn supply a feeder to a motor substation and a long feeder to a distant MV/LV transformer. The installation is earthed via a resistor at the incoming transformer neutral point, which limits to the current to about 10 Amps.


## Logic discrimination Example of setting: radial network

Based on a network coordination study, the installation relay settings are as follows:
■ incomer: Sepam T81 (relay A)

- busbar fault thresholds
$50 / 51,50 \mathrm{~N} / 51 \mathrm{~N}$ : $\mathrm{T}=0.1 \mathrm{~s}$ (DT)
Logic discrimination group 1:
- blocked by relays B and D
- blocking send 1 to high voltage relays
$\square$ backup thresholds
$50 / 51,50 \mathrm{~N} / 51 \mathrm{~N}$ : $\mathrm{T}=0.7 \mathrm{~s}$ (DT)
Time-based thresholds
■ feeder to motor substation: Sepam S80 (relay B)
- busbar fault thresholds
$50 / 51,50 \mathrm{~N} / 51 \mathrm{~N}$ : $\mathrm{T}=0.1 \mathrm{~s}$ (DT)
Logic discrimination group 1:
- blocked by relays C1 and C2
- blocking send 1 to relay A
$\square$ backup thresholds
$50 / 51,50 \mathrm{~N} / 51 \mathrm{~N}: ~ \mathrm{~T}=0.4 \mathrm{~s}$ (DT)
Time-based thresholds
■ motor feeders:
- motor 1: Sepam M81 (relay C1)
- motor fault thresholds
$50 / 51,50 \mathrm{~N} / 51 \mathrm{~N}: ~ \mathrm{~T}=0.1 \mathrm{~s}$ (DT)
Logic discrimination group 1:
- blocking send 1 to relay B
- motor 2: Sepam M87 (relay C2)
- motor fault thresholds
- $50 / 51,50 \mathrm{~N} / 51 \mathrm{~N}: ~ T=0.1 \mathrm{~s}$ (DT)

Logic discrimination group 1: blocking send 1 to relay B
Measurement origin: I1, I2, I3
-50/51 self-balancing differential scheme: $T=0 s$ (DT)
Time-based threshold
Measurement origin: $\mathrm{I}^{\prime} 1, \mathrm{I}^{\prime} 2$, $\mathrm{I}^{\prime} 3$

- transformer feeder
- cable fault thresholds

50/51, 67N: T = 0.4 s (DT)
Logic discrimination group 1:

- these thresholds are set time-wise in relation to relay E
- blocking send 1 to relay A.

The logic input and output settings for all the relays concerned are:

- blocking reception 1 on I103
- blocking send 1 on 0102

When using GOOSE logic inputs (IEC 61850), the input and output parameters are: - blocking reception 1: Each Sepam should subscribe to the GOOSE blocking message 1 gcbBasicGse (LDO/PTCR1/blkInd1) concerning it and then send this blocking GOOSE message to a GOOSE logic input (G401 by default for BSIG1).
■ blocking send 1: Each Sepam should generate a GOOSE blocking message called GOOSE Control Block standard which contains BSIG1 (gcbBasicGse (LDO/ PTRC1/blkInd1)).

For more information, refer to the Sepam IEC 61850 communication user's manual, reference SEPED306024EN.

Substations supplied by 2 (or more) parallel incomers may be protected using Sepam S82, T82 or G82, by a combination of directional phase (67) and earth fault $(67 \mathrm{~N})$ protection functions, with the logic discrimination function.

« : direction of protection function detection
4 : direction of blocking signal orders

To avoid both incomers tripping when a fault occurs upstream from one incomer, the incomer protection devices must operate as follows:

- protection function 67 of the faulty incomer detects the fault current in the "line" direction, the protection tripping direction:
- sends a blocking signal to inhibit the phase overcurrent protection functions (50/

51) of both incomers

- and initiates tripping of the incomer circuit breaker
- protection function 67 of the fault-free incomer is insensitive to fault current in the "busbar" direction.


## Example of setting

■ logic input/output assignment:

- I104: blocking reception 2 - Do not assign any inputs to blocking reception 1 - O102: blocking send 1
- protection function 67 unit 1: tripping direction $=$ line
- instantaneous output: blocking send 1
- delayed output: not blocked (no input assigned to blocking signal 1), circuit breaker tripping on faults upstream from incomer
- protection function $50 / 51$, unit 5 :
- delayed output:
- blocked by protection 67, unit 1 if there is a fault upstream from the incomer
- not blocked for busbar faults
- blocked for feeder faults
- protection function $50 / 51$, unit 3 as backup.

■ blocking send 2: Each Sepam needing to provide the BSIG2 data should generate a GOOSE blocking send 2 message.
■ blocking reception 2: Each Sepam needing the BSIG2 data should subscribe to the GOOSE blocking send 2 message available over the Ethernet TCP/IP network, then wire this GOOSE blocking message on a GOOSE logic input (G402 by default for BSIG2). Do not assign the input to BSIG1.

- blocking send 1: Each Sepam needing to provide the BSIG1 data should generate a GOOSE blocking send 1 message.
■ blocking reception 1: Each Sepam needing the BSIG1 data should subscribe to the GOOSE blocking send 1 message available over the Ethernet TCP/IP network, then wire this GOOSE blocking message on a GOOSE logic input (G401 by default for BSIG1).

No change on the protection settings:

- protection function 67, unit 1: tripping direction $=$ line
$\square$ instantaneous output: blocking send 1
$\square$ delayed output: not blocked (no input assigned to blocking signal 1), circuit breaker tripping on faults upstream from incomer
- protection function $50 / 51$, unit 5 :
- delayed output:
- blocked by protection 67, unit 1 if there is a fault upstream from the incomer
- not blocked for busbar faults
- blocked for feeder faults
- protection function 50/51, unit 3 as backup.

Control and monitoring function

Logic discrimination Example of setting:
closed ring network

Closed ring network protection may be provided by Sepam S82 or T82, which include the following functions:

- 2 units of directional phase (67) and earth fault (67N) protection functions:
- one unit to detect faults in the "line" direction
- one unit to detect faults in the "busbar" direction

■ use of 2 discrimination groups:
$\square$ sending of 2 blocking signals, according to the detected fault direction

- reception of 2 blocking signals, to block the directional protection relays according to the detection direction.


へ, 乞, direction of protection function detection
4 : direction of blocking signal orders

With the combination of directional protection functions and the logic discrimination function, the faulty section may be isolated with a minimal delay by tripping of the circuit breakers on either side of the fault.

Blocking signals are initiated by both protection functions 67 and 67N. Priority is given to protection function 67: when protection functions 67 and 67 N detect faults in opposite directions at the same time, the blocking signal sent is determined by the direction of the fault detected by protection function 67.

The instantaneous output of protection functions 67 and 67 N , activated at $80 \%$ of the Is threshold, is used to send blocking signals. This avoids uncertainty when the fault current is close to the Is threshold.

## Logic discrimination Example of setting: closed ring network

## Example of setting:

Case of a closed ring with 2 substations, each of which comprises 2 Sepam S82 relays, marked R11, R12 and R21, R22.

$\Rightarrow, \hookleftarrow \quad$ : direction of protection function detection
4 : direction of blocking signal orders

Starting at one end of the ring, the detection direction of units 1 and 2 of the directional protection functions should be alternated between line and busbars.

Example of setting of the different Sepam relays linked to logic discrimination:

## Substation 1

## Sepam S82 No. R11

- Logic input/output assignment:

I103: blocking reception 1
O102: blocking send 1
O103: blocking send 2

- $67,67 \mathrm{~N}$, unit 1 :
tripping direction = busbars
- $67,67 \mathrm{~N}$, unit 2 :
tripping direction $=$ line


## Substation 2

## Sepam S82 No. R22

■ Logic input/output assignment:
1103: blocking reception 1
I104: blocking reception 2
O102: blocking send 1
O103: blocking send 2

- $67,67 \mathrm{~N}$, unit 1 :
tripping direction = busbars
- $67,67 \mathrm{~N}$, unit 2 :
tripping direction $=$ line


## Sepam S82 No. R12

- Logic input/output assignment:

1103: blocking reception 1
104: blocking reception 2
O102: blocking send 1
O103: blocking send 2

- $67,67 \mathrm{~N}$, unit 1 :
tripping direction $=$ line
- $67,67 \mathrm{~N}$, unit 2 :
tripping direction = busbars


## Sepam S82 No. R21

- Logic input/output assignment:

1103: blocking reception 1
O102: blocking send 1
O103: blocking send 2

- $67,67 \mathrm{~N}$, unit 1 :
tripping direction = line
- $67,67 \mathrm{~N}$, unit 2 :
tripping direction = busbars

Control and monitoring functions

## Operation

Motor load shedding is done to reduce the load on the electrical network so as to keep the voltage within an acceptable range.
Load shedding may be triggered:
■ by an order from outside Sepam in the presence of a logic input assigned for the reception of load shedding orders. Orders may be delayed
■ by a voltage dip detected by the delayed output of Sepam 27D protection unit 1 (typical setting 40\% Un).
Load shedding triggers:

- tripping by the switchgear control function
- inhibition of closing as long as the load shedding order is maintained.

The load shedding order is maintained as long as one of the following three conditions is present:
■ external order via logic input (lx or Gx)

- positive sequence voltage less than load shedding voltage detected by 27D unit 1 threshold
- insufficient positive sequence voltage for a restart order to be given and detected by the delayed 27D unit 2 threshold. The time delay for the detection of correct voltage recovery must be shorter than the load shedding delay (27D unit 1) in order for the load shedding order to be maintained correctly. This unit is also used by the restart function.
The function may be validated by the switchgear closed and not racked out conditions.



## Operation

With this function, motors can be automatically restarted after a shutdown triggered by a voltage dip (load shedding).
The restart function is to be associated with the load shedding function It allows staggered restarting of process motors, as long as the voltage dip that caused load shedding was brief.
When tripping occurs due to a dip in the network supply voltage detected by 27D protection unit 1, two situations are possible:
■ the voltage dip lasts for a period longer than the maximum voltage dip duration:
tripping is final. External action is required for restart.
■ the voltage dip lasts for a period shorter than the maximum dip duration: a restart order is given. Delayed restart allows motor restart orders to be staggered to avoid network overload.
The enabling of restart is detected after the delayed output of protection 27D unit 2 drops out. This threshold allows the return of voltage to be detected independently with respect to the load shedding threshold. The typical setting is $50 \%$ Un. The restart order is given by the switchgear control function.

Block diagram


Characteristics

| Settings |  |  |  |
| :---: | :---: | :---: | :---: |
| Activity |  |  |  |
| Setting range | On / Off |  |  |
| Maximum voltage dip duration |  |  |  |
| Setting range | 0 to 300 s |  |  |
| Accuracy ${ }^{(1)}$ | $\pm 2 \%$ or from -10 ms to +25 ms |  |  |
| Resolution | 10 ms or 1 digit |  |  |
| Restart delay |  |  |  |
| Setting range | 0 to 300 s |  |  |
| Accuracy (1) | $\pm 2 \%$ or from -10 ms to +25 ms |  |  |
| Resolution | 10 ms or 1 digit |  |  |
| Outputs |  |  |  |
| Designation | Syntax Equations | Logipam | Matrix |
| Restart order | V_RESTARTING | $\square$ |  |
| Restart on | V_RESTART_ON | ■ |  |

(1) Under reference conditions (IEC 60255-6).

Example 1: Voltage dip with restart order


Example 2: Voltage dip without restart order


## Operation

This function controls shutdown of the driving machine, tripping of the breaking device and interruption of the generator excitation supply in case of:

- detection of an internal generator fault
- receipt of a genset shutdown order on a logic input or via the communication link.


Generator shutdown and tripping involve: (1)tripping of the circuit breaker connecting the machine to the network
(2) tripping of the excitation circuit breaker
(3) shutdown of the prime mover.

The combination of these three orders determines four types of shutdown and tripping orders:

- total shutdown (simultaneous tripping)
- generator tripping
- generator separation
- sequential tripping.


## Total shutdown

This type of control function gives the following orders at the same time:
■ a trip order to the generator coupling circuit breaker

- a trip order to the excitation circuit breaker
- a shutdown order to the prime mover.

This mode is reserved for internal faults in generators and transformers of generator-transformer units.

## Generator tripping

This type of control function gives the following orders:

- a trip order to the generator coupling circuit breaker
- a trip order to the excitation circuit breaker.

The prime mover is not shut down.
This mode is reserved for power network faults and allows the generator to be quickly reconnected after the fault is cleared.

## Generator separation

This type of control function gives the following order: ■ a trip order to the generator coupling circuit breaker.
The machine remains excited and the prime mover is not shut down.
This mode is used to the isolate the machine from a network which no longer meets the coupling conditions (voltage, frequency, loss of power network).
The generator may continue to supply loads locally.

## Sequential tripping

This type of control function gives the following orders on after the other:

- a trip order to the generator coupling circuit breaker
- a delayed trip order to the excitation circuit breaker
- a delayed shutdown order to the prime mover.

This mode is reserved for certain machines.
Sepam enables these operating modes by combining:
■ switchgear control for tripping of the generator coupling circuit breaker

- de-excitation function for tripping of the excitation circuit breaker - genset shutdown function to order the shutdown of the prime mover.

Function output delays are used for sequential tripping.
Typical parameter setting for industrial network generators

| Protection functions | Circuit breaker tripping | Genset shutdown | De-excitation |
| :---: | :---: | :---: | :---: |
| 12 | ■ |  |  |
| 21B | $\square$ |  |  |
| 24 | $\square$ | - | ■ |
| 27 | $\square$ |  |  |
| 32Q | $\square$ | - | ■ |
| 37P | $\square$ |  |  |
| 40 | $\square$ | - | - |
| 46 | $\square$ |  |  |
| 47 | $\square$ |  |  |
| 49RMS | - |  |  |
| 50/27 | $\square$ |  |  |
| 50/51 | $\square$ |  |  |
| $50 \mathrm{~N} / 51 \mathrm{~N}$ $50 \mathrm{G} / 51 \mathrm{G}$ | $\square$ | - | - |
| $50 \mathrm{~V} / 51 \mathrm{~V}$ | $\square$ |  |  |
| 59 | - |  |  |
| 59N | $\square$ | - | ■ |
| 64G2/27TN ${ }^{(1)}$ |  |  |  |
| 64REF | - | - | - |
| 67 | - | - | ■ |
| 67N/NC | $\square$ | - | - |
| 78PS | $\square$ |  |  |
| 81H | $\square$ |  |  |
| 81L | $\square$ |  |  |
| 81R | - |  |  |
| 87M | $\square$ | - | - |
| 87 T | $\square$ | $\square$ | - |

(1) Generally initiates an alarm, but may otherwise initiate circuit breaker tripping, genset shutdown and de-excitation.

Control and monitoring functions

## Generator shutdown and tripping Genset shutdown

## Operation

This function, available in generator applications, is used to shut down the genset:
■ mechanical shutdown by shutting down the prime mover
■ electrical shutdown by tripping the generator.
Genset shutdown may be initiated in the following ways:
■ by a external shutdown order

- remote control order if enabled
- logic input if set up

■ by logic equation or by Logipam to take into account all specific generator installation characteristics - by delayed protection functions.

The protection functions concerned are those that detect internal faults in generators or transformers of generator-transformer units. They are divided into 2 groups: protection functions that contribute to shutdown regardless of the circuit breaker position and those whose contribution is dependent on the circuit breaker position:
■ protection functions unrelated to circuit breaker position 12, 21B, 24, 27TN, 32Q, 40, 51V, 64REF, 67, 67N, 81L, 87M, 87T
$\square$ protection functions dependent on circuit breaker position 50/51, 50N/51N, 59N. The delayed, unlatched outputs of these protection units activate shutdown, only if the circuit breaker is open.
Participation in the function is to be set individually in the protection setting tabs of the SFT2841 software for each protection unit that can take part in genset shutdown.
At the same time, the function gives a tripping order via switchgear control to disconnect the generator from the power network. It must be associated with a logic output in the matrix to initiate genset shutdown.

## Block diagram



## Characteristics

| Settings |  |  |  |
| :---: | :---: | :---: | :---: |
| Activity |  |  |  |
| Setting range | On / Off |  |  |
| Selection of protection functions activating genset shutdown |  |  |  |
| Setting range per protection unit | Enabled / disabled |  |  |
| Genset shutdown time delay |  |  |  |
| Setting range | 0 to 300 s |  |  |
| Accuracy ${ }^{(1)}$ | $\pm 2 \%$ or from -10 ms to +25 ms |  |  |
| Resolution | 10 ms or 1 digit |  |  |
| Inputs |  |  |  |
| Designation | Syntax Equations | Logipam |  |
| Genset shutdown | V_SHUTDOWN ■ | - |  |
| Outputs |  |  |  |
| Designation | Syntax Equations | Logipam | Matrix |
| Genset shutdown | V_SHUTDN_ORD | - | $\square$ |
| Genset shutdown on | V_SHUTDN_ON | $\square$ |  |
| (1) Under reference conditions (IEC 60255-6). |  |  |  |
| TS/TC equivalence for each protocol |  |  |  |
| Modbus DNP3 | IEC 60870-5-103 | IEC 61850 |  |
| TC Binary Output | ASDU, FUN, INF | LN.DO.DA |  |
| TC35 BO15 | 20, 21, 102 (ON) | - |  |
| TC36 BO16 | 20, 21, 102 (OFF) | - |  |

Control and monitoring functions

Generator shutdown and tripping De-excitation

## Operation

This function, available in generator applications, is used to quickly cut off the power supply to an internal fault when the generator is disconnected from the network:

- de-excitation of the generator
- electrical shutdown by tripping.

De-excitation may be initiated in the following ways:

- by an order
- remote control order if enabled
$\square$ logic input if set up
■ by logic equation or by Logipam to take into account all specific generator installation characteristics
- by delayed protection functions.

The protection functions concerned are those that detect internal faults in generators or transformers of generator-transformer units. They are divided into 2 groups: protection functions that contribute to deexcitation regardless of the circuit breaker position and those whose contribution is dependent on the circuit breaker position:

- protection functions unrelated to circuit breaker position 12, 21B, 24, 27TN, 32Q, 40, 51V, 59, 64REF, 67, 67N.81L, 87M, 87T
- protection functions dependent on circuit breaker position 50/51, 50N/51N, 59N. The delayed, unlatched outputs of these protection units trigger de-excitation only if the circuit breaker is open.
Participation in the function is to be set individually in the protection function setting tabs of the SFT2841 software for each protection unit that can take part in de-excitation.
At the same time, the function gives a tripping order via switchgear control to disconnect the generator from the power network. It must be associated with a logic output in the control matrix to initiate the de-excitation order.


## Block diagram



## Characteristics

| Settings |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Activity |  |  |  |  |
| Setting range |  | On / Off |  |  |
| Selection of protection functions activating de-excitation |  |  |  |  |
| Setting range per protection unit |  | Enabled / disabled |  |  |
| De-excitation time delay |  |  |  |  |
| Setting range |  | 0 to 300 s |  |  |
| Accuracy ${ }^{(1)}$ |  | $\pm 2 \%$ or from -10 ms to +25 ms |  |  |
| Resolution |  | 10 ms or 1 digit |  |  |
| Inputs |  |  |  |  |
| Designation |  | Syntax Equations | Logipam |  |
| De-excitation |  | V_DE-EXCITATION ■ | ■ |  |
| Outputs |  |  |  |  |
| Designation |  | Syntax Equations | Logipam | Matrix |
| De-excitation |  | V_DE-EXCIT_ORD | - | $\square$ |
| De-excitation on |  | V_DE-EXCIT_ON | $\square$ |  |
| (1) Under reference conditions (IEC 60255-6). |  |  |  |  |
| TS/TC equivalence for each protocol |  |  |  |  |
| Modbus | DNP3 | IEC 60870-5-103 IE | EC 61850 |  |
| TC | Binary Output | ASDU, FUN, INF L | N.DO.DA |  |
| TC35 | B015 | 20, 21, 102 (ON) |  |  |
| TC36 | B016 | 20, 21, 102 (OFF) |  |  |

## Installation description

The electrical installation consists of busbars to which the following are connected:

- an incomer supplied by a 10 MVA transformer
- a 3.15 MVA power generator

In normal operation, the generator and transformer are coupled to the busbars. The generator provides backup power to the installation in the absence of the transformer power supply. The installation is earthed by a neutral point coil connected to the busbars. When the generator is not coupled to the network, its neutral is isolated. When faults occur, the generator is over-excited for 3 seconds. Its fault current is equal to 3 times its rated current. After the 3 seconds have elapsed, the fault current drops to 0.5 times the rated current.
The generator is protected:
■ against network electrical short-circuits by a phase overcurrent protection function
50/51 and a backup protection function $50 \mathrm{~V} / 51 \mathrm{~V}$

- against internal faults in generators by a generator differential protection function 87M.
- against earth faults by an earth fault protection function $50 \mathrm{~N} / 51 \mathrm{~N}$ when the generator is coupled to the busbars and by a neutral voltage displacement protection function when it is not coupled
■ against overloads by a thermal overload protection function 49RMS
- against unbalance by a negative sequence / unbalance protection function 46
- against frequency variations by underfrequency and overfrequency protection
functions 81 L and 81 H
■ against voltage variations by undervoltage and overvoltage protection functions 27 and 59
- against field loss by a protection function 40
- against loss of synchronization of the main network by a protection function 78PS.


## Setting of genset shutdown and de-excitation

The participation of these protection functions in circuit breaker tripping, genset shutdown and de-excitation depends on the type of faults detected:

- circuit breaker tripping against network faults:
- 50/51, $50 \mathrm{~V} / 51 \mathrm{~V}, 50 \mathrm{~N} / 51 \mathrm{~N}, 49 \mathrm{RMS}, 46,81 \mathrm{~L}, 81 \mathrm{H}, 27,59,78 \mathrm{PS}$
- genset shutdown for prime mover faults and internal faults:
- 50/51, 87M, 59N, 40
- de-excitation for internal faults:
- 50/51, 87M, 59N, 40.

Shutdown is total and not sequential. The genset shutdown and de-excitation time delays are zero.

Control and monitoring functions

## Automatic transfer



Automatic "one out of two" transfer.


Automatic "two out of three" transfer with synchro-check managed by Sepam series 80.

## Description

The automatic transfer function is used to transfer busbar supply from one source to another.
The function reduces busbar supply interruptions, thereby increasing the service continuity of the network supplied by the busbars.

Automatic transfer performs:
■ automatic transfer with interruption if there is a loss of voltage or a fault upstream
■ manual transfer and return to normal operation without interruption, with or without synchro-check
■ control of the coupling circuit breaker (optional)

- selection of the normal operating mode
- the necessary logic to ensure that at the end of the sequence, only 1 circuit breaker out of 2 or 2 out of 3 are closed.


## Automatic "one out of two" or "two out of three" transfer

The operation and implementation of the automatic transfer function depend on the type of substation:
■ automatic "one out of two" transfer is suitable for dual-incomer substations without coupling
■ automatic "two out of three" transfer is suitable for dual-incomer substations with coupling.
These two applications are described separately to make them easier to understand.
The automatic transfer function is symmetrical:
■ hardware symmetry: dual-incomer substations, with 2 incoming circuit breakers, and each incomer is protected by a Sepam series 80 unit

- functional symmetry: automatic transfer is distributed between the two

Sepam series 80 units protecting the two incomers.
Each of the functions is therefore described from the viewpoint of one of the two incomers, the other incomer being referred to as the "opposite side" incomer.


Automatic "two out of three" transfer with synchro-check managed by Sepam B80.

## Equipment used

## Sepam protection relay

Each incomer is protected by a Sepam series 80 unit.
At least two MES120 modules need to be added to each Sepam.
The synchro-check function (ANSI 25) is performed by an optional MCS025 module connected to one of the two Sepam units.

For busbars with motors, it is necessary to check the remanent voltage on the busbars during automatic transfer.
2 solutions are proposed:

- protection of the two incomers with Sepam B80:
- to measure the 3 phase voltages upstream of the circuit breaker and detect the loss of phase voltage
$\square$ to measure 1 additional phase voltage on the busbars and detect the presence of remanent voltage
- protection of the two incomers with another type of Sepam series 80, and checking of remanent voltage on the busbars with Sepam B21.


## Local control of automatic transfer

Local control of automatic transfer requires the following components:
■ 1 "NO circuit breaker" selector (ANSI 10), 2 or 3-position selector which designates the circuit breaker that remains open at the end of voluntary transfer without interruption
■ 1 optional "Manual / Auto" selector (ANSI 43)

- in Auto mode, automatic transfer is enabled

口 in Manual mode, automatic transfer is disabled
$\square$ when this optional selector is not included, all the automatic transfer functions are enabled.

- 1, 2 or 3 optional "Local / Remote" selectors (one selector for the function or one selector per circuit breaker)
$\square$ in Remote mode, automatic transfer on voltage loss is enabled and the other functions are disabled
- in Local mode, automatic transfer on voltage loss is disabled and the other functions are enabled
$\square$ when these optional selectors are not included, all the automatic transfer functions are enabled.
- 2 or 3 optional pushbuttons with LEDs (one pushbutton per circuit breaker):
- "Breaker closing" pushbutton
$\square$ "Closing ready" LED.


# Automatic "one out of two" transfer <br> Operation 

## Definition

Automatic "one out of two" transfer is suitable for substations with busbars supplied by two incomers with no coupling.
Automatic transfer comprises two functions:

- automatic transfer with busbar supply interruption

■ voluntary return to normal without busbar supply interruption.
The 2 functions are described separately below.


## Automatic transfer with supply interruption

Description
The function is used to transfer busbar supply from one source to the other, after the detection of voltage loss or a fault upstream of the source.

Automatic source transfer takes place in two steps:
■ tripping of the circuit breaker triggered by the detection of the loss of voltage or an external trip order (trip order from upstream protection units): loss of busbar supply ■ closing of the opposite side circuit breaker to resupply the busbars (when motors are connected to the busbars, it is necessary to check for remanent voltage on the busbars using the ANSI 27R Remanent undervoltage function).

## Compulsory transfer conditions

These conditions are always required to enable transfer:
■ the incoming circuit breaker is closed

- no phase-to-phase fault detected by the incomer on the busbars or downstream

■ no phase-to-earth fault detected by the incomer on the busbars or downstream
■ voltage OK on the opposite incomer.

## Optional transfer conditions

These conditions are required when the associated optional functions are enabled:

- the "Auto / Manual" selector is in the Auto position

■ the 2 "Local / Remote" selectors are in the Remote position
■ the 2 incoming circuit breakers are racked in
■ no VT fault detected by the VT Supervision function (ANSI 60FL), to avoid transfer
on the loss of voltage transformers
■ no inhibition of transfer by V_TRANS_STOP by logic equations or by Logipam.

## Initialization of transfer

Three events may trigger automatic transfer:

- loss of voltage detected on the incomer by the Phase undervoltage function (ANSI 27)
- or detection of a fault by the protection units upstream of the incomer, with intertripping order on the "External tripping 1" logic input
■ or V_TRANS_ON_FLT, initialization of transfer by logic equations or by Logipam.

Control and monitoring functions

## Automatic "one out of two" transfer <br> Operation

## Block diagram

Necessary conditions for transfer


## Closing of opposite side circuit breaker

The following conditions are required to order the closing of the opposite side circuit breaker:

- the circuit breaker is open
- no opposite side circuit breaker inhibit close conditions

■ no remanent voltage on the busbars (checking necessary when motors are connected to the busbars).
The opposite side circuit breaker closing order is transmitted by a Sepam logic output to a logic input of the opposite side Sepam.
It is taken into account by the Switchgear control function of the opposite side Sepam.

## Block diagram (Opposite side Sepam)



## Automatic "one out of two" transfer <br> Operation



## Voluntary return to normal without interruption

## Description

The voluntary return to normal without interruption involves two separate control functions:

- closing of the open incoming circuit breaker, with or without synchro-check:
the two incoming circuit breakers are closed
- then opening of the normally open circuit breaker, designated by the "NO circuit breaker" selector.
These two functions may also be used to transfer the busbar supply source without any interruption.


## Compulsory transfer conditions

These conditions are always required to enable transfer:

- the incoming circuit breaker is open

■ the voltage is OK upstream of the incoming circuit breaker.

## Optional transfer conditions

These conditions are required when the associated optional functions are enabled:
■ the "Auto / Manual" selector is in the Manual position
■ the 2 "Local / Remote" selectors are in the Local position
■ the 2 incomer circuit breakers are racked in
■ no VT fault detected by the VT Supervision function (ANSI 60FL), to avoid transfer on the loss of voltage transformers
■ no inhibition of transfer by V_TRANS_STOP by logic equations or by Logipam.

## Initialization of the return to normal

■ voluntary incoming circuit breaker close order.

## Closing of the open circuit breaker

## Description

Circuit breaker closing is ensured by the Switchgear control function, with or without synchro-check.

The AT function checks that all the required conditions are met and indicates to the user that the return to normal is possible.

Block diagram


Control and monitoring functions

## Automatic "one out of two" transfer <br> Operation

## Opening of the normally open circuit breaker

## Description

This function controls the opening of the circuit breaker designated as being normally open by the position of the "NO circuit breaker" selector, when the two incomer circuit breakers are closed.
It guarantees, for all the automatic control sequences that put the two sources in parallel, that at the end of the transfer, only one circuit breaker out of the two is closed.
The open order is taken into account by the Switchgear control function.

## Block diagram



Control and monitoring
functions

Automatic "one out of two" transfer
Implementation

Connection


-     -         -             -                 -                     - optional wiring.

Control and monitoring functions

## Automatic "one out of two" transfer <br> Implementation

SFT2841: parameter setting of predefined control logic.

## Parameter setting of predefined control functions

The Automatic transfer function is set up at the same time as the Switchgear control function in the "Control logic" tab of the SFT2841 software.

## Switchgear control function

- activation of the Switchgear control function
- activation of the Synchro-check function if necessary.

Automatic transfer function
■ activation of the Automatic transfer function and adjustment of associated parameters:

- voltage return time $\operatorname{Tr}$ (typically 3 s)
- normal coupling position: no coupling.

VT supervision function
The VT supervision (ANSI 60FL) is to be activated if necessary.

## Protection function setting

| Protection functions | Use | Setting information |
| :---: | :---: | :---: |
| Phase undervoltage (ANSI 27) Unit 1 | Initialization of automatic transfer on detection of voltage loss. | Voltage set point: 60\% Unp Delay: 300 ms |
| Phase overcurrent <br> (ANSI 50/51) <br> Unit 1, instantaneous output | Detection of downstream phase fault, to inhibit automatic transfer. | To be set according to discrimination study (the most sensitive set point). |
| Earth fault (ANSI 50N/51N) Unit 1, instantaneous output | Detection of downstream earth fault, to inhibit automatic transfer. | To be set according to discrimination study (the most sensitive set point). |
| Phase overvoltage (ANSI 59) Unit 1 | Detection of phase voltage upstream of the circuit breaker. <br> To be assigned to a Sepam logic output in the control matrix. | Voltage set point: 90\% Unp Delay: 3 s |
| Optional protection functions | Use | Setting information |
| Remanent undervoltage (ANSI 27R) <br> Unit 1 | Detection of no remanent voltage on the busbars to which the motors are connected. | Voltage set point: $30 \%$ Unp Delay: 100 ms |

Control and monitoring functions

## Automatic "one out of two" transfer <br> Implementation

## Logic input assignment

The logic inputs required for the AT function are to be assigned in the SFT2841 "Logic I/Os" screen.
The "Standard assignments" button proposes an assignment of the main inputs required for the AT function. The other inputs are to be assigned manually.

## Logic output assignment in the control matrix

The assignment of the logic outputs required for the AT function takes place in 2 steps:
■ declaration of the required logic outputs "Used", indicating the control mode of each output, in the SFT2841 "Logic I/Os" screen
■ assignment of each predefined output associated with the AT function to a Sepam logic output in the SFT2841 "Control matrix" screen.

The predefined outputs associated with the AT function are as follows:

| "Protection" button | Description | Use |
| :--- | :--- | :--- |
| $59-1$ | Delayed output of the Phase <br> overvoltage function (ANSI 59) <br> Unit 1 | Indication for the opposite side <br> Sepam: the voltage is OK <br> upstream of the incoming <br> circuit breaker. |
| "Logic" button | Description | Use |

Control and monitoring functions

## Automatic "one out of two" transfer <br> Characteristics

| Setting |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Activity |  |  |  |  |
| Setting range | On / Off |  |  |  |
| Voltage return time |  |  |  |  |
| Setting range | 0 to 300 s |  |  |  |
| Accuracy ${ }^{(1)}$ | $\pm 2 \%$ or from -10 ms to +25 ms |  |  |  |
| Resolution | 10 ms or 1 digit |  |  |  |
| Normal coupling position |  |  |  |  |
| Setting range | No coupling / Normally open / Normally closed |  |  |  |
| Inputs |  |  |  |  |
| Designation | Syntax | Equations | Logipam |  |
| Transfer order on fault | V_TRANS_ON_FLT | ■ | $\square$ |  |
| Transfer off order | V_TRANS_STOP | $\square$ | $\square$ |  |
| Outputs |  |  |  |  |
| Designation | Syntax | Equations | Logipam | Matrix |
| Automatic transfer on | V_TRANSF_ON |  | $\square$ | $\square$ |
| Tripping by $2 / 3$ or $1 / 2$ logic | V_2/3_TRIPPING |  | $\square$ | $\square$ |
| Tripping by automatic transfer | V_AT_TRIPPING |  | $\square$ | ■ |
| NO circuit breaker closing | V_CLOSE_NO_ORD |  | - | - |
| Breaker closing ready | V_CLOSE_EN |  | $\square$ | $\square$ |

# Automatic "two out of three" transfer <br> Operation 



Automatic transfer with normally open coupling.


Automatic transfer with normally closed coupling.

## Definition

Automatic "two out of three" transfer is suitable for substations with busbars supplied by two incomers and with coupling.
Automatic transfer comprises two functions:

- automatic transfer with busbar supply interruption

■ voluntary return to normal without busbar supply interruption.
The 2 functions are described separately below.

## Automatic transfer with supply interruption

## Description

The function is used to transfer busbar supply from one source to the other, after the detection of voltage loss or a fault upstream of the source.

Automatic source transfer takes place in two steps:
■ tripping of the circuit breaker triggered by the detection of the loss of voltage or an external trip order (trip order from upstream protection units): loss of busbar supply ■ closing of the normally open circuit breaker to resupply the busbars. According to the parameter setting, the normally open circuit breaker may be one of the following: $\square$ the coupling circuit breaker, when coupling is normally open
$\square$ the opposite side circuit breaker, when coupling is normally closed. When motors are connected to the busbars, it is necessary to check for remanent voltage on the busbars using the Remanent undervoltage function (ANSI 27R).

## Compulsory transfer conditions

These conditions are always required to enable transfer:

- the incoming circuit breaker is closed
- according to the coupling setup:
$\square$ the opposite side circuit breaker is closed and the coupling circuit breaker is open, when coupling is normally open (NO coupling)
$\square$ or the opposite side circuit breaker is open and the coupling circuit breaker is closed, when coupling is normally closed (NC coupling)
■ no phase-to-phase fault detected by the incomer on the busbars or downstream
- no phase-to-earth fault detected by the incomer on the busbars or downstream
$\square$ voltage OK on the opposite incomer.


## Optional transfer conditions

These conditions are required when the associated optional functions are enabled:

- the "Auto / Manual" selector is in the Auto position
- the 3 "Local / Remote" selectors are in the Remote position

■ the 3 circuit breakers are racked in

- no VT fault detected by the VT Supervision function (ANSI 60FL), to avoid transfer on the loss of voltage transformers
■ no inhibition of transfer by V_TRANS_STOP by logic equations or by Logipam.


## Initialization of transfer

Three events may trigger automatic transfer:

- loss of voltage detected on the incomer by the Phase undervoltage function
(ANSI 27)
■ or the detection of a fault by the protection units upstream of the incomer, with intertripping order on the "External tripping 1" logic input
■ or V_TRANS_ON_FLT, initialization of transfer by logic equations or by Logipam.

Control and monitoring functions

## Automatic "two out of three" transfer <br> Operation



## Closing of the normally open circuit breaker

The following conditions are required to order the closing of the normally open circuit breaker:

- the incoming circuit breaker is open
- no normally open circuit breaker inhibit close conditions

■ no remanent voltage on the busbars (checking necessary when motors are connected to the busbars.)
If the normally open circuit breaker is the opposite side circuit breaker: the NO circuit breaker closing order is transmitted by a Sepam logic output to a logic input of the opposite side Sepam where it is taken into account by the Switchgear control function (see block diagram below).
If the normally open circuit breaker is the coupling circuit breaker:
the NO circuit breaker closing order is transmitted by a Sepam logic output to close the circuit breaker directly, without any intermediary.

Block diagram (Opposite side Sepam)


# Automatic "two out of three" transfer <br> Operation 



Voluntary return to normal with normally closed coupling.


Voluntary return to normal with normally open coupling.


## Voluntary return to normal without interruption

## Description

The voluntary return to normal without interruption involves two separate control functions:

- closing of the open circuit breaker, with or without synchro-check: the 3 circuit breakers are closed
■ then opening of the normally open circuit breaker, designated by the "NO circuit breaker" selector.
These two functions may also be used to transfer the busbar supply source without any interruption.


## Compulsory transfer conditions

These conditions are always required to enable transfer:

- the incoming circuit breaker is open
- the opposite side circuit breaker and the coupling circuit breaker are closed
- The voltage is OK upstream of the incoming circuit breaker. This voltage is detected either by function ANSI 59, or by a processing operation in Logipam using V_TRANS_V_EN.


## Optional transfer conditions

These conditions are required when the associated optional functions are enabled:
■ the "Auto / Manual" selector is in the Manual position
■ the 3 "Local / Remote" selectors are in the Local position
$\square$ the 3 circuit breakers are racked in
■ no VT fault detected by the VT Supervision function (ANSI 60FL), to avoid transfer on the loss of voltage transformers
■ no inhibition of transfer by V_TRANS_STOP by logic equations or by Logipam.

## Initialization of the return to normal

- voluntary incoming circuit breaker close order.


## Closing of the open circuit breaker

Description
Circuit breaker closing is ensured by the Switchgear control function, with or without synchro-check.

The AT function checks that all the required conditions are met and indicates to the user that the return to normal is possible.

Block diagram


Control and monitoring functions

## Automatic "two out of three" transfer <br> Operation



Normally closed coupling.


Normally open coupling.

## Opening of the normally open circuit breaker

## Description

This function controls the opening of the circuit breaker designated as being normally open by the position of the "NO circuit breaker" selector, when the three circuit breakers are closed.
It guarantees, for all the automatic control sequences that put the two sources in parallel, that at the end of the transfer, only two circuit breakers out of the three are closed.
The open order is taken into account by the Switchgear control function.

Block diagram



# Automatic "two out of three" transfer <br> Operation 

## Coupling closing

## Description

The voluntary closing of the coupling circuit breaker without interruption involves two separate control functions:

- closing of the coupling circuit breaker, with or without synchro-check: the 3 circuit breakers are closed
■ then opening of the normally open circuit breaker, designated by the "NO circuit breaker" selector.


## Compulsory transfer conditions

These conditions are always required to enable transfer:

- the opposite side voltage is OK
- the 3 following conditions are not fulfilled simultaneously:
$\square$ the incoming circuit breaker is closed
$\square$ the opposite side circuit breaker is closed
$\square$ the coupling circuit breaker is the normally open circuit breaker (NO coupling).


## Optional transfer conditions

These conditions are required when the associated optional functions are enabled:
■ the "Auto / Manual" selector is in the Manual position

- the 3 "Local / Remote" selectors are in the Local position
- the 3 circuit breakers are racked in

■ no VT fault detected by the VT Supervision function (ANSI 60FL), to avoid transfer on the loss of voltage transformers
■ no inhibition of transfer by V_TRANS_STOP by logic equations or by Logipam.

## Initialization of coupling closing

Voluntary coupling circuit breaker close order.

Block diagram
Necessary conditions for coupling closing


Control and monitoring functions

## Automatic "two out of three" transfer <br> Implementation

Connection for normally open coupling

------ optional wiring.

## Automatic "two out of three" transfer

Implementation

Connection for normally closed coupling


Control and monitoring functions

## Automatic "two out of three" transfer <br> Implementation

## Parameter setting of predefined control functions

The Automatic transfer function is set up at the same time as the Switchgear control function in the "Control logic" tab of the SFT2841 software.

## Switchgear control function

- activation of the Switchgear control function
- activation of the Synchro-check function if necessary.

Automatic transfer function
■ activation of the Automatic transfer function and adjustment of associated parameters:
ㅁ voltage return time $\operatorname{Tr}$ (typically 3 s)

- normal coupling position: normally open or normally closed, according to the network operating mode.


## VT supervision function

The VT supervision (ANSI 60FL) is to be activated if necessary.

## Protection function setting

| Protection functions | Use | Setting information |
| :---: | :---: | :---: |
| Phase undervoltage (ANSI 27) Unit 1 | Initialization of automatic transfer on detection of voltage loss. | Voltage set point: 60\% Unp Delay: 300 ms |
| Phase overcurrent (ANSI 50/51) <br> Unit 1, instantaneous output | Detection of downstream phase fault, to inhibit automatic transfer. | To be set according to discrimination study (the most sensitive set point). |
| Earth fault (ANSI 50N/51N) Unit 1, instantaneous output | Detection of downstream earth fault, to inhibit automatic transfer. | To be set according to discrimination study (the most sensitive set point). |
| Phase overvoltage (ANSI 59) Unit 1 | Detection of phase voltage upstream of the circuit breaker. <br> To be assigned to a Sepam logic output in the control matrix. | Voltage set point: 90\% Unp Delay: 3 s |
| Optional protection functions | Use | Setting information |
| Remanent undervoltage (ANSI 27R) <br> Unit 1 | Detection of no remanent voltage on the busbars to which the motors are connected. | Voltage set point: $30 \%$ Unp Delay: 100 ms |

Control and monitoring functions

## Automatic "two out of three" transfer <br> Implementation



SFT2841: standard assignment of the inputs required for the AT function.

## Logic input assignment

The logic inputs required for the AT function are to be assigned in the SFT2841 "Logic I/Os" screen.
The "Standard assignments" button proposes an assignment of the main inputs required for the AT function. The other inputs are to be assigned manually.

## Logic output assignment in the control matrix

The assignment of the logic outputs required for the AT function takes place in 2 steps:

- declaration of the required logic outputs "Used", indicating the control mode of each output, in the SFT2841 "Logic I/Os" screen
- assignment of each predefined output associated with the AT function to a Sepam logic output in the SFT2841 "Control matrix" screen.

The predefined outputs associated with the AT function are as follows:

| "Protection" button | Description <br> 59-1 | Delayed output of the Phase <br> overvoltage function (ANSI 59) <br> Unit 1 |
| :--- | :--- | :--- |
| Uescription | Use <br> Indication for the opposite side <br> Sepam: voltage OK upstream <br> of the incoming circuit breaker. |  |
| NO circuit breaker closing | Predefined output <br> V_CLOSE_NO_ORD <br> of the AT function | Automatic closing order of <br> normally open circuit breaker. |
| Coupling closing | Predefined output <br> V_TIE_CLOSING <br> of the AT function | Coupling circuit breaker close <br> order. |
| Coupling tripping | Predefined output <br> V_TIE_OPENING <br> of the AT function | Coupling circuit breaker open <br> order. |
| Breaker closing ready | Predefined output <br> V_CLOSE_EN <br> of the AT function | LED indication: the return to <br> normal conditions are met. <br> (neglecting the synchro- <br> check) |
| Coupling closing ready | Predefined output <br> V_TIE_CLOSE_EN <br> of the AT function | LED indication: the coupling <br> close conditions are met. <br> (neglecting the synchro- <br> check) |

Control and monitoring functions

## Automatic "two out of three" transfer Characteristics

| Setting |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Activity |  |  |  |  |
| Setting range | On / Off |  |  |  |
| Voltage return time |  |  |  |  |
| Setting range | 0 to 300 s |  |  |  |
| Accuracy ${ }^{(1)}$ | $\pm 2$ \% or from -10 ms | +25 ms |  |  |
| Resolution | 10 ms or 1 digit |  |  |  |
| Normal coupling position |  |  |  |  |
| Setting range | No coupling / Normal | open / Norm | lly closed |  |
| Inputs |  |  |  |  |
| Designation | Syntax | Equations | Logipam |  |
| Transfer order on fault | V_TRANS_ON_FLT | ■ | $\square$ |  |
| Transfer off order | V_TRANS_STOP | $\square$ | $\square$ |  |
| Voltage OK upstream of the incoming circuit breaker | V_TRANS _ V_EN |  | $\square$ |  |
| Outputs |  |  |  |  |
| Designation | Syntax | Equations | Logipam | Matrix |
| Automatic transfer on | V_TRANSF_ON |  | $\square$ |  |
| Tripping by $2 / 3$ or $1 / 2$ logic | V_2/3_TRIPPING |  | $\square$ | - |
| Tripping by automatic transfer | V_AT_TRIPPING |  | $\square$ | - |
| NO circuit breaker closing | V_CLOSE_NO_ORD |  | $\square$ | - |
| Breaker closing ready | V_CLOSE_EN |  | $\square$ | $\square$ |
| Coupling tripping | V_TIE_OPENING |  | $\square$ | $\square$ |
| Coupling closing ready | V_TIE_CLOSE_EN |  | $\square$ | $\square$ |
| Coupling closing | V_TIE_CLOSING |  | $\square$ | $\square$ |
| Coupling closing with synchro-check failed | V_TIESYNCFAIL |  | $\square$ | - |

## Triggering the Motor start report (MSR)

## Operation

This function is only found in motor applications. It is used to record values specific to motors, during the starting phase.
While there is no recording in progress, recording can be triggered by:

- the "starting in progress" output of the 48/51LR protection function

■ the V_MSR_START output from the Logipam or the logic equation editor

- the remote control order TC51
- the "Trigger MSR" logic input

■ the "Trigger MSR" GOOSE logic input
Recording can be conditional upon the closed circuit breaker position.

## Block diagram



## Characteristics

| Inputs |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- |
| Designation | Syntax | Equations | Logipam | Matrix |
| Trigger MSR | V_MSR_START | ■ | ■ |  |
|  |  |  |  |  |
| Outputs |  |  |  |  |
| Designation | Syntax | Equations | Logipam | Matrix |
| MSR triggered | V_MSR_TRIGGED | $■$ | $■$ |  |

Control and monitoring functions

## Activating / Deactivating the Data log function (DLG)

## Operation

This function is found in all applications.
Depending on the chosen parameter setting, activation and deactivating the log of selected electrical values can be achieved by:
■ logic input or GOOSE type IEC 61850 logic input

- Logipam or logic equation editor

■ remote control order
■ SFT2841 software.

## Block diagram



Characteristics

| Inputs |  |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- |
| Designation | Syntax | Equations | Logipam | Matrix |  |
| DLG activation | V_DLG_START | $■$ | $\boxed{ }$ |  |  |
| Outputs |  |  |  |  |  |
| Designation | Syntax | Equations | Logipam | Matrix |  |
| DLG in progress | V_DLG_ACTIVED | $\boxed{ }$ | $\boxed{ }$ |  |  |

## Operation

This function is found in all applications.
The change of phase rotation direction can be triggered by:
■ logic input or GOOSE type IEC 61850 logic input

- remote control order (TC)

The phase rotation direction can be defined as:
■ positive sequence (123)
■ negative sequence (132)

## Block diagram



## Characteristics

| Outputs |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- |
| Designation | Syntax | Equations | Logipam | Matrix |
| Discrepancy in the phase rotation <br> direction | V_PHASE_DISC | ■ | ■ |  |
| Phase rotation direction 123 <br> activated | V_PHASE_DIR | ■ | ■ |  |
| Phase rotation direction 132 <br> activated | V_PHASE_INV | ■ | ■ |  |
| Phase rotation direction active | V_PHASE_ACTIVE | ■ | ■ |  |

## A WARNING

WARNING: protection functions inhibited for 350 ms .
Form the time it receives the change phase rotation direction request, Sepam cannot protect the electrical network for 350 ms .
This inhibition of protection functions can result in death or serious injury.

Control and monitoring functions

Local indication
ANSI code 30

## Operation

Events may be indicated locally on the front panel of Sepam by:
■ appearance of a message on the display

- switching on of one of the 9 yellow LEDs.


## Message type indication

## Predefined messages

All the messages connected to the standard Sepam functions are predefined and available in two language versions:

- in English, factory-set messages, not modifiable

■ in the local language, according to the version delivered.
The language version is chosen at the time of Sepam parameter setting. The messages are visible on the Sepam display and on the SFT2841 Alarms screen. The number and type of predefined messages depend on the type of Sepam. The table below gives the complete list of all predefined messages.

| Functions |  | English | Local language (e.g. French) |
| :---: | :---: | :---: | :---: |
| Control and monitoring ANSI code |  |  |  |
| External trip (1 to 3) |  | EXT. TRIP (1 to 3) | DECLT.EXT. (1 à 3) |
| Buchholz trip |  | BUCHH/GAS TRIP | BUCHH/GAZ DECL ${ }^{\top}$ |
| Buchholz alarm |  | BUCHHOLZ ALARM | BUCHH ALARME |
| Thermostat trip |  | THERMOS ${ }^{\text { }}$. TRIP | THERMOS ${ }^{\top}$. DECL ${ }^{\top}$. |
| Thermostat alarm |  | THERMOS ${ }^{\top}$. ALARM | THERM ${ }^{\text {OT }}$.ALARME |
| Pressure trip |  | PRESSURE TRIP | PRESSION DECL ${ }^{\text { }}$ |
| Pressure alarm |  | PRESSURE ALARM | PRESSION ALARME |
| Thermistor alarm |  | THERMISTOR AL. | THERMISTOR AL. |
| Thermistor trip |  | THERMISTOR TRIP | THERMISTOR DECL. |
| Control fault |  | CONTROL FAULT | DEFAUT COMMANDE |
| Load shedding |  | LOAD SHEDDING | DÉLESTAGE |
| Genset shutdown |  | GENSET SHUTDOWN | ARRÊT GROUPE |
| De-excitation |  | DE-EXCITATION | DÉSEXCITATION |
| Tripping order by automatic transfer |  | AUTO TRANSFER | AUTO TRANSFER |
| Phase rotation direction command complementarity fault |  | ROTATION DISC CMD | DISC CDE ROTATION |
| Diagnosis ANSI code |  |  |  |
| SF6 fault |  | SF6 LOW | BAISSE SF6 |
| MET148-2 No 1 RTD fault |  | RTD'S FAULT MET1 ${ }^{(1)}$ | DEF SONDE MET1 ${ }^{(1)}$ |
| MET148-2 No 2 RTD fault |  | RTD'S FAULT MET2 ${ }^{(1)}$ | DEF. SONDE MET2 ${ }^{(1)}$ |
| VT supervision 60FL | Phase VT supervision | VT FAULT | DEFAUT TP |
|  | Residual VT supervision | VT FAULT Vo | DEFAUT TP Vo |
| $\overline{\text { CT supervision } 60}$ | Main CT supervision | CT FAULT | DEFAUT TC |
|  | Additional CT supervision | CT' FAULT | DEFAUT TC' |
| Trip circuit supervision (TCS) fault or mismatching of open/closed position contacts |  | TRIP CIRCUIT | CIRCUIT DECL ${ }^{\top}$ |
| Closing circuit fault |  | CLOSE CIRCUIT | CIRCUIT ENCL ${ }^{\top}$ |
| Capacitor step matching fault |  | COMP. FLT. STP (1 to 4) | DEF. COMP. GR (1 à 4) |
| Cumulative breaking current monitoring |  | I ${ }^{2}$ BREAKING >> | $\Sigma^{2}$ COUPES |
| Battery monitoring |  | BATTERY LOW ${ }^{(1)}$ | PILE FAIBLE ${ }^{(1)}$ |
| Auxiliary power supply monitoring | Low threshold | LOW POWER SUP. | ALIM. SEUIL BAS |
|  | High threshold | HIGH POWER SUP. | ALIM. SEUIL HAUT |

(1) RTD FAULT, BATTERY LOW messages: refer to the maintenance chapter.

| Functions |  | English | Local language |
| :--- | :--- | :--- | :--- |
|  |  |  |  |
| Protection | ANSI code |  | (e.g. French) |

(1) With indication of the faulty phase, when used with phase-to-neutral voltage.
(2) With indication of the faulty phase.
(3) With indication of the protection unit that has initiated the cycle (phase fault, earth fault, ...).

## Personalized user messages

100 additional messages may be created using the SFT2841 software to link a message to a logic input or the result of a logic equation, for example, or to replace a predefined message by a user message.

## User message editor in SFT2841

The user message editor is included in the SFT2841 software and may be accessed in connected or disconnected mode from the control matrix screen:

- display the "Event" tab on the screen: the user messages appear
- double-click on one of the messages displayed to activate the user message editor.


## User message editor functions

- creation and modification of user messages:
- in English and the local language
- by text input or importing of an existing bitmap file (*.bmp) or by point to point drawing
- deletion of user messages
- assignment of predefined or user messages to an event defined in the control matrix:
- from the control matrix screen, "Events" tab, double-click on the event to be linked to a new message
ㅁ select the new predefined or user message from the messages presented
$\square$ "assign" it to the event.
The same message may be assigned to several events, with no limitations.


## Message display in SFT2841

■ The predefined messages are stored in Sepam's memory and are displayed in connected mode. In disconnected mode, the last messages stored in Sepam connected mode are displayed.

- The user messages are saved with the other Sepam parameters and protection settings and are displayed in connected and disconnected modes.


## Message processing on the Sepam display

When an event occurs, the related message appears on the Sepam display. The user presses the key to clear the message and enable normal consultation of all the display.
The user must press the (rese) key to acknowledge latched events (e.g. protection outputs).
The list of messages remains accessible in the alarm history ( $\$$ key), in which the last 16 messages are stored. The last 250 messages may be consulted with the SFT2841 software.
To delete the messages stored in the alarm history:

- display the alarm history on the display
- press the clear key.


## LED indication

The 9 yellow LEDs on the front of Sepam are assigned by default to the following events:

| LED | Event | Name on label <br> on front panel |
| :--- | :--- | :--- |
| LED 1 | Tripping of protection $50 / 51$ unit 1 | $\mathrm{l}>51$ |
| LED 2 | Tripping of protection $50 / 51$ unit 2 | $\mathrm{l} \gg 51$ |
| LED 3 | Tripping of protection $50 \mathrm{~N} / 51 \mathrm{~N}$ unit 1 | lo $>51 \mathrm{~N}$ |
| LED 4 | Tripping of protection $50 \mathrm{~N} / 51 \mathrm{~N}$ unit 2 | lo >>51N |
| LED 5 |  | Ext |
| LED 6 |  |  |
| LED 7 | Circuit breaker open (I102) | 0 Off |
| LED 8 | Circuit breaker closed (I101) | I On |
| LED 9 | Tripping by circuit breaker control | Trip |

The default parameter setting may be personalized using the SFT2841 software:

- LEDs are assigned to events in the "LEDs" tab of the control matrix screen
- editing and printing of personalized labels are proposed in the general
characteristics screen.


Local control using the mimic-based UMI

## Description

Switchgear may be controlled locally using Sepam series 80 units equipped with the mimic-based UMI.
The control functions available are:

- selection of the Sepam control mode
- viewing of device status on the animated mimic diagram
- local control of the opening and closing of all the devices controlled by Sepam


## Selection of the Sepam control mode

A key-switch on the front of the mimic-based UMI is used to select the Sepam control mode. Three modes are available: Remote, Local or Test.

In Remote mode:

- remote control orders are taken into account

■ local control orders are disabled, with the exception of the circuit breaker open order.
Remote mode is indicated by the variable V_MIMIC_REMOTE $=1$.
In Local mode:
■ remote control orders are disabled, with the exception of the circuit breaker open order.

- local control orders are enabled.

Local mode is indicated by the variable V_MIMIC_LOCAL $=1$.
Test mode should be selected for tests on equipment, e.g. during preventive maintenance operations:
■ all functions enabled in Local mode are available in Test mode
■ no time-tagged events are sent by the communication link.
Test mode is indicated by the variable V_MIMIC_TEST $=1$.
The Logipam programming software can be used to customize control-mode processing.

## Mimic diagram and symbols

A mimic diagram or single-line diagram is a simplified diagram of an electrical installation. It is made up of a fixed background on which symbols and measurements are placed.
The mimic diagram editor integrated in the SFT2841 software may be used to personalize and setup mimic diagrams.

The symbols making up the mimic-diagram constitute the interface between the mimic-based UMI and the other Sepam control functions.
There are three types of symbols:
■ fixed symbol: represents the electrotechnical devices that are neither animated or controlled, e.g. a transformer
■ animated symbol with one or two inputs: represents the electrotechnical devices that change on the mimic diagram, depending on the symbol inputs, but cannot be controlled via the Sepam mimic-based UMI.
This type of symbol is used for switch-disconnectors without remote control, for example.
■ controlled symbol with one or two inputs/outputs: represents the electrotechnical devices that change on the mimic diagram, depending on the symbol inputs, and can be controlled via the Sepam mimic-based UMI.
This type of symbol is used for circuit breakers, for example.
The symbol outputs are used to control the electrotechnical device:
$\square$ directly via the Sepam logic outputs
$\square$ by the switchgear control function
$\square$ by logic equations or the Logipam program.

## Symbol animation

Depending on the value of their inputs, symbols change. A graphic representation corresponds to each state. Animation is carried out automatically by changing the symbol each time the state changes.
The symbol inputs must be assigned directly to the Sepam inputs indicating the position of the symbolized switchgear.

## Animated symbols with one input

"Animated -1 input" and "Controlled -1 input/output" symbols are animated symbols with one input. The value of the input determines the state of the symbol:
■ input set to $0=$ inactive
■ input set to 1 = active
This type of symbol is used for simple presentation of information, for example the racked out position of a circuit breaker.

| Symbol inputs | Symbol state | Graphic representation <br> (example) |
| :--- | :--- | :--- |
| Input $=0$ | Inactive |  |
| Input $=1$ | Active |  |

## Animated symbols with two inputs

"Animated - 2 inputs" and "Controlled - 2 inputs/outputs" symbols are animated symbols with two inputs, one open and the other closed.
This is the most common situation in representing switchgear positions.
The symbol has three states, i.e. three graphic representations: open, closed and unknown.
The latter is obtained when the inputs are not matched, in which case it is impossible to determine the position of the switchgear.

| Symbol inputs | Symbol state | Graphic representation <br> (example) |
| :--- | :--- | :--- |
| Input 1 (open) $=1$ <br> Input 2 (closed) $=0$ | Open |  |
| Input 1 (open) $=0$ <br> Input 2 (closed) $=1$ | Closed |  |
| Input 1 (open) $=0$ <br> Input 2 (closed) $=0$ | Unknown |  |
| Input 1 (open) $=1$ <br> Input 2 (closed) $=1$ | Unknown |  |

## Local control using a symbol

"Controlled - 1 input/output" and "Controlled - 2 inputs/outputs" symbols are used to control the switchgear corresponding to the symbol via the Sepam mimic-based UMI.

## Control symbols with two outputs

"Controlled - 2 inputs/outputs" symbols have two control outputs for opening and closing of the symbolized device.
An order on the mimic-based UMI sends a 300 ms pulse on the controlled output.

## Control symbols with one output

"Controlled - 1 input/output" symbols have one control output. The output remains in the last state to which it was ordered.
A new order results in a change in the output state.

## Inhibition of orders

"Controlled - 1 input/output" and "Controlled - 2 inputs/outputs" symbols have two inhibition inputs that, when set to 1 , block opening and closing orders. This makes it possible to create interlocking systems or other order-disabling systems that are taken into account by the UMI.

## Symbol inputs/outputs

Depending on the desired operation of the mimic-based UMI, Sepam variables must be assigned to the inputs of animated symbols and the inputs/outputs of controlled symbols.

| Sepam variables assigned to symbol inputs |  |  |  |
| :---: | :---: | :---: | :---: |
| Sepam variables |  | Name | Use |
| Logic inputs |  | Ixxx | Symbol animation directly based on device positions |
| Outputs of predefined functions | Switchgear control | V_CLOSE_INHIBITED | Circuit-breaker operation disabled |
|  | Position of key on the front panel of Sepam | V_MIMIC_LOCAL, <br> V_MIMIC_REMOTE, <br> V_MIMIC_TEST | Representation of key position Operation disabled depending on the control mode |
|  | Logic equations or Logipam program | V_MIMIC_IN_1 to <br> V_MIMIC_IN_16 | Representation of Sepam internal status conditions Cases where operation is disabled |
| Sepam variables to be assigned to symbol outputs |  |  |  |
| Sepam variables |  | Name | Use |
| Logic outputs |  | Oxxx | Direct control of devices |
| Inputs of predefined functions | Switchgear control | V_MIMIC_CLOSE_CB <br> V_MIMIC_OPEN_CB | Circuit-breaker control using the switchgear-control function via the mimic-based UMI |
|  | Logic equations or Logipam program | V_MIMIC_OUT1 to <br> V_MIMIC_OUT16 | Order processing by logic functions: interlocking, order sequence, etc. |

## Block diagram

The block diagrams below present the functions ensured by the controlled symbols, based on two examples.
Voluntary user control orders (selection of the device to be controlled in the mimic diagram and action on a control key) are represented in the block diagrams by the following icons:
(O) : open order
(I): close order


SFT2841: example of the logic input / output assignment of a symbol with two outputs.


SFT2841: example of the logic input / output assignment of a symbol with one output.

Local control using symbols with two outputs


## Local control using a symbol with one output

## Description

The control matrix is used for simple assignment of the logic outputs and LEDs to data produced by the protection functions, control logic and logic inputs. Each column creates a logic OR between all the lines selected.
The matrix may also be used to display the alarms associated with the data. It guarantees the consistency of the parameter setting with the predefined functions. The following data are managed in the control matrix and may be set using the SFT2841 software tool.

## Control matrix inputs

| "Protection" button | Meaning | Comments |
| :---: | :---: | :---: |
| All application protection functions | Protection tripping output and additional outputs when applicable |  |
| "Inputs" button |  |  |
| Logic inputs I101 to I114 | According to configuration | If first MES120 module is configured |
| Logic inputs I201 to I214 | According to configuration | If second MES120 module is configured |
| Logic inputs I301 to I314 | According to configuration | If third MES120 module is configured |
| "Equations" button | Meaning | Comments |
| V1 to V20 | Logic equation editor outputs |  |
| "Logipam" button | Meaning | Comments |
| MAT001 to MAT128 | Logipam output variables to the control matrix | Only the variables actually used in the Logipam program are displayed |
| "Logic" button | Meaning | Comments |
| Switchgear control |  |  |
| Closing | Closing by switchgear control function | By default on O3. Only available if switchgear control is in circuit breaker mode |
| Tripping | Tripping by switchgear control function | Forced on O1, if switchgear control is in circuit breaker mode |
| Inhibit closing | Inhibition by switchgear control function | By default on O2. Only available if switchgear control is in circuit breaker mode |
| Contactor control | Contactor control | Forced on O1, if switchgear control is in circuit breaker mode |
| Pick-up | Logic OR of the instantaneous output of all protection units with the exception of protection units <br> 38/49T, 48/51LR, 49RMS, 64G2/27TN, 66. |  |
| Drop-out | A protection unit time delay counter has not yet gone back to 0 . |  |
| Logic discrimination |  |  |
| Logic discrimination trip | Tripping order sent by logic discrimination function | Only when logic discrimination function is used without switchgear control function |
| Blocking send 1 | Sending of blocking signal to next Sepam in logic discrimination chain 1 | By default on O102. |
| Blocking send 2 | Sending of blocking signal to next Sepam in logic discrimination chain 2 | By default on O103 |
| Motor/generator control |  |  |
| Load shedding | Sending of a load shedding order | Motor application |
| Genset shutdown | Sending of a prime mover shutdown order | Generator application |
| De-excitation | Sending of a de-excitation order | Generator application |
| Recloser |  |  |
| Recloser in service | The recloser is in service |  |
| Reclosing successful | The recloser has successfuly reclosed | Pulse type output |
| Permanent trip | The circuit breaker is permanently open after the reclosing cycles | Pulse type output |
| Recloser ready | The recloser is ready to operate |  |
| Recloser cycle 1 | Cycle 1 in progress |  |
| Recloser cycle 2 | Cycle 2 in progress |  |
| Recloser cycle 3 | Cycle 3 in progress |  |
| Recloser cycle 4 | Cycle 4 in progress |  |
| Closing by recloser | A closing order is given by the recloser |  |
| "GOOSE" button | Meaning | Comments |
| Logic inputs G401 to G416 and G501 to G516 | According to configuration | Only with ACE850 configured |


| "Logic" button | Meaning | Comments |
| :---: | :---: | :---: |
| Diagnosis |  |  |
| TCS fault | Trip circuit fault |  |
| CCS fault | Closing circuit fault |  |
| TC / breaker position discrepancy | Discrepancy between the last state ordered by the remote monitoring and control system and the position of the circuit breaker |  |
| Breaker monitoring | A circuit breaker or contactor open or close order has not been executed |  |
| Reverse phase rotation | Reverse voltage rotation due to a wiring error |  |
| Additional-phase reverse rotation | Reverse rotation of additional phase voltages due to a wiring error |  |
| Disturbance recording inhibited | Disturbance recording inhibited |  |
| Cumulative breaking current monitoring | Overshooting of the cumulative breaking current set point |  |
| Low auxiliary voltage threshold | The auxiliary voltage is below the low threshold |  |
| High auxiliary voltage threshold | The auxiliary voltage is above the high threshold |  |
| Low battery fault | Battery low or absent |  |
| MET148-2 No 1 fault MET148-2 No 2 fault | Hardware problem on an MET 148-2 module (module 1 or 2) or on an RTD |  |
| Watchdog | Monitoring of Sepam operation | Always on O 5 if used |
| CT supervision |  |  |
| Main CT fault | I current input CT fault |  |
| Additional CT fault | I' current input CT fault |  |
| VT supervision |  |  |
| Main VT fault, phase channel | V voltage input phase VT fault |  |
| Main VT fault, residual channel | V0 voltage input residual VT fault |  |
| Additional VT fault, phase channel | V' voltage input phase VT fault |  |
| Additional VT fault, residual channel | V'0 voltage input residual VT fault |  |
| Synchro-check |  |  |
| Closing with synchro-check | Circuit breaker close request with synchro-check by the ANSI 25 function has been initiated | Switchgear control with synchro-check function |
| Closing with synchro-check completed | Breaker closing with synchro-check by the ANSI 25 function successful | Switchgear control with synchro-check function |
| Closing failed, out-of-sync | Synchronism conditions too short to enable breaker closing | Switchgear control with synchro-check function |
| Closing failed, out-of-sync, cause dU | Breaker closing inhibited because sources are out-ofsync due to an excessive voltage difference | Switchgear control with synchro-check function |
| Closing failed, out-of-sync, cause dPHI | Breaker closing inhibited because sources are out-ofsync due to an excessive phase difference | Switchgear control with synchro-check function |
| Closing failed, out-of-sync, cause dF | Breaker closing inhibited because sources are out-ofsync due to an excessive frequency difference | Switchgear control with synchro-check function |
| Stop closing with synchro-check | A synchrochecked circuit breaker close request has been interrupted | Switchgear control with synchro-check function |
| Automatic transfer |  |  |
| Coupling closing with synchro-check failed | The coupling close request initiated by automatic transfer has failed because the sources are out-of-sync |  |
| Tripping by automatic transfer | Breaker tripping initiated by automatic transfer (tripping is performed by the switchgear control function) |  |
| Tripping by $2 / 3$ or $1 / 2$ logic | Breaker tripping initiated by $2 / 3$ or $1 / 2$ logic (tripping is performed by the switchgear control function) |  |
| NO circuit breaker closing | Normally open circuit breaker close order for automatic transfer function |  |
| Breaker closing ready | Indication that breaker closing is possible to return to normal operation |  |
| Coupling closing | Coupling closing order for automatic transfer function |  |
| Coupling closing ready | Indication that coupling closing is possible to return to normal operation |  |
| Coupling tripping | Coupling tripping order for automatic transfer function |  |
| Control of capacitor banks |  |  |
| Tripping of capacitor step x | Capacitor step x tripping output |  |
| Closing of capacitor step x | Capacitor step x closing output |  |
| Capacitor step x position fault | Capacitor step x positions mismatched |  |
| Automatic capacitor step control | Capacitor steps in automatic control mode |  |
| Manual capacitor step control | Capacitor steps in manual control mode |  |

Control and monitoring functions

## Logic equations

Adaptation of the predefined control and monitoring functions by the addition of simple logic functions.

## Use

This function may be used to configure simple logic functions by combining data received from the protection functions, logic inputs, remote control orders or the mimic-based UMI.
GOOSE logic inputs (Gx) available with the IEC 61850 protocol are not managed. By using logic operators (AND, OR, XOR, NOT) and timers, new processing operations and indications may be added to the existing ones.
The logic functions produce outputs that may be used:

- in the matrix to control output relays, switch on a LED or display new messages
- in the protection functions to create, for example, new inhibit or reset conditions
- in the main predefined control and monitoring functions to complete processing operations or add new cases of tripping or genset shutdown, for example - for mimic diagram animation.



## Logic function configuration



SFT2841: logic equation editor.
Editing assistance


SFT2841: data input assistance tool.

Logic functions are entered in text format in the SFT2841 equation editor. Each line includes a logic operation, the result of which is assigned to a variable.
Example:
V1 = P5051_2_3 OR I102.
The variable V 1 is assigned the result of the logic OR operation involving the value from protection function 50/51 and logic input I102.
The variables may be used for other operations or as outputs to produce actions in the control matrix, protection functions or predefined control and monitoring functions.
A program is a series of lines executed sequentially every 14 ms .
A data input assistance tool provides quick access to each of the equation editor operators and variables.

## Description of operations

## Operators

■ =: assignment of a result
V2 = VL3 //V2 is assigned the value of VL3

- NOT: logic inversion

VL1 = NOT VL2 // VL1 is assigned the opposite logic state of VL2

- OR: logic OR

V1 = VL3 OR I103 // V1 is assigned state 1 if VL3 or IO3 are in state 1

- AND: logic AND

VV3 = VL2 AND VV1 // VV3 is assigned state 1 if VL2 and VV3 are in state 1
■ XOR: exclusive OR
V3 = VL1 XOR VL2 // V3 is assigned state 1 if only one of the variables VL1 or VL2 is in state 1.
This is equivalent to V3 = (V1 AND (NOT V2)) OR (V2 AND (NOT V1))
■ II: commentary
The characters on the right are not processed

- (,): the operations may be grouped between brackets to indicate the order in which they are carried out
V1 = (VL3 OR VL2) AND 1213.



## Functions

■ $\mathrm{x}=\mathbf{S R}(\mathrm{y}, \mathrm{z})$ : bistable with priority to Set
$x$ is set to 1 when $y$ is equal to 1
x is set to 0 when z is equal to 1 (and y is equal to 0 )
otherwise x is not changed.
V1 $=\mathbf{S R}(1104$, I105) // I104 sets V1 to 1, I105 sets V1 to 0
■ LATCH $(x, y, \ldots)$ : latching of variables $x, y, \ldots$
The variables are maintained constantly at 1 after being initially set. They are reset to 0 when Sepam is reset (reset button, external input or remote control order).
The LATCH function accepts as many parameters as the number of variables that the user wishes to latch.
It applies to the entire program, whatever the position of LATCH in the program. For easier reading, it is advisable to put it at the start of the program.
LATCH(V1, VL2, VV3) // V1, VL2 and VV3 are latched, ie. once they are set to 1, only a Sepam reset can set them back to 0
■ $x=\operatorname{TON}(y, t)$ : "on" delay timer
The variable x goes to 1 t ms after variable y goes to 1 .
V1 = TON(I102.2000) // used to filter input I102 which must be present for // 2 s to be taken into account in V1

■ $x=\operatorname{TOF}(y, t)$ : "off" delay timer.
The variable x goes to 0 t ms after variable y goes to 0 .
VL2 $=$ TOF(VL1, 100) // VL2 stays at 1 for 100 ms after VL1

$$
/ / \text { goes back to } 0
$$

■ $\mathrm{x}=$ PULSE(s, $\mathrm{i}, \mathrm{n})$ : time-tagger
Used to generate $n$ periodic pulses, separated by an interval $i$ as of the starting time $s$ $s$ is expressed in hours:minutes:seconds
$i$ is expressed in hours:minutes:seconds
n is a whole number ( $\mathrm{n}=-1$ : repeated until the end of the day).
V1 = PULSE (8:30:00, 1:0:0.4) will generate 4 pulses at 1-hour intervals at $8 \mathrm{~h} 30,9 \mathrm{~h} 30,10 \mathrm{~h} 30$ and 11 h 30 . This will be repeated every 24 hours. The pulses last for a 14 ms cycle. V1 is assigned the value of 1 during the cycle. If necessary, V1 may be extended using the TOF, SR or LATCH functions.

## Timer values

A timer editor is used to give a name and value to each timer. The name may then be used in the TON and TOF functions. The timer value may therefore be adjusted without changing the program content.
V1 = TON (VL1, start) // start set to 200 ms in the timer editor.
Maximum number of functions
The number of time delays (TON, TOF) and time-taggers (PULSE) is globalized and may not be more than 16 .
There is no limitation for the SR and LATCH functions.

## Description of variables

■ input variables: they come from the protection functions, logic inputs or predefined control functions. They may only appear on the right of the = sign
$\square$ output variables: they are produced by the equation editor to generate actions in the matrix, protection functions or predefined control functions

- local variables: they are intended for intermediary calculations and are not available outside the logic equation editor.

| Input variables |  |  |
| :---: | :---: | :---: |
| Type | Syntax | Example, meaning |
| Logic inputs | Ixxx | 1101: input 1 of MES120 No 1 module I312: input 12 of MES120 No 3 module |
| Protection function outputs | ```Pnnnn_x_y nnnn: ANSI code x : unit y: data``` | P50/51_2_1: Protection 50/51, unit 2, delayed output. The protection function output data numbers are given in the characteristics of each function and may be accessed using the data input assistance tool. |
| Remote control orders | TC1 to TC64 | Pulse type value (duration of one 14 ms cycle) of remote control orders received |
| Predefined control function outputs | V_TRIPPED | Tripping order present at switchgear control function output |
|  | V_CLOSE_INHIBITED | Inhibit closing order present at switchgear control function output |
|  | V_CLOSED | Closing order present at switchgear control function output |
| Phase rotation direction management functions output | V_PHASE_DIR | The phase rotation direction 123 command is active |
|  | V_PHASE_INV | The phase rotation direction 132 command is active |
|  | V_PHASE_DISC | The phase rotation direction commands are not complementary after more than 2 s |
| Mimic-based UMI outputs | V_MIMIC_OUT_1 to <br> V_MIMIC_OUT_16 | Variables that may be assigned to the mimic diagram symbol outputs and that change values when control orders are transmitted from the mimic-based UMI |
|  | V_MIMIC_LOCAL <br> V_MIMIC_TEST, <br> V_MIMIC_REMOTE | Position of the key on the mimic-based UMI |
| Output variables |  |  |
| Type | Syntax | Example, meaning |
| Outputs to matrix | V1 to V20 | They may initiate LEDs, logic outputs or messages in the matrix. |
| Protection function inputs | Pnnnn_x_y <br> nnn: ANSI code <br> $x$ : unit <br> $y$ : data | P50N/51N_6_113: Protection 50N/51N, unit 6, inhibit order. The protection function output data numbers are given in the characteristics of each function and may be accessed using the data input assistance tool. |
| Predefined control function inputs | V_TRIPCB | Tripping of circuit breaker (contactor) by the switchgear control function. Used to adapt tripping and recloser activation conditions. |
|  | V_INHIBCLOSE | Inhibition of circuit breaker (contactor) closing by the switchgear control function. Used to add circuit breaker (contactor) inhibit closing conditions. |
|  | V_CLOSECB | Closing of circuit breaker (contactor) by the switchgear control function. Used to generate a circuit breaker (contactor) close order based on a particular condition. |
|  | V_SHUTDOWN | Shutdown of genset prime mover. Used to adapt cases of genset shutdown |
|  | V_DE_EXCITATION | Generator de-excitation Used to adapt cases requiring generator de-excitation |
|  | V_FLAGREC | Data saved in disturbance recording. <br> Used to save a specific logic state in addition to those already present in disturbance recording. |
|  | V_RESET | Sepam reset |
|  | V_CLEAR | Clearing of alarms present |
|  | V_INHIBIT_RESET_LO | Inhibition of Sepam reset by UMI Reset key. |
|  | V_CLOSE_NOCTRL | Breaking device closing enabled without synchro-check. Used to adapt the Switchgear control function |
|  | V_TRIP_STP1 to <br> V_TRIP_STP4 | Tripping of capacitor steps 1 to 4 . Used to adapt the Capacitor step control function |
|  | V_CLOSE_STP1 to <br> V_CLOSE_STP4 | Closing of capacitor steps 1 to 4. <br> Used to adapt the Capacitor step control function |
|  | V_TRANS_ON_FLT | Automatic transfer order on fault. Used to adapt automatic transfer |
|  | V_TRANS_STOP | Stopping automatic transfer Used to adapt automatic transfer |
|  | V_DLG_START | Data log function activation |
|  | V_MSR_START | Start an MSR |
| Local variables, constants |  |  |
| Type | Syntax | Example, meaning |
| Local variables stored | VL1 to VL31 | The values of these variables are saved in the event of an auxiliary power outage and are restored when Sepam starts again. |
| Local variables not stored | VV1 to VV31 | The values of these variables are not saved in the event of an auxiliary power outage. They are assigned the value of 0 when Sepam starts. |
| Constants | K_1, K_0 | Value not modifiable <br> K_1: always 1 <br> K_0: always 0 |

## Processing in the event of auxiliary power outage

All the variables, with the exception of the variables VVx , are saved in the event of a Sepam auxiliary power outage. The states of the variables are restored when the power is recovered, allowing the states produced by LATCH, SR or PULSE type memory operators to be saved.

## Special cases

■ brackets must be used in expressions that comprise different OR, AND, XOR or NOT operators:
■ V1 = VL1 AND I12 OR P27/27S_1_1. // expression incorrect

- V1 = (VL1 AND I12) OR P27/27S_-1_1. // expression correct
- V1 = VL1 OR I12 OR P27/27S_1_1. // expression correct

■ protection input/output variables (Pnnn_x_y) may not be used in the LATCH function

- function parameters may not be expressions:
$\square$ VL3 = TON ((V1 AND V3), 300) // expression incorrect
- VL4 = V1 AND V3
$\square$ VL3 $=$ TON (VL4, 300) // correct.
Use limit
The number of operators and functions (OR, AND, XOR, NOT, =, TON, TOF, SR, PULSE is limited to 200.


## Examples of applications

## ■ latching of recloser permanent trip signal

By default, this signal is of the pulse type at the recloser output. If required by LATCH (V1) // V1 may be latched
V1 = P79_1_204 // recloser "permanent trip" output.
V1 may then control a LED or output relay in the matrix.

## ■ latching of a LED without latching the protection function

Certain operating conditions call for the latching of indications on the front panel of Sepam, without latching of the tripping output O1.
LATCH (V1, V2) // V1 and V2 may be latched
V1 = P50/51_1_1 OR P50/51_3_1 // tripping, units 1 and 3 of protection 50/51
V2 = P50/51_2_1 OR P50/51_4_1 // tripping, units 2 and 4 of protection 50/51 V1 and V2 must be configured in the matrix to control 2 front panel LEDs.
■ circuit breaker tripping if input $\mathbf{I 1 1 3}$ is present for more than 300 ms
V_TRIPCB = TON (1113, 300).

## ■ live line work (example 1)

If work is underway with power on (indicated by input I205), the relay behavior is to be changed as follows:
1 - circuit breaker tripping by the instantaneous output of protection 50/51 unit 1 or $50 \mathrm{~N} / 51 \mathrm{~N}$ unit 1 AND if input I205 is present:
V_TRIPCB = (P50/51_1_1 OR P50N/51N_1_1) AND I205
2 - Inhibit recloser:
P79_1_113 = I205
■ live line work (example 2)
The user wishes to inhibit protection functions $50 \mathrm{~N} / 51 \mathrm{~N}$ and 46 by an input I204:
P50N/51N_1_113 = $\mathbf{I 2 0 4}$
P46_1_113 = $\mathbf{I 2 0 4}$
■ validation of a $50 \mathrm{~N} / 51 \mathrm{~N}$ protection function by logic input $\mathbf{I} 210$
A $50 \mathrm{~N} / 51 \mathrm{~N}$ protection function with a very low threshold must only initiate tripping of the circuit breaker if it is validated by an input. The input comes from a relay which gives a very accurate measurement of the neutral point current:

## V_TRIPCB = P50N/51N_1_3 AND I210

■ inhibition of circuit breaker closing if thermal alarm thresholds are overrun The temperature protection function 38/49T supplies 16 alarm bits. If one of the first three bits is activated (1 state), the user wishes to inhibit circuit breaker closing V_INHIBCLOSE = P38/49T_1_10 OR P38/49T_2_10 OR P38/49T_3_10
■ remote control order to inhibit protection 50/51 unit 1
VL1=SR(TC63,TC64) // TC63 set inhibition, TC64 reset inhibition
P50/51_1_113 = VL1 // VL1 is stored in the event of an auxiliary power outage.

Control and monitoring functions

## Customized functions using Logipam

The SFT2885 programming software (Logipam) can be used to enhance Sepam by programming specific control and monitoring functions.

Only the Sepam series 80 with a cartridge containing the Logipam SFT080 option can run the control and monitoring functions programmed by Logipam.
Operating principle


## Logipam programming software

The Logipam SFT2885 programming software can be used to:

- adapt predefined control and monitoring functions
- program specific control and monitoring functions, either to replace the predefined versions or to create completely new functions, to provide all the functions required by the application.
It is made up of:
- a ladder-language program editor used to address all Sepam data and to program complex control functions
- a simulator for complete program debugging
- a code generator to run the program on Sepam.

The ladder-language program and the data used can be documented and a complete file can be printed.

Offering more possibilities than the logic-equation editor, Logipam can be used to create the following functions:

- specific automatic transfer functions
- motor starting sequences.

It is not possible to combine the functions programmed by Logipam with functions adapted by the logic-equation editor in a given Sepam.

The Logipam program uses the input data from:

- protection functions
- Ix logic inputs
- GOOSE logic inputs (Gx) available with the IEC 61850 protocol
- remote control orders

■ local control orders transmitted by the mimic-based UMI.
The result of Logipam processing may then be:
■ assigned to a logic output, directly or via the control matrix

- assigned to a LED or message via the control matrix
- transmitted by the communication link, as a new remote indication
- used by the predefined control and monitoring functions
- used to inhibit or reset a protection function.


## Presentation

The reliability of a device is the property that allows its users to have well-placed confidence in the service it delivers.
For a Sepam protection relay, operational reliability consists of ensuring the safety and availability of the installation. This means avoiding the following 2 situations:
■ Nuisance tripping of the protection
Continuity of the electrical power supply is as vital for a manufacturer as it is for an electricity distribution company. Nuisance tripping caused by the protection can result in considerable financial losses. This situation affects the availability of the installation.

- Failure of the protection to trip

The consequences of a fault that is not eliminated can be catastrophic. For safety of operation, the protection relay must detect faults in the power supply as quickly as possible, using discrimination. This situation affects the safety of the installation.

## Self-tests and monitoring functions

On initialization and cyclically during operation, Sepam runs a series of self-tests. These self-tests are designed to detect any failure in its internal and external circuits so as to ensure Sepam's reliability. These failures are classified into 2 categories, major failures and minor failures:

- A major failure reaches the hardware resources used by the protection functions (program memory and analog input for example).
This type of failure risks resulting in failure to trip on a fault or nuisance tripping. In this case, Sepam must go into the fail-safe position as quickly as possible.
- A minor failure affects Sepam's peripheral functions (display, communication except for ACE969-2 and ACE850).
This type of failure does not prevent Sepam from protecting the installation and providing continuity of service. Sepam then operates in downgraded mode.
The classification of failures into 2 categories improves both safety and availability of the installation.

The possibility of a Sepam major failure must be taken into account when selecting the trip command type to maximize availability or safety of the installation (see "Selecting the trip command" page 316).

In addition to the self-tests, the user can activate monitoring functions to improve the installation monitoring:
■ VT supervision (ANSI code 60FL)

- CT supervision (ANSI code 60)
- Trip circuit and closing circuit supervision (ANSI code 74)

■ Auxiliary power supply supervision
These functions send an alarm message to the Sepam display unit and a data item is automatically available to the communication to alert the user.

## Self-tests

The self-tests are run when Sepam is initialized and/or during its operation.
List of self-tests which place Sepam in the fail-safe position
Failures which have caused this are deemed to be major ones.

| Function | Test type | Execution period |
| :--- | :--- | :--- |
| Power supply | Power supply presence | During operation |
| CPU | Embedded software | During operation |
|  | Processor RAM memories | On initializization and during operation |
| Program memory | Checksum | On initialization and during operation |
| Parameter memory | Checksum | On initialization |
| Analog inputs | Acquisition consistency  <br> Infinite gain During operation <br> Logic outputs Relay driver | During operation |
| Connection | CCA630, CCA634, <br> CCA671, CCT640 | On initialization and during operation |

List of self-tests which do not place Sepam in the fail-safe position
Failures which have caused this are deemed to be minor ones.

| Function | Test type | Execution period |
| :--- | :--- | :--- |
| UMI | Module presence | On initialization and during operation |
|  | Memory On initialization <br>  Software | During operation |
| Analog output | Module presence | On initialization and during operation |
| Temperature inputs | Module presence | On initialization and during operation |
| Battery voltage | Minimum value <br> check | During operation |



## Fail-safe position

When Sepam is in working order, it runs self-tests continuously. Detection of a major failure places Sepam in the fail-safe position.

## State of Sepam in the fail-safe position

- All the output relays are forced to the idle state
- All protection functions are inhibited
- The watchdog output indicates failure (output in the idle state)
- A red LED on the Sepam front panel is on and a diagnostic message appears on the Sepam display unit (see "Local indication" page 300).


## How Sepam deals with failures

- Minor failure: Sepam switches to downgraded operation.

The failure is indicated on the Sepam display unit and also by the communication. Sepam continues to protect the installation.

- Major failure: Sepam switches to the fail-safe position and attempts a restart during which it again runs its self-tests. There are 2 possible scenarios:口 The internal failure is still present. It is a permanent failure. Intervention on Sepam is required. Only removing the cause of the failure, followed by de-energizing and then energizing Sepam, will allow the unit to exit the fail-safe position.
$\square$ The internal failure is no longer present. It is a transient failure. Sepam restarts so that it can continue to protect the installation. Sepam has been in the fail-safe position for 5 to 7 s .


## Limiting the number of transient failure detections

Each time a transient internal failure appears, Sepam increments an internal counter. The fifth time the failure occurs, Sepam is placed in the fail-safe position. Deenergizing Sepam reinitializes the failure counter. This mechanism can be used to avoid keeping a Sepam running that is subject to repeated transient failures.

## Selecting the trip command and examples of use

An analysis of the operational reliability of the whole installation should determine whether availability or safety of this installation should be prioritized if Sepam is in the fail-safe position. This information is used to determine the choice of trip command as outlined in the table below.

## NOTICE

RISK OF UNPROTECTED INSTALLATION
Always connect the watchdog output to a monitoring device when the selected trip command does not result in the installation tripping when Sepam fails.
Failure to follow these instructions can result in equipment damage.

## Selecting the trip command

| Diagram | Control | Event | Trip | Advantage | Disadvantage |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Shunt trip breaker or mechanical latching contactor | Sepam failure or loss of the auxiliary power supply | No | Availability of the installation | Installation not protected until remedial intervention ${ }^{(1)}$ |
| 2 | Breaker with undervoltage trip coil (fail-safe) | Sepam failure or loss of the auxiliary power supply | Yes | Safety of the installation | Installation not available until remedial intervention |
| 3 | Breaker with undervoltage trip coil (not fail-safe) | Sepam failure | No | Availability of the installation | Installation not protected until remedial intervention ${ }^{(1)}$ |
|  |  | Loss of auxiliary power supply | Yes | Safety of the installation | Installation not available until remedial intervention |
| 4 | Contactor without coil latching (permanent order) | Sepam failure or loss of the auxiliary power supply | Yes | Safety of the installation | Installation not available until remedial intervention |

(1) It is essential to use the watchdog, see the warning notice opposite.

Example of use with shunt trip coil (diagram 1)



Example of use with undervoltage trip coil without fail-safe condition (diagram 3)


## Example of use with contactor under permanent order command (diagram 4)


(1) Standard assignments, can be modified.

## Using the watchdog

The watchdog is extremely important in the monitoring system, as it indicates to the user that the Sepam protection functions are working correctly. When Sepam detects an internal failure, an LED flashes automatically on the Sepam front panel regardless of whether the watchdog output is connected correctly. If the watchdog output is not correctly connected to the system, this LED is the only way of knowing that Sepam has failed. We therefore strongly recommend connecting the watchdog output at the highest level of the installation so that an effective alarm is generated when necessary. For example, an audible alarm or flashing alarm lamp can be used to warn the operator.

| Watchdog output status | No failure detected | Failure detected |
| :---: | :---: | :---: |
| Watchdog output connected correctly to the control system | The protection functions are in working order | - The protection functions are not working. <br> - Sepam is in the fail-safe position. <br> - The Sepam alarm LED flashes. <br> - The watchdog output activates a system alarm. <br> - The operator is warned that he needs to intervene. |
| Watchdog output not connected | The protection functions are in working order | - The protection functions are not working. <br> - Sepam is in the fail-safe position. <br> - The Sepam alarm LED flashes. <br> - The need of maintenance is detected only if an operator controls the front panel of the digital relay. |

Notes

Notes

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$\square$
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[^0]:    SFT2841: parameter setting of the Capacitor step control

[^1]:    (1) By default.

